

REV	DESCRIPTION	DATE	BY	APPROVED	DOCUMENT
A	General Revisions				

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 E: info@mswconsulting.ie
 Kimmage, Dublin 12.
 Ravensthal Park,
 Unit B19, KCR Estate,



Re:	SUDS Maintenance Plan
SD22A/0124	Citywise Science & Language Centre, Durrkan Centre, Fortunesdown Way, Tallaght, Dublin, A94 YX22.
Client: Citywise Education	
Date: 19th October 2021	

2011-0001

For this proposed development it is proposed that nature-based solutions will be employed within the SUDS networks where suitable.

Nature-based solutions (NBS) are structures used to replicate the management of stormwater as would be done without urban intervention. The use of these systems aids biodiversity and ecosystems, mitigates the risk of floods and also improves water quality and prevents erosion. NBS uses trees and plants reduce water run-off in extreme rain events, taking pressure off the urban drainage system.

Sustainable Urban Drainage Systems (SUDS) have been developed and are in use to alleviate the detrimental effects of traditional urban storm water drainage practice that typically consisted of piping rainfall runoff from developments to the nearest watercourse. Storm water drainage methods that take account of the quantity, quality and amenity issues associated with the management of surface/storm water run-off are referred to as Sustainable Urban Drainage Systems. These systems include one or more structures that manage the surface/storm water run-off in a way that minimises the negative impacts on the quantity and quality of stormwater runoff, while maximising the benefits to the amenity and biodiversity of the surrounding environment. These systems are particularly effective at achieving the above objectives with the use of nature based

2.0 SUDS & Storm water:

All new hardstanding contributing areas (i.e. pavement and flat roof) for this new development are to be served by the proposed SUDS measures.

All proposed developments must ensure that SUDS are incorporated into the development. SUDS requires that post development run-off rates be maintained at the equivalent to, or lower than, the predevelopment run-off levels. Thus, the development must be able to retain, within its boundaries, storm volumes from extreme storm events up to and including a design for a 1 in 100 year storm event, also expressed as a 1.0% AEP (Annual Exceedance Probability), while also allowing for climate change factors (+CC). Any new development must have physical capacity to retain storm volumes as directed under the Greater Dublin Strategic Drainage Study (GDS) and, if necessary, release this attenuated surface water run-off before it enters a natural watercourse or into a public sewer, which ultimately discharges to a water body. This is to ensure the highest possible standard of storm water quality.

The west side of this area of the campus site is affected by the proposed development which is 1940m². The new development has impermeable roof area of 750m² and pavement area of 360m². The stormwater runoff from the new roof area and the new pavement area are to be managed as parts of the SUDs plan for the new development.

The existing Citywise Education site is 0.44ha, has an existing building used for education purposes, with a footprint area of 800m².

With reference to Condition No.7 of the Grant of Permission, regarding the details of the Sustainable Drainage Systems (SUDS), and storm water management to be included in the proposed development.

1.0 Introduction:

- 3.0 Site Characteristics:**
- The site is predominantly level/flat, with raised berms at parts of the south and south-west boundaries. The extent of the development site is quite small, approximately 1940m² (0.194Ha), of which the footprint of the new building having an approximate plan area of 750m². The surface water drainage is currently serviced by a 300mm diameter public storm sewer to the front/north boundary of the site, and a 225mm diameter public storm sewer which runs adjacent to the front/north boundary of the site, and a 225mm diameter public storm sewer to the rear/south-east of the site in Bawulea Close. The invert levels of both the surface water manholes are relatively shallow, 0.75m and 0.84m below ground level.
- 4.0 Site Specific Design:**
- 4.1 To assess the properties of the underlying soils on the site to ensure suitable site-specific SUDS components are employed for this development.
- A trial pit was excavated, and the existing sub-soil conditions were exposed. The exposed soil conditions appeared to be a silty sandy loam composition. The trial pit excavation was carried out to the south-west of the site. A trial pit was excavated to a depth of 1.5m below ground level.
- 4.2 The presence of ground water was noted at the base of the excavation and was recorded at 1.5m below ground level.
- For the assessment of the underlying soil for infiltration of the stormwater runoff, Percolation tests were carried out in accordance with the procedure described in BRE Digest 365. This test was carried out from the 27th to the 30th of July 2022.
- An infiltration rate (f) of 2.8×10^{-6} m/s was calculated*, and was deemed satisfactory for infiltration SUDS components to be employed as per CIRIA 753 SUDS Manual Table 25.1. See Appendix A.4 for attached infiltration calculation sheet. [* Trial pit was already empty after third fill when inspection of the 30th July 2022, therefore f value calculated is believed to be conservative].
- 4.3**
- With reference to CIRIA CT53 SUDS Manual, a Factor of Safety of 2.5 was applied to give an Adjusted Soil Infiltration Rate (q) of 1.12×10^{-6} m/s, which was used for hydraulic calculations associated with the SUDS elements.
- 4.4**

