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SUDS Drainage Report Re: SD22A/0124 Citywise Science & Language Centre, Durkan Centre, Fortunestown Way, Tallaght, Dublin, A94 YX22.

**Client: Citywise Education** 

Date: 19<sup>th</sup> October 2023



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### 1.0 Introduction:

With reference to Condition No.7 of the Grant of Permission, regarding the details of the Sustainable Drainage Systems (SUDS), and storm water management to be included in the proposed development.

The existing Citywise Education site is 0.44ha, has an existing building used for education purposes, with a footprint area of  $800m^2$ .

The west side of this area of the campus site is affected by the proposed development is  $1940m^2$ . The new development has impermeable roof area of  $750m^2$  and pavement area of  $360m^2$ . The stormwater runoff from the new roof area and the new pavement area are to be managed as parts of the SUDs plan for the new development.

All proposed developments must ensure that SUDS are incorporated into the development. SUDS requires that post development run-off rates be maintained at the equivalent to, or lower than, the predevelopment run-off levels. Thus, the development must be able to retain, within its boundaries, storm water volumes from extreme storm events up to and including a design for a 1 in 100year storm event, also expressed as a 1.0% AEP (Annual Exceedance Probability), while also allowing for climate change factors (+CC). Any new development must have physical capacity to retain storm water volumes as directed under the Greater Dublin Strategic Drainage Study (GDSDS) and, if necessary, release this attenuated surface water runoff before it enters a natural watercourse or into a public sewer, which ultimately discharges to a water body. This is to ensure the highest possible standard of storm water quality.

All new hardstanding contributing areas (i.e. pavement and flat roof) for this new development are to be served by the proposed SUDS measures.

#### 2.0 SUDS & Storm water:

Sustainable Urban Drainage Systems (SUDS) have been developed and are in use to alleviate the detrimental effects of traditional urban storm water drainage practice that typically consisted of piping rainwater runoff from developments to the nearest watercourse. Storm water drainage methods that take account of the quantity, quality and amenity issues associated with the management of the stormwater are referred to as Sustainable Urban Drainage Systems. These systems include one or more structures that manage the surface/storm water run-off in a way that minimises the negative impacts on the quantity and quality of stormwater runoff, while maximising the benefits to the amenity and biodiversity for people and the surrounding environment. These systems are particularly effective at achieving the above objectives with the use of 'nature based solutions'.

Nature-based solutions (NBS) are structures used to replicate the management of stormwater as would be done without urban intervention. The use of these systems aids biodiversity and ecosystems, mitigates the risk of floods and also improves water quality, and prevents erosion. NBS uses trees and plants reduce water run-off in extreme rain events, taking pressure off the urban drainage system.

For this proposed development it is proposed that nature-based solutions will be employed within the SUDS networks where suitable.

### **3.0** Site Characteristics:

The site is predominantly level/flat, with raised berms at parts of the south and south-west boundaries. The extent of the development site is quite small, approximately  $1940m^2$  (0.194Ha), of which the footprint of the new building having an approximate plan area of  $750m^2$ .

The surface water drainage is currently serviced by a 300mm diameter public storm sewer which runs adjacent to the front/north boundary of the site, and a 225mm diameter public storm sewer to the rear/south-east of the site in Bawnlea Close. The invert levels of both the surface water manholes are relatively shallow, 0.75m and 0.84m below ground level.

### 4.0 Site Specific Design:

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- 4.1 To assess the properties of the underlying soils on the site to ensure suitable site-specific SUDS components are employed for this development. A trial pit was excavated, and the existing sub-soil conditions were exposed. The exposed soil conditions appeared to be a silty sandy loam composition. The trial pit excavation was carried out to the south-west of the of the site and was excavated to a depth of 1.5m below ground level.
- 4.2 The presence of ground water was noted at the base of the excavation and was recorded at 1.5m below ground level.
- 4.3 For the assessment of the underlying soil for infiltration of the stormwater runoff, Percolation tests were carried out in accordance with the procedure described in BRE Digest 365. This test was carried out from the 27<sup>th</sup> to the 30<sup>th</sup> of July 2022.
  An infiltration rate (f) of 2.8x10<sup>-6</sup>m/s was calculated\*, and was deemed satisfactory for infiltration SUDs components to be employed as per CIRIA C753 SUDS Manual Table 25.1. See Appendix A.4 for attached Infiltration Calculation sheet. [\* Trial pit was already empty after third fill when inspection of the -30<sup>th</sup> July 2022, therefore f value calculated is believed to
- 4.4 With reference to CIRIA C753 SUDS Manual, a Factor of Safety of 2.5 was applied to give an Adjusted Soil Infiltration Rate (q) of 1.12x10<sup>-6</sup>m/s, which was used for hydraulic calculations associated with the SUDS elements.

# 4.5 Stormwater Runoff Outflow Limits:

To assess the required attenuation volumes and flow control requirements the maximum runoff from the site has to be ascertained This was done using the following references:

**4.5.1** Qbar (rural) – which is the estimation of equivalent Flow for Mean Annual Flood, reference CIRIA C753 SUDS Manual Equation 24.3.

Qbar (rural) - Site Specific Calculation:	
Hydrological Characteristics of the Site:	
Standard Area Average Rainfall [SAAR]	822mm
[Ref. Met Eireann].	
Soil Index/Factor	0.387
(see appendix A.5)	
Qbar(rural) (mean annual flood flow rate)	3.8 L/s/Ha
(see appendix A.5 for calculation sheet)	

**4.5.2 Greater Dublin Regional Code of Practice** – Runoff discharge rate equal to 1-year greenfield site peak runoff rate or **2 l/s/ha**, whichever is the greater.