The first component of the SUDS treatment train is the use of Surface Channels. Surface Channels and/or rills are used for conveying rainwater have a positive presence in the urban

5.1 Surface Channels/Rills:

- treatment trains for this development:
 - Surface Channel/Rill conveyance element.
 - Bio-Retention Swales/Rainwater Gardens (both with Type A – infiltration), both using soil/sand media to increase volume storage and infiltration.
 - Attenuation Flow control outlet chamber.

The following SUDS measures are the elements that make up the proposed SUDS

It is proposed that there will be two SUDS treatment trains to address the rainwater run-off from the impermeable roof surface of the new development, and that a single treatment train will be located in the longitudinal section of the proposed SUDS treatment trains. Stage (permeable paving) for the new hardstand pavements areas. See attached plan drawing D-01 Rev E and Section drawing D-03 Rev A, documenting the proposed drainage layout, systems. This is due to the observed level of the ground water table in this location and the stormwater outlets servicing the site are also relatively shallow/close to the surface.

It is noted that the SUDS components proposed for this development are typically 'shallow' due to the risk of inundation of their specialised root systems/structure, that typically require a low-level drain which on this site would fall below our Storm Sewer outlet level.

3.6 Site Specific SUDS Measures:
Sustainable Urban Drainage Systems (SUDS) were considered for the site, in line with recommendations of Greater Dublin Strategic Drainage Strategy (GDS), CIRIA Report 753 The SUDS Manual, and Sustainable Drainage Exploratory Design & Evaluation Guide 2022. Particular consideration was given to employing Nature Based SUDS Solutions (NBS) which replicate the natural characteristics of rainfall runoff from any site.

5.0 Site Specific SUDs Measures:

is the greater.

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Qbar (rural) - Site Specific Calculations:	Hydrological Characteristics of the Site:	SStandard Area Average Rainfall [SALAR]	[Ret. Met Breanna].	Soil Index/Factor	0.387
822mm	SStandard Area Average Rainfall [SALAR]	[Ret. Met Breanna].	[Ret. Met Breanna].	(see Appendix A.5)	0.387
822mm	SStandard Area Average Rainfall [SALAR]	[Ret. Met Breanna].	(see Appendix A.5)	Qbar(rural) (mean annual flood flow rate)	3.8 l/s/Ha
822mm	SStandard Area Average Rainfall [SALAR]	[Ret. Met Breanna].	(see Appendix A.5)	(see Appendix A.5 for calculation sheet)	(see Appendix A.5 for calculation sheet)

Annual Flood, reference CIRIA C753 SUDS Manual Equation 24.3.

4.5.1 \bar{Q}_{bar} (rural) - which is the estimation of equivalent Flow for Mean

the following references:

The following table gives the relative values:

The maximum profit from the site has to be ascertained. This was done using the following approach:

1.0 assess the technical acquisition requirements and how could it be accelerated.

To assess the required attenuation volumes and flow control requirements:

4.5 Stormwater Runoff Outflow Limits:

MSW & Associates Ltd.