# 5.0 Site Specific SUDs Measures:

Sustainable Urban Drainage Systems (SUDS) were considered for the site, in line with recommendations of *Greater Dublin Strategic Drainage Strategy (GDSDS)*, *CIRIA Report 753 The SUDs Manual*, and *Sustainable Drainage Explanatory Deign & Evaluation Guide 2022*. Particular consideration was given to employing Nature Based SUDS Solutions (NBS) which replicate the natural characteristics of rainfall runoff from any site.

It is proposed that there will two SUDS treatment trains to address the rainwater run-off from the impermeable roof surface of the new development, and that a single treatment stage (permeable paving) for the new hardstand pavement areas. See attached plan drawing D-01 Rev E and Section drawing D-03 Rev A, documenting the proposed drainage layout, and longitudinal section of the proposed SUDS treatment trains.

It is noted that the SUDS components proposed for this development are typically 'shallow' systems. This is due to the observed level of the ground water table in this location and that the stormwater outfalls servicing the site are also relatively shallow/close to the surface.

It is for these reasons that **Bio- Retention Tree pits** have **not** been included in this proposal, due to the risk of inundation of their specialised root systems/structure, that typically require a low-level drain which on this site would fall below our Storm Sewer outfall level.

The following SUDS measures are the elements that make up the proposed SUDS treatment trains for this development:

- Surface Channel/Rill conveyance element.
- Bio- Retention Swales/ Rainwater Gardens (both with Type A infiltration), both using soakaway media to increase volume storage and infiltration.
- Attenuation Flow control outlet/chamber.

# 5.1 Surface Channels/Rills:

The first component of the SUDS treatment train is the use of Surface Channels. Surface Channels and/or rills are used for conveying rainwater have a positive presence in the urban

environment, creating unique spaces that can be enjoyed. The use of rills/surface channels with other nature based solutions connects people, nature and water.

Surface channels in this case are proposed to convey the collected rainwater from the new building's roof to the next SUDS component in the train. See drawing D-03 Rev C for proposed detail.

# 5.2 **Bio-Retention Swale:**

The next component in each SUDS train is the use of a Bio Retention swale. Swales are based on open channel design for conveyance, but also provide a means runoff volume control with infiltration, and attenuation. We have included 2no. vegetated swales (one in each treatment train), which we believe will improve the amenity space of this recreation area. These bio retention swales are also under drained with a length of modular geocellular units (which have a high void ratio) to increase below ground runoff storage capacity. Typically the swales will have suitable ground cover plants to the lower level, with suitable trees to the perimeter, (both plant and trees specifications as advised by the Landscape Architect). These swales have a maximum attenuation depth of 150mm, before conveying to the next element. See drawing D-03 Rev C for proposed details and composition.

# 5.3 Bio Retention Rainwater Garden:

Both swales, from each SUDS treatment train convey their overflows to a single Bio Retention Rainwater Garden which is located at the south end of the site. The Bio Retention Rainwater Garden is a shallow landscaped depression that is used to intercept and manage the stormwater runoff. Rainwater Gardens typically are attractive landscape features that improve the amenity space. Like the bio retention swale, it offers full infiltration in this case and is also under drained with modular geo-cellular units, but to the full plan area to increase runoff storage capacity. See detail drawing D-03 Rev C for proposed details and composition. Like the previous swales, the Rainwater Garden will have suitable ground cover plants to the lower level, with suitable trees planted to the perimeter, (both plant and trees specifications as advised by the Landscape Architect). These Rainwater Garden will also have a maximum attenuation depth of 150mm, and an overflow outlet.

# 5.4 Attenuation Chamber with Flow Control Device:

The overflow from the Bio Retention Rainwater Garden drains to a small attenuation chamber which contains a simple overflow device. As a means of controlling the outflow from the development, a Perforated Riser is the proposed control structure to restrict the overflow from the SUDS treatment trains. From our rainwater attenuation calculations, the flow control chamber will only be utilised for the greater storm event; i.e. 100 year- 6 hour storm.

The Perforated Riser located within a small attenuation chamber downstream of the proposed SUDS measures, has been designed in accordance with SUDS Handbook CIRIA C753 28.5.3 to restrict the outflow and have a Total Flow Capacity of 3.8L/sec/ha when connected to the existing stormwater sewer within the site. See Appendix A.11 calculation sheet for the Perforated design calculations

# 5.5 **Permeable/Pervious Paving:**

Outside the above SUDS treatment trains, it is also proposed to use a Type A [Total Infiltration] Permeable Pavement to receive the run-off from all of the new paved areas.

Permeable pavements provide a pavement suitable for pedestrian and/or vehicular traffic, while allowing rainwater to infiltrate through the surface and into the underlying structural layers, and also attenuates the rainwater beneath the overlying surface before infiltration. Permeable pavements are an efficient means of managing surface water runoff close to its source – intercepting runoff, reducing the volume and frequency of runoff, and providing a treatment medium. See attached plan drawing D-01 Rev E and details drawing D-02 Rev C for proposed extent and section of the permeable pavement.

#### 6.0 Stormwater Quantity Design;

6.1 The extreme storm event, 100year – 6hour storm, defines the stormwater volumes that are to be managed for at the new development. It is proposed to use two SUDS treatment trains to manage the stormwater run-off from the impermeable areas (roofs) of the new development. These treatment trains will attenuate all of the stormwater runoff from a 100year – 6 hr. storm event. These treatment trains will also maintain within the site curtilage 89% of the stormwater runoff from a 100year – 6 hr. storm event .

6.2 The attenuated runoff is stored for infiltration, with the estimated excess (2.8m<sup>3</sup>) released via the perforated riser flow control device to the existing stormwater outfall. This release rate 1.87L/sec/Ha is significantly less than the maximum allowable outfall rate (Qbar or the GDRCP rate 2L/sec/Ha); see attached calculation sheet, Appendix A.11.