3.3.1. **Permeable Pavement** - Various paving options are proposed to receive the run-off from all of the new paved areas.

5.5 Permeable/Previous Pavings:

The Perforated Riser located within a small attenuation chamber downstream of the proposed SUDS measures, has been designed in accordance with SUDS Handbook CIRIA C753 28.5.3 to restrict the outflow and have a Total Flow Capacity of 3.8L/sec/ha when connected to the existing stormwater sewer within the site. See Appendix A.11 calculation sheet for the Perforated design calculations.

The overflow from the Bio Retention Chamber drains to a small attenuation chamber which contains a simple overflow device. As a means of controlling the outflow from the development, a Perforated Riser is the proposed control structure to restrict the overflow from the SUDS treatment trains. From our rainwater attenuation calculations, the flow control chamber will only be utilised for the greater storm event; i.e. 100 year-6 hour

5.4 Attenuation Chamber with Flow Control Device:

Both swales, from each SUDS treatment train convey their overflows to a single Bio Retention Rainwater Garden which is located at the south end of the site. The Bio Retention Rainwater Garden is a shallow landscaped depression that is used to intercept and manage the stormwater runoff. Rainwater Gardens typically are attractive landscape features that improve the amenity space. Like the bio retention swale, it offers full infiltration in this case and is also under drained with modular geo-cellular units, but to the full plan area to increase storage capacity. See detail drawing D-03 Rev C for proposed details and composition. Like the previous swales, the Rainwater Garden will have suitable ground cover plants to the lower level, with suitable trees planted to the perimeter, (both plant and trees specifications as advised by the Landscape Architect). These Rainwater Garden will also have a maximum attenuation depth of 150mm, and an overflow outlet.

5.3 Bio Retention Rainwater Garden:

The next component in each SUDS train is the use of a Bio Retention swale. Swales are based on open channel design for conveyance, but also provide a means runoff volume control with infiltration, and attenuation. We have included Zno. vegetated swales (one in each treatment train), which we believe will improve the amenity space of this re-creation area. These bio retention swales are also framed with a length of modular geo-cellular units (which have a high void ratio) to increase below ground storage capacity. Typically the swales will have suitable ground cover plants to the lower level, with suitable trees to the perimeter, (both plant and trees specifications as advised by the Landscape Architect). These swales have a maximum attenuation depth of 150mm, before conveying to the next element. See drawing D-03 Rev C for proposed details and composition.

5.2 Bio-Retention Swale:

environment, creating unique spaces that can be enjoyed. The use of hills/surface channels with other nature based solutions connects people, nature and water.

See attached SUDS calculation sheet and Summary sheet for 10year and 100year storm events calculations, Appendix A.6-A.10.

Total Inflow (m^3)	71.7
Less Treatment Train AC storage Volume (m^3)	29.7
Less Treatment Train BC storage Volume (m^3)	34.1
Less Infiltration during Storm Duration Volume (m^3)	5.2
Net Excess inflow over Storage Capacity (m^3)	2.7

6.5 100 Year - 6HR Storm: Runoff & Storage Quantities Recap:

Design Parameters:	Ref.
Max Run-off Rate:	3.8L/s/ha
Storm Return Periods:	10yr.; 100yr.
Max Rainfall Return Periods:	20.9m; 68mm
Max Rainfall for Extreme Storm Duration:	60 min.; 6 hour
Rainfall Return Periods:	50m ²
Impenetrable area:	Melbourne (Caserment)
Climatic Change Factor:	20%

(See Appendix A.6-A.10 attached calculation sheets):

6.3 Storage Components of the Treatment Trains:

6.2 The attenuated runoff is stored for infiltration, with the estimated excess (2.8m³) released via the perforated riser flow control device to the existing stormwater outfall. This release rate 1.87L/sec/Ha is significantly less than the maximum allowable outfall rate (Qbar or the GDRCP rate 2L/sec/Ha); see attached calculation sheet, Appendix A.11.