#### 6.3 Storage Components of the Treatment Trains:

**Treatment Train AC**: Bio-Ret. Swale A + Bio-Ret. Rainwater Garden C (50%) **Treatment Train BC**: Bio-Ret. Swale B + Bio-Ret. Rainwater Garden C (50%)

#### **6.4 Attenuation Volume Design:**

(See Appendix A.6-A.10 attached calculation sheets):

Design Parameters:		Ref.
Max Run-off Rate:	3.8L/s/ha	See Q bar(rural) above
Storm Return Periods :	10yr.; 100yr.	
Storm Duration:	60 min.; <b>6 hour</b>	
Max Rainfall for Extreme		
Rainfall Return for Storm Periods:	20.9mm; <b>68mm</b>	MetEireann (Casement)
Impermeable area :	750m <sup>2</sup>	
Climate Change Factor :	20%	

#### 6.5 100 Year - 6Hr Storm: Runoff & Storage Quantities Recap:

100year – 6Hr Storm Recap	
Total Inflow (m <sup>3</sup> )	71.7
Less Treatment Train AC storage Volume (m <sup>3</sup> )	29.7
Less Treatment Train BC storage Volume (m <sup>3</sup> )	34.1
Less Infiltration during Storm Duration Volume (m <sup>3</sup> )	5.2
Net Excess inflow over Storage Capacity (m <sup>3</sup> )	2.7

See attached SUDS calculation sheet and Summary sheet for 10year and 100year storm events calculations, Appendix A.6-A.10.

19/10/23 Thrandot Signed: Date: Marty Wardick Chartered Engineer MSW

# **Appendix A**

- 1. Storm Drainage Layout Plan Drawing D-01 Rev E
- 2. Storm Drainage Details Drawing D-02 Rev C
- 3. Storm Drainage Long. Sections D-03 Rev A
- 4. Infiltration Rate Calculation Sheet
- 5. Mean Annual Flood Flow Calculation [Qbar(rural)]
- 6. SUDS Train A-C Calculation Sheet–10 Year 60min Storm
- 7. SUDS Train A-C Calculation Sheet–100 Year 6 Hr. Storm
- 8. SUDS Train B-C Calculation Sheet–10 Year 60min Storm
- 9. SUDS Train B-C Calculation Sheet–100 Year 6 Hr. Storm
- 10. Summary of SUDS Soakaway & Attenuation water volumes
- 11. Perforated Riser Flow Control Calculation Sheet

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Soil Infiltra	ation Rate Calculation:		<u></u>			
Project:	New Citywise Science & La	anguage	Centre			
Location:	Durkan Centre, Fortunstow	n Way, 1	Tallaght, Dub	lin 24.		
	Trial Pit					
	Dimensions:					
	Length (I) =	0.6 (		1st filling:		27-Jul-22
I	Width (w) =	0.875		2nd filling:		28-Jul-22
I	Hole Depth=	1.5 (		3rd filling:		29-Jul-22
I	Depth of water (d1) =	0.520 (		15.35	•	29-Jul-22
1		0.00		12.30		30-Jul-22
	Depth delta =	0.52 ו		[use 24hr c	lck]	
	Initial Volume of Water	+ + -				
	Final Volume of Water	0 1	m3			
	Soil Infiltration Rate (f) =	Vp(100-(	0) / Ap50 x tp	(100-0)		
	as per BRE 365					
	tp (100-0)					
	Time delta =	1257 i	minutes	20.95	hrs	
		75420 :	secs			
1						
I	Vp(100-0)	0.273 1	m3		50% percolation	on in 24hrs test
I	Volume delta				drop in volume	of water in 24 hours
				100.00%		
				OK percola	ition voumne gro	eater than 50% in24hrs
	Ap50=	1.292	m2			
	Ap50= [(I+w) x2 x delta d] +	F [l x w]				
1	Soil Inflitration Rate (f) =		2.80E-06			
			0.01008593	m/hr		
	Safety Factor (1.5 - 10)		2.5		Ref SUDS Man	ual C697 4-30
	Adjusted Soil Infitration R	tate (q)	1.1207E-06			
			0.00403437	m/hr		

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Project:	<ul> <li>Citywise, Fortunestown Lane</li> </ul>	1		
			0.5 km <sup>2</sup>	50 ha
Catchment	Area =	1940 m <sup>2</sup>	0.00194 km <sup>2</sup>	0.194 Ha
Standard Ar	ea Average Rainfall (SAAR) =	822 mm	Citywise, Tallaght	Ref. Met Eireann
	Soil Type 1 ≍	0 %		
	Soll Type 2 =	10 %		
	Soil Type 3 =	60 %		
	Soil Type 4 =	30 %		
	Soil Type 5 =	0 %		
	Total =	100 %		
SPR (Soil	Index: Per-centage Run-off)	0.387		
		011] + 0.3 [Soil2] + 0.3 18 x (AREA) <sup>0.89</sup> x SAA	7 [Soil3] + 0.47 [Soil4] + R <sup>1.17</sup> x SPR <sup>2.17</sup>	0.53 [Soil5]
an Annual I	Q <sub>bar</sub> = 0.0010	98 x (AREA) <sup>0.89</sup> x SAA		0.53 [Soil5]
		98 x (AREA) <sup>0.89</sup> x SAA	R <sup>1.17</sup> x SPR <sup>2.17</sup> for Area = 50Ha	0.53 [Soil5] C753 The Suds Manual
Greenfield Q <sub>t</sub>	Q <sub>bar</sub> = 0.0010	<b>191.1</b> <b>191.1</b> <b>0.1911</b> m <sup>3</sup> /sec res/sec =	R <sup>1.17</sup> x SPR <sup>2.17</sup> for Area = 50Ha	C753 The Suds Manual
Greenfield Q <sub>b</sub> Q <sub>bar</sub>	Q <sub>bar</sub> = 0.0010 Flood Flow Rate (Q <sub>ber(rural</sub> )) ≕ Peak Run-off <sub>er(rural)</sub> for 50 Ha = 191.1 lit	191.1 litres/sec 0.1911 m <sup>3</sup> /sec res/sec = tres/sec	R <sup>1.17</sup> x SPR <sup>2.17</sup> for Area = 50Ha Ref. Eqn. 24.3 Ciria 3.8 litres/se	C753 The Suds Manual
Greenfield Q <sub>b</sub> Q <sub>bari</sub> This is the	Q <sub>bar</sub> = 0.0010 Flood Flow Rate (Q <sub>bar(rural)</sub> ) = Peak Run-off er(rural) for 50 Ha = 191.1 lit (rural) for .194 Ha = 0.74 lit	191.1 litres/sec 0.1911 m <sup>3</sup> /sec res/sec = tres/sec	R <sup>1.17</sup> x SPR <sup>2.17</sup> for Area = 50Ha Ref. Eqn. 24.3 Ciria 3.8 litres/se	C753 The Suds Manual
Greenfield Q <sub>b</sub> Q <sub>bar</sub>	Q <sub>bar</sub> = 0.0010 Flood Flow Rate (Q <sub>bar(rural)</sub> ) = Peak Run-off ar(rural) for 50 Ha = 191.1 lit (rural) for .194 Ha = 0.74 lit Maximum Allowable Discharg Area of Catchment (km <sup>2</sup> ) Standard Area Average Rain	98 x (AREA) <sup>0.69</sup> x SAA 191.1 litres/sec 0.1911 m <sup>3</sup> /sec res/sec = tres/sec e from the Developm fall (mm)	R <sup>1.17</sup> x SPR <sup>2.17</sup> for Area = 50Ha Ref. Eqn. 24.3 Ciria 3.8 litres/se	C753 The Suds Manual
Greenfield Q <sub>b</sub> Q <sub>bar</sub> This is the Area =	Q <sub>bar</sub> = 0.0010 Flood Flow Rate (Q <sub>bar(rural)</sub> ) = Peak Run-off er(rural) for 50 Ha = 191.1 lit (rural) for .194 Ha = 0.74 lit Maximum Allowable Discharg Area of Catchment (km <sup>2</sup> )	98 x (AREA) <sup>0.69</sup> x SAA 191.1 litres/sec 0.1911 m <sup>3</sup> /sec res/sec = tres/sec e from the Developm fall (mm)	R <sup>1.17</sup> x SPR <sup>2.17</sup> for Area = 50Ha Ref. Eqn. 24.3 Ciria 3.8 litres/se	C753 The Suds Manual