6.1 The extreme storm event, 100year - 6hour storm, defines the stormwater volumes that are to be managed for the new development. It is proposed to use two SUDS treatment trains to manage the stormwater runoff from a 100year stormwater runoff from a 100year - 6 hr. storm event.

6.0 Stormwater Quantity Design:

Permeable pavements provide a permeable suitable for pedestrian and/or vehicular traffic, while allowing rainwater to infiltrate through the surface and into the underlying structural layers, and also attenuates the rainwater beneath the overlying surface before infiltration. Permeable pavements are an efficient means of managing surface water close to its source - intercepting runoff, reducing the volume and frequency of runoff, and providing a treatment medium. See attached plan drawing D-01 Rev E and details drawing D-02 Rev C for proposed extent and section of the permeable pavement.

1. Storm Drainage Layout Plan - Drawing D-01 Rev E
2. Storm Drainage Details - Drawing D-02 Rev C
3. Storm Drainage - Long. Sections D-03 Rev A
4. Infiltration Rate Calculation Sheet
5. Mean Annual Flood Flow Calculation [$Q_{bar(wa)}]$
6. SUDS Train A-C Calculation Sheet - 10 Year 60min Storm
7. SUDS Train A-C Calculation Sheet - 100 Year 6 Hr. Storm
8. SUDS Train B-C Calculation Sheet - 10 Year 60min Storm
9. SUDS Train B-C Calculation Sheet - 100 Year 6 Hr. Storm
10. Summary of SUDS Soakaway & Attenuation water volumes
11. Perforated Riser Flow Control Calculation Sheet