#### 26/10/2023

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Project: New Citywise Scienc Location: Durkan Centre, Fortu		ght, Dublin 24.				
Total Area of Site	1940 m2		SUDS CHAIN	A-C (See Section	A-C)	
Area Data:	Area			Impermeability [%]	Effective Area In	21
Impermeable area	750 m2	New Roof	Area	50%		375 m2
				0070		010 1112
Partial permable area	31 m2	Swale A pl	20.0002	100%		31 m2
Other: Landscaped, green roof	26 m2		an area (50%)			26 m2
	807 m2	onbio o pi		00 /0		
			Eff. Area	drained to Soakway		518 m2
					incl 20% CCA	
Return Period Rainfall Depths [R	ef. Met Eireann)					
Location: Casement Aerodrom	e Dublin					
i0 year Return Period - 60 min d	luration		20.9	mm		
Sector Deletell 2040 controls						
Design Rainfall (R10-60MIN): 10 year storm - 60 min duratior						
	····		10.8	3	Inflow	
nflow to Soakway [A x R10-60]:	•		10.8	118	IT BLOW	
SUDS MEASURE #1						
Proposed Infiltration Structure -	Dims: BIO-RE	T. SWALE #A				
Area	31.25 m2					
Perimeter	31 m					
Depth of filter layer 1:	0.45 m	STONE	Infiltration			
Depth of filter layer 2:		CELLS	Infiltration	Length of Cells		11 m
Dept of Retained water	0.15 m	Attenuation	n	Width of Cells		1 m
Total Volume of Soakway	18.46 m <sup>3</sup>			30%		
Net Volume of Soakway	8.40 m <sup>3</sup>	Free volum	18 %	95%		
				(95% for 'Aquacell	s; 30% for stone)	
Attenuation Surface Storage	4.69 m <sup>3</sup>			95% for Aquacell	s"; 30% for stonej	
Attenuation Surface Storage	4.69 m <sup>3</sup>			(95% for 'Aquacell	s"; 30% for stonej	
Attenuation Surface Storage Outflow from Soakaways during			BIO-RET. SV		s'; 30% for stonej	
Outflow from Soakaways during	storm (O) O=As5(	Internal su Calculated	rface area of S Adjusted Infill	VALE		
Outflow from Soakaways during As50=	storm (O) O=As5( 44.43 m2	Internal su	rface area of S Adjusted Infill	VALE Swale to 50% effecti		
Outflow from Soakaways during s As50= f= D=	storm (O) O=As5( 44.43 m2 1.12E-06 m/s 3600 secs	Internal su Calculated	rface area of S Adjusted Infill	VALE Swale to 50% effecti		
Outflow from Soakaways during As50≈ f=	storm (O) O=As50 44.43 m2 1.12E-06 m/s	Internal su Calculated	rface area of S Adjusted Infill	VALE Swale to 50% effecti		
Outflow from Soakaways during s As50= f= D= Outflow =	storm (O) O=As5( 44.43 m2 1.12E-06 m/s 3600 secs	Internal su Calculated	rface area of S Adjusted Infill	VALE Swale to 50% effecti		
Outflow from Soakaways during s As50= f= D= Outflow = SUDS MEASURE #2	storm (O) O=As5( 44.43 m2 1.12E-06 m/s 3600 secs 0.31 m <sup>3</sup>	Internal su Calculated	rface area of 5 Adjusted Infili f storm	VALE Swale to 50% effecti	ve depth	
Outflow from Soakaways during s As50= f= D= Outflow = SUDS MEASURE #2	storm (O) O=As5( 44.43 m2 1.12E-06 m/s 3600 secs 0.31 m <sup>3</sup>	Internal su Calculated Duration of	rface area of 5 Adjusted Infili f storm	VALE Swale to 50% effecti		
Outflow from Soakaways during : As50= f= D= Outflow = SUDS MEASURE #2 Proposed Infiltration Structure -	storm (O) O=As50 44.43 m2 1.12E-06 m/s 3600 secs 0.31 m <sup>3</sup> Dims: BIO-RE	Internal su Calculated Duration of	rface area of 5 Adjusted Infili f storm	VALE Swale to 50% effecti	ve depth	
Dutflow from Soakaways during : As50= f= D= Outflow = SUDS MEASURE #2 Proposed Infiltration Structure - Area	storm (O) O=As50 44.43 m2 1.12E-06 m/s 3600 secs 0.31 m <sup>3</sup> Dims: BIO-RE 26 m2 15 m	Internal su Calculated Duration of	rface area of 5 Adjusted Infili f storm	VALE Swale to 50% effecti	ve depth	
Dutflow from Soakaways during : As50= f= D= Outflow = SUDS MEASURE #2 Proposed Infiltration Structure - Area Perimeter	storm (O) O=As50 44.43 m2 1.12E-06 m/s 3600 secs 0.31 m <sup>3</sup> Dims: BIO-RE 26 m2 15 m 0.35 m	Internal su Calculated Duration of	rface area of 5 Adjusted Infili f storm R GRDN #C	VALE Swale to 50% effecti	ve depth	
Dutflow from Soakaways during : As50= f= D= Outflow = SUDS MEASURE #2 Proposed Infiltration Structure - Area Perimeter Depth of filter layer 1:	storm (O) O=As50 44.43 m2 1.12E-06 m/s 3600 secs 0.31 m <sup>3</sup> Dims: BIO-RE 26 m2 15 m 0.35 m 0.4 m	Internal su Calculated Duration of ET. RAINWATE STONE	rface area of \$ Adjusted Infili f storm R GRDN #C	VALE Swale to 50% effecti	ve depth	
Dutflow from Soakaways during a As50= f= D= Outflow = SUDS MEASURE #2 Proposed Infiltration Structure - Area Perimeter Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water	storm (O) O=As5( 44.43 m2 1.12E-06 m/s 3600 secs 0.31 m <sup>3</sup> Dims: BIO-RE 26 m2 15 m 0.35 m 0.4 m 0.15 m	Internal su Calculated Duration of ET. RAINWATE STONE	rface area of \$ Adjusted Infili f storm <b>R GRDN #C</b> Infiltration Infiltration	VALE Swale to 50% effecti ration Rate (FOS)	ve depth	
Dutflow from Soakaways during a As50= f= D= Outflow = SUDS MEASURE #2 Proposed Infiltration Structure - Area Perimeter Depth of filter layer 1: Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water	storm (O) O=As50 44.43 m2 1.12E-06 m/s 3600 secs 0.31 m <sup>3</sup> Dims: BIO-RE 26 m2 15 m 0.35 m 0.4 m 0.15 m 19.13 m <sup>3</sup>	Internal su Calculated Duration of ET. RAINWATE STONE CELLS	rface area of \$ Adjusted Infili f storm <b>R GRDN #C</b> Infiltration Infiltration Attenuation	VALE Swale to 50% effecti ration Rate (FOS)	ve depth 50% STONE	
Dutflow from Soakaways during a As50= f= D= Outflow = SUDS MEASURE #2 Proposed Infiltration Structure - Area Perimeter Depth of filter layer 1: Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water	storm (O) O=As5( 44.43 m2 1.12E-06 m/s 3600 secs 0.31 m <sup>3</sup> Dims: BIO-RE 26 m2 15 m 0.35 m 0.4 m 0.15 m	Internal su Calculated Duration of ET. RAINWATE STONE	rface area of \$ Adjusted Infili f storm <b>R GRDN #C</b> Infiltration Infiltration Attenuation	VALE Swale to 50% effecti ration Rate (FOS) 30% 95%	ve depth 50% STONE CELLS	
Outflow from Soakaways during a As50= f= D= Outflow = SUDS MEASURE #2 Proposed Infiltration Structure - Area Perlmeter Depth of filter layer 1: Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water Total Volume of Soakway	storm (O) O=As50 44.43 m2 1.12E-06 m/s 3600 secs 0.31 m <sup>3</sup> Dims: BIO-RE 26 m2 15 m 0.35 m 0.4 m 0.15 m 19.13 m <sup>3</sup>	Internal su Calculated Duration of ET. RAINWATE STONE CELLS	rface area of \$ Adjusted Infili f storm <b>R GRDN #C</b> Infiltration Infiltration Attenuation	VALE Swale to 50% effecti ration Rate (FOS)	ve depth 50% STONE CELLS	
Outflow from Soakaways during : As50= f= D= Outflow = SUDS MEASURE #2 Proposed Infiltration Structure - Area Perimeter Depth of filter layer 1: Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water Total Volume of Soakway Net Volume of Soakway	storm (O) O=As50 44.43 m2 1.12E-06 m/s 3600 secs 0.31 m <sup>3</sup> Dims: BIO-RE 26 m2 15 m 0.35 m 0.4 m 0.15 m 19.13 m <sup>3</sup> 12.37 m <sup>3</sup>	Internal su Calculated Duration of ET. RAINWATE STONE CELLS	rface area of \$ Adjusted Infili f storm <b>R GRDN #C</b> Infiltration Infiltration Attenuation	VALE Swale to 50% effecti ration Rate (FOS) 30% 95%	ve depth 50% STONE CELLS	
Outflow from Soakaways during : As50= f= D= Outflow = SUDS MEASURE #2 Proposed Infiltration Structure - Area Perimeter Depth of filter layer 1: Depth of filter layer 2:	storm (O) O=As50 44.43 m2 1.12E-06 m/s 3600 secs 0.31 m <sup>3</sup> Dims: BIO-RE 26 m2 15 m 0.35 m 0.4 m 0.15 m 19.13 m <sup>3</sup>	Internal su Calculated Duration of ET. RAINWATE STONE CELLS	rface area of \$ Adjusted Infili f storm <b>R GRDN #C</b> Infiltration Infiltration Attenuation	VALE Swale to 50% effecti ration Rate (FOS) 30% 95%	ve depth 50% STONE CELLS	
Outflow from Soakaways during : As50= f= D= Outflow = SUDS MEASURE #2 Proposed Infiltration Structure - Area Perimeter Depth of filter layer 1: Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water Total Volume of Soakway Net Volume of Soakway Attenuation Surface Storage	storm (O) O=As50 44.43 m2 1.12E-06 m/s 3600 secs 0.31 m <sup>3</sup> Dims: BIO-RE 26 m2 15 m 0.35 m 0.4 m 0.15 m 19.13 m <sup>3</sup> 12.37 m <sup>3</sup>	Internal su Calculated Duration of ET. RAINWATE STONE CELLS Free volum	rface area of \$ Adjusted Infili f storm <b>ER GRDN #C</b> Infiltration Infiltration Attenuation	VALE Swale to 50% effecti ration Rate (FOS) 30% 95%	ve depth 50% STONE CELLS s'; 30% for stone}	
Outflow from Soakaways during s As50= f= D= Outflow = SUDS MEASURE #2 Proposed Infiltration Structure - Area Perimeter Depth of filter layer 1: Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water Total Volume of Soakway Net Volume of Soakway	storm (O) O=As50 44.43 m2 1.12E-06 m/s 3600 secs 0.31 m <sup>3</sup> Dims: BIO-RE 26 m2 15 m 0.35 m 0.4 m 0.15 m 19.13 m <sup>3</sup> 12.37 m <sup>3</sup>	Internal su Calculated Duration of ET. RAINWATE STONE CELLS Free volum	rface area of \$ Adjusted Infilit f storm <b>R GRDN #C</b> Infiltration Infiltration Attenuation ne % BIO-RET. RA	VALE Swale to 50% effecti ration Rate (FOS) 30% 95% [95% for 'Aquaceti	ve depth 50% STONE CELLS s'; 30% for stone}	
Dutflow from Soakaways during s As50= f= D= Outflow = SUDS MEASURE #2 Proposed Infiltration Structure - Area Perimeter Depth of filter layer 1: Depth of filter layer 1: Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water Fotal Volume of Soakway Net Volume of Soakway Net Volume of Soakway	storm (O) O=As50 44.43 m2 1.12E-06 m/s 3600 secs 0.31 m <sup>3</sup> Dims: BIO-RE 26 m2 15 m 0.35 m 0.4 m 0.15 m 19.13 m <sup>3</sup> 12.37 m <sup>3</sup> 3.825 m <sup>3</sup> storm (O) O=As50	Internal su Calculated Duration of ET. RAINWATE STONE CELLS Free volum	rface area of \$ Adjusted Infilit f storm <b>R GRDN #C</b> Infiltration Infiltration Attenuation ne % BIO-RET. RA	VALE Swale to 50% effecti ration Rate (FOS) 30% 95% [95% for 'Aquacell	ve depth 50% STONE CELLS s'; 30% for stone}	
Dutflow from Soakaways during s As50= f= D= Outflow = SUDS MEASURE #2 Proposed Infiltration Structure - Area Perimeter Depth of filter layer 1: Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water Total Volume of Soakway Net Volume of Soakway Net Volume of Soakway Net Volume of Soakway Net Volume of Soakway Dutflow from Soakaways during s As50=	storm (O) O=As50 44.43 m2 1.12E-06 m/s 3600 secs 0.31 m <sup>3</sup> Dims: BIO-RE 26 m2 15 m 0.35 m 0.4 m 0.15 m 19.13 m <sup>3</sup> 12.37 m <sup>3</sup> 3.825 m <sup>3</sup> storm (O) O=As50 31.13 m2	Internal su Calculated Duration of ET. RAINWATE STONE CELLS Free volum	rface area of \$ Adjusted Infilit f storm <b>R GRDN #C</b> Infiltration Infiltration Attenuation ne % <b>BIO-RET. RA</b> rface area (ex Adjusted Infil	VALE Swale to 50% effecti ration Rate (FOS) 30% 95% [95% for 'Aquacell NINWATER GRDN f cl. base area) of soc	ve depth 50% STONE CELLS s'; 30% for stone}	
Dutflow from Soakaways during : As50= f= D= Outflow = SUDS MEASURE #2 Proposed Infiltration Structure - Area Perimeter Depth of filter layer 1: Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water Total Volume of Soakway Net Volume of Soakway Net Volume of Soakway Net Volume of Soakway Net Volume of Soakway Outflow from Soakaways during : As50= f= D=	storm (O) O=As50 44.43 m2 1.12E-06 m/s 3600 secs 0.31 m <sup>3</sup> Dims: BIO-RE 26 m2 15 m 0.35 m 0.4 m 0.15 m 19.13 m <sup>3</sup> 12.37 m <sup>3</sup> 3.825 m <sup>3</sup> storm (O) O=As50 31.13 m2 1.12E-06 m/s 3600 secs	Internal su Calculated Duration of ET. RAINWATE STONE CELLS Free volum D x f x D Internal su Calculated	rface area of \$ Adjusted Infilit f storm <b>R GRDN #C</b> Infiltration Infiltration Attenuation ne % <b>BIO-RET. RA</b> rface area (ex Adjusted Infil	VALE Swale to 50% effecti ration Rate (FOS) 30% 95% [95% for 'Aquacell NINWATER GRDN f cl. base area) of soc	ve depth 50% STONE CELLS s'; 30% for stone}	
Outflow from Soakaways during s As50= f= D= Outflow = SUDS MEASURE #2 Proposed Infiltration Structure - Area Perimeter Depth of filter layer 1: Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water Total Volume of Soakway Net Volume of Soakway Net Volume of Soakway Net Volume of Soakway Outflow from Soakaways during s As50= f=	storm (O) O=As50 44.43 m2 1.12E-06 m/s 3600 secs 0.31 m <sup>3</sup> Dims: BIO-RE 26 m2 15 m 0.35 m 0.4 m 0.15 m 19.13 m <sup>3</sup> 12.37 m <sup>3</sup> 3.825 m <sup>3</sup> storm (O) O=As50 31.13 m2 1.12E-06 m/s	Internal su Calculated Duration of ET. RAINWATE STONE CELLS Free volum D x f x D Internal su Calculated	rface area of \$ Adjusted Infilit f storm <b>R GRDN #C</b> Infiltration Infiltration Attenuation ne % <b>BIO-RET. RA</b> rface area (ex Adjusted Infil	VALE Swale to 50% effecti ration Rate (FOS) 30% 95% [95% for 'Aquacell NINWATER GRDN f cl. base area) of soc	ve depth 50% STONE CELLS s'; 30% for stone}	