Appendix A

Signed: _____ Date: _____

Marty Wardick
Chartered Engineer
MSW

Soil Infiltration Rate Calculation:																																																																												
Project:	New Citywise Science & Language Centre																																																																											
Location:	Durkan Centre, Fortunstown Way, Tallaght, Dublin 24.																																																																											
Dimensions:	<table border="1"> <tr> <td>Length (l) =</td> <td>0.6 m</td> <td>1st filling:</td> <td>2nd filling:</td> <td>3rd filling:</td> </tr> <tr> <td>Width (w) =</td> <td>0.875 m</td> <td></td> <td></td> <td></td> </tr> <tr> <td>Height (h) =</td> <td>1.5 m</td> <td></td> <td></td> <td></td> </tr> <tr> <td>Depth Depth:</td> <td>0.520 m</td> <td>15.35 pm</td> <td>12.30 pm</td> <td>0.00 m</td> </tr> <tr> <td>Depth of water (d1) =</td> <td>0.520 m</td> <td>29-JUL-22</td> <td>28-JUL-22</td> <td>29-JUL-22</td> </tr> <tr> <td>Depth of water (d2) =</td> <td>0.520 m</td> <td>30-JUL-22</td> <td>30-JUL-22</td> <td>30-JUL-22</td> </tr> <tr> <td>Initial Volume of Water</td> <td>0.273 m³</td> <td>15.35 pm</td> <td>12.30 pm</td> <td>0.00 m</td> </tr> <tr> <td>Final Volume of Water</td> <td>0 m³</td> <td>12.30 pm</td> <td>0.00 m</td> <td>0.00 m</td> </tr> <tr> <td>Depth delta =</td> <td>0.52 m</td> <td>[use 24hr click]</td> <td></td> <td></td> </tr> <tr> <td>Time delta =</td> <td>1257 minutes</td> <td>75420 secs</td> <td>20.95 hrs</td> <td>td (100-0)</td> </tr> <tr> <td>Soil Infiltration Rate (f) = VP(100-0) / AP50 x tp(100-0)</td> <td>as per BRE 365</td> <td></td> <td></td> <td></td> </tr> <tr> <td>VP(100-0)</td> <td>0.273 m³</td> <td>percentage drop in volume of water in 24 hours</td> <td>100.00%</td> <td>OK percolation volume greater than 50% in 24hrs</td> </tr> <tr> <td>AP50 =</td> <td>1.292 m²</td> <td>$AP50 = ((l+w) \times 2 \times \text{delta } d) + (l \times w)$</td> <td></td> <td></td> </tr> <tr> <td>Safety Factor (1.5 - 10)</td> <td>2.5</td> <td>0.01008593 m/hr</td> <td>2.80E-06 m/s</td> <td>Ref SUDS Manual C697 4-30</td> </tr> <tr> <td>Adjusted Soil Infiltration Rate (q)</td> <td>1.1207E-06 m/s</td> <td>0.00403437 m/hr</td> <td></td> <td></td> </tr> </table>	Length (l) =	0.6 m	1st filling:	2nd filling:	3rd filling:	Width (w) =	0.875 m				Height (h) =	1.5 m				Depth Depth:	0.520 m	15.35 pm	12.30 pm	0.00 m	Depth of water (d1) =	0.520 m	29-JUL-22	28-JUL-22	29-JUL-22	Depth of water (d2) =	0.520 m	30-JUL-22	30-JUL-22	30-JUL-22	Initial Volume of Water	0.273 m ³	15.35 pm	12.30 pm	0.00 m	Final Volume of Water	0 m ³	12.30 pm	0.00 m	0.00 m	Depth delta =	0.52 m	[use 24hr click]			Time delta =	1257 minutes	75420 secs	20.95 hrs	td (100-0)	Soil Infiltration Rate (f) = VP(100-0) / AP50 x tp(100-0)	as per BRE 365				VP(100-0)	0.273 m ³	percentage drop in volume of water in 24 hours	100.00%	OK percolation volume greater than 50% in 24hrs	AP50 =	1.292 m ²	$AP50 = ((l+w) \times 2 \times \text{delta } d) + (l \times w)$			Safety Factor (1.5 - 10)	2.5	0.01008593 m/hr	2.80E-06 m/s	Ref SUDS Manual C697 4-30	Adjusted Soil Infiltration Rate (q)	1.1207E-06 m/s	0.00403437 m/hr		
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Project: Citywise, Fortunestown Lane	
Catchment Area =	1940 m ²
Catchment Area =	0.5 km ²
Catchment Area =	50 ha
Standard Area Average Rainfall (SARR) =	0.00194 km ²
Citywise, Tailaght	822 mm
Citywise, Tailaght	0 %
Citywise, Tailaght	10 %
Citywise, Tailaght	60 %
Citywise, Tailaght	30 %
Citywise, Tailaght	0 %
SPR (Soil Index: Per-centagge Run-off)	0.387
Total =	100 %
Soil Type 5 =	0 %
Soil Type 4 =	30 %
Soil Type 3 =	60 %
Soil Type 2 =	10 %
Soil Type 1 =	0 %
Soil =	$0.37 [SOIL1] + 0.47 [SOIL4] + 0.53 [SOIL5]$
$Q_{bar} = 0.00108 \times (AREA)^{0.89} \times SARR^{1.17} \times SPR^{2.17}$	
Mean Annual Flood Rate ($Q_{bar(ran)}$) = 191.1 ltrs/sec	
for Area = 50Ha	
Ref. Eqn. 24.3 China C753 The Suds Manual	
Greenfield Peak Run-off = 0.1911 m³/sec	
for Area = 50Ha	
Ref. Eqn. 24.3 China C753 The Suds Manual	
This is the Maximum Allowable Discharge from the Development Site	
$Q_{bar} = 0.74 \text{ ltrs/sec}$ $Q_{bar(ran)} \text{ for } 194 \text{ Ha} = 191.1 \text{ ltrs/sec}$	
Area = Area of Catchment (km ²)	
SARR = Standard Area Average Rainfall (mm)	
SPR = Standard Percentage Run-off (also known as Soil Index)	
Qbar = The peak rate of flow from a catchment for the mean annual flood (a return period of approx 1:2.3 years)	