Outflow from Soakaways during : As50= f= D= Outflow = SUDS MEASURE #2 Proposed Infiltration Structure - Area Perlmater Depth of filter layer 1: Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water Total Volume of Soakway Net Volume of Soakway Net Volume of Soakway Net Volume of Soakway Attenuation Surface Storage Outflow from Soakaways during : As50= f= D= Outflow =	storm (O) O=As50 44.43 m2 1.12E-06 m/s 3600 secs 0.31 m <sup>3</sup> Dims: BIO-RE 26 m2 15 m 0.35 m 0.4 m 0.15 m 19.13 m <sup>3</sup> 12.37 m <sup>3</sup> 3.825 m <sup>3</sup> storm (O) O=As50 31.13 m2 1.12E-06 m/s 3600 secs 0.13 m <sup>3</sup>	Internal su Calculated Duration of ET. RAINWATE STONE CELLS Free volum STONE CELLS	rface area of \$ Adjusted Infilit f storm <b>R GRDN #C</b> Infiltration Infiltration Attenuation Me % BIO-RET. RA Inface area (ex I Adjusted Infilit f storm	VALE Swale to 50% effecti ration Rate (FOS) 30% 95% [95% for 'Aquacell NNWATER GRDN for the cl. base area) of sor tration Rate (FOS)	ve depth 50% STONE CELLS s'; 30% for stone} #C akway to 50% eff.	depth
Outflow from Soakaways during : As50= f= D= Outflow = SUDS MEASURE #2 Proposed Infiltration Structure - Area Perimeter Depth of filter layer 1: Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water Total Volume of Soakway Net Volume of Soakway Net Volume of Soakway Net Volume of Soakway Net Volume of Soakway Outflow from Soakaways during : As50= f= D=	storm (O) O=As50 44.43 m2 1.12E-06 m/s 3600 secs 0.31 m <sup>3</sup> Dims: BIO-RE 26 m2 15 m 0.35 m 0.4 m 0.15 m 19.13 m <sup>3</sup> 12.37 m <sup>3</sup> 3.825 m <sup>3</sup> storm (O) O=As50 31.13 m2 1.12E-06 m/s 3600 secs 0.13 m <sup>3</sup>	Internal su Calculated Duration of ET. RAINWATE STONE CELLS Free volum D x f x D Internal su Calculated	rface area of \$ Adjusted Infilit f storm <b>R GRDN #C</b> Infiltration Infiltration Attenuation ne % <b>BIO-RET. RA</b> rface area (ex Adjusted Infil	VALE Swale to 50% effecti ration Rate (FOS) 30% 95% [95% for 'Aquacell NNWATER GRDN for the cl. base area) of sor tration Rate (FOS)	ve depth 50% STONE CELLS s'; 30% for stone}	depth
Outflow from Soakaways during s As50= f= D= Outflow = SUDS MEASURE #2 Proposed Infiltration Structure - Area Perlmater Depth of filter layer 1: Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water Total Volume of Soakway Net Volume of Soakway Net Volume of Soakway Attenuation Surface Storage Outflow from Soakaways during s As50= f= D= Outflow = Inflow - Outflow = Storage	storm (O) O=As50 44.43 m2 1.12E-06 m/s 3600 secs 0.31 m <sup>3</sup> Dims: BIO-RE 26 m2 15 m 0.35 m 0.4 m 0.15 m 19.13 m <sup>3</sup> 12.37 m <sup>3</sup> 3.825 m <sup>3</sup> storm (O) O=As50 31.13 m2 1.12E-06 m/s 3600 secs 0.13 m <sup>3</sup> orage Required	Internal su Calculated Duration of ET. RAINWATE STONE CELLS Free volum STONE CELLS 0 x f x D Internal su Calculated Duration o	rface area of \$ Adjusted Infilit f storm <b>R GRDN #C</b> Infiltration Infiltration Attenuation Attenuation ne % BIO-RET. RA rface area (ex Adjusted Infilit f storm	VALE Swale to 50% effecti ration Rate (FOS) 30% 95% [95% for 'Aquacell NNWATER GRDN # cl. base area) of so tration Rate (FOS)	ve depth 50% STONE CELLS s'; 30% for stone} #C akway to 50% eff.	depth
Dutflow from Soakaways during : As50= f= D= D= D= D= D= SUDS MEASURE #2 Proposed Infiltration Structure - Area Perimeter Depth of filter layer 1: Depth of filter layer 1: Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water Total Volume of Soakway Net Volume of Soakway Net Volume of Soakway Attenuation Surface Storage Dutflow from Soakaways during : As50= f= D= D= D= Inflow - Outflow = Storage	storm (O) O=As50 44.43 m2 1.12E-06 m/s 3600 secs 0.31 m <sup>3</sup> Dims: BIO-RE 26 m2 15 m 0.35 m 0.4 m 0.15 m 19.13 m <sup>3</sup> 12.37 m <sup>3</sup> 3.825 m <sup>3</sup> storm (O) O=As50 31.13 m2 1.12E-06 m/s 3600 secs 0.13 m <sup>3</sup> orage Required (50%) Filter Layer	Internal su Calculated Duration of ET. RAINWATE STONE CELLS Free volum 0 x f x D Internal su Calculated Duration o [I-O=S] Storage Vol =	rface area of S Adjusted Infili f storm R GRDN #C Infiltration Infiltration Attenuation Attenuation ne % BIO-RET. RA rface area (ex I Adjusted Infili f storm 10.44	VALE Swale to 50% effecti ration Rate (FOS) 30% 95% [95% for 'Aquacell NNWATER GRDN so tration Rate (FOS) 0 m <sup>3</sup>	ve depth 50% STONE CELLS s'; 30% for stone} #C akway to 50% eff.	depth
Outflow from Soakaways during s As50= f= D= Outflow = SUDS MEASURE #2 Proposed Infiltration Structure - Area Perlmater Depth of filter layer 1: Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water Total Volume of Soakway Net Volume of Soakway Net Volume of Soakway Attenuation Surface Storage Outflow from Soakaways during s As50= f= D= Outflow = Inflow - Outflow = Storage	storm (O) O=As50 44.43 m2 1.12E-06 m/s 3600 secs 0.31 m <sup>3</sup> Dims: BIO-RE 26 m2 15 m 0.35 m 0.4 m 0.15 m 19.13 m <sup>3</sup> 12.37 m <sup>3</sup> 3.825 m <sup>3</sup> storm (O) O=As50 31.13 m2 1.12E-06 m/s 3600 secs 0.13 m <sup>3</sup> orage Required (50%) Filter Layer	Internal su Calculated Duration of ET. RAINWATE STONE CELLS Free volum 0 x f x D Internal su Calculated Duration o [I-O=S] Storage Vol =	rface area of S Adjusted Infili f storm R GRDN #C Infiltration Infiltration Attenuation Attenuation ne % BIO-RET. RA rface area (ex Adjusted Infili f storm 10.40	VALE Swale to 50% effecti ration Rate (FOS) 30% 95% [95% for 'Aquacell NNWATER GRDN # cl. base area) of sor tration Rate (FOS) m <sup>3</sup> a m <sup>3</sup> a m <sup>3</sup>	ve depth 50% STONE CELLS s'; 30% for stone} s'; 30% for stone}	depth ed
Outflow from Soakaways during : As50= f= D= Outflow = SUDS MEASURE #2 Proposed Infiltration Structure - Area Perlmeter Depth of filter layer 1: Depth of filter layer 1: Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water Total Volume of Soakway Net Volume of Soakway Attenuation Surface Storage Outflow from Soakaways during : As50= f= D= Outflow = Inflow - Outflow = Storage	storm (O) O=As50 44.43 m2 1.12E-06 m/s 3600 secs 0.31 m <sup>3</sup> Dims: BIO-RE 26 m2 15 m 0.35 m 0.4 m 0.15 m 19.13 m <sup>3</sup> 12.37 m <sup>3</sup> 3.825 m <sup>3</sup> storm (O) O=As50 31.13 m2 1.12E-06 m/s 3600 secs 0.13 m <sup>3</sup> orage Required (50%) Filter Layer	Internal su Calculated Duration of ET. RAINWATE STONE CELLS Free volum 0 x f x D Internal su Calculated Duration o [I-O=S] Storage Vol =	rface area of S Adjusted Infili f storm R GRDN #C Infiltration Infiltration Attenuation Attenuation ne % BIO-RET. RA rface area (ex I Adjusted Infili f storm 10.44	VALE Swale to 50% effecti ration Rate (FOS) 30% 95% [95% for 'Aquacell NNWATER GRDN for tration Rate (FOS) m <sup>3</sup> m <sup>3</sup> m <sup>3</sup> m <sup>3</sup> m <sup>3</sup>	ve depth 50% STONE CELLS s'; 30% for stone} #C akway to 50% eff.	depth ed

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Project: New Citywise Science Location: Durken Centre, Fortu	e & Language Centre Instown Way, Tallagh			
Total Area of Site	1940 m2	SUDS CH/	AIN A-C ( See Section	A-C)
<u>Area Data:</u> Impermeable area	Area 750 m2	New Roof Area	Impermeability [%] 50%	Effective Area (m2) 375 m2
Partial permable area Other: Landscaped, green roof	31 m2 26 m2 807 m2	Swale A plan area Swale C plan area (50 Eff. Are	%) 100% %) 50%	<u>26</u> m2
Return Period Rainfall Depths (F Location: Casement Aerodrom 100 year Return Period - 6hr d	e Dublin		68 mm	incl 20% CCA
Design Rainfall [R100-6HR]; 100 year storm - 6hr duration: Inflow to Soakway [A x R10-60];		3	5.2 m <sup>3</sup>	Inflow
SUDS MEASURE #1 Proposed Infiltration Structure - Area Perimeter	31.25 m2 31 m	SWALE #A		
Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water	0.45 m 0.40 m 0.15 m	STONE Infiltration CELLS Infiltration Surface Attenuation	Length of Cells Width of Cells	
Total Volume of Soakway Net Volume of Soakway	18.86 m <sup>3</sup> 8.78 m <sup>3</sup>	Free volume %	30% 95% [95% for