Project: New Ciwicise Science & Language Centre		Location: Durkan Centre, Fortunstown Way, Tallaght, Dublin 24.	
Total Area of Site		SUDS CHAIN-B-C (See Section B-C)	
Area Data:		Impenetrable Area 750 m ² New Roof Area 1940 m ² Effective Area [m ²] 375 m ²	
Rainfall Period Rainfall Depths [Ref. Met Éireann]		Eff. Area drained to Soakaway 637 m ² Incl 20% CCA	
Design Rainfall (100-6hr):		Inflow to Soakaway [A x R10-60]:	
100 year storm - 6hr. duration:		36.5 m ³	
SUDS MEASURE #1		Proposed infiltration Structure - Dims: BIO-RET. SWALE #B	
SUDS MEASURE #2		Proposed infiltration Structure - Dims: BIO-RET. RAINWATER GRDN #C	
SUDS MEASURE #2		Outflow = 2.57 m ³	
SUDS MEASURE #1		Outflow = 7.050 m ³	
SUDS MEASURE #1		Outflow from Soakaways during storm (Q) Q=AS50 x f x D BIO-RET. SWALE	
SUDS MEASURE #2		Outflow from Soakaways during storm (Q) Q=AS50 x f x D BIO-RET. RAINWATER GRDN #C	
SUDS MEASURE #2		Outflow = 0.75 m ³	
SUDS MEASURE #1		Outflow = Storage Required (I-O=S) 33.19 m ³	
SUDS MEASURE #1		Storage Available 34.15 m ³	
SUDS MEASURE #1		Total Soakage Vol = 10.9 m ³	
SUDS MEASURE #1		Total Soakage #B & RWG #C (50%) Filter Layer Storage Vol = 23.3 m ³	
SUDS MEASURE #1		Adequate Attenuation Volume: greater than inflow	

CITYWISE EDUCATION, FORTUNESTOWN LANE, DUBLIN 2.
SUMMARY RECAP OF STORAGE & ATTENUATION CAPACITIES

Project:	New Citywise Science & Language Centre	Location:	Duthraen Centre, Fortunestown Way, Tallaght, Dublin 24.
Total Flow Capacity of Perforeted Riser	$Q = CP \cdot 2AP \cdot (2g)_{1/2} \cdot (H_{3/2})^2$	Q_{HS}	m^3/s
Ref.: CIRIA C753	285.3	0.000164932 m^3/sec	$1.65E-04 \text{ m}^3/sec$
Q= discharge, m^3/s	(Using input below in blue)	0.165 m^3/sec	1.87 $m^3/sec/ha$
$C_P =$ discharge coeff (0.61 for perforations)	0.61	0.00076302 m^2	0.0045 m
no of holes per row	4.5 mm	4.5 mm	0.0045 m
no. of rows	3 no.	3 no.	12 no.
Radius of holes	9.81 mm	9.81 mm	9.81 mm^2
no. of holes	12 no.	12 no.	12 no.
Gravty	$g = 9.81 \text{ m/s}^2$	$g = 9.81 \text{ m/s}^2$	$g = 9.81 \text{ m/s}^2$
hs=Distance from S/2 below the lowest row of holes to S/2 above the top row, m	225 mm	0.225 m	0.225 m
S=distance between holes, m	75 mm	0.075 m	0.075 m
H=effective head, m	90 mm	0.090 m	0.090 m
Allowable flow for Area	$0.000176 \text{ m}^3/sec$	$0.000176 \text{ m}^3/sec$	0.176 L/sec
Catchment area served =	860 m^2	$0.000002 \text{ m}^3/s/m^2$	$0.000176 \text{ m}^3/sec$
Allowable flow for Row	$2 \text{ L/ha}=$	$0.000002 \text{ m}^3/s/m^2$	$0.000176 \text{ m}^3/sec$
Impenetrable & permeable areas served by SUDs measures on catchment chains with overflow to Flow Control Chamber			
OK Prefered Riser Outflow < Max Allowable Flow for Area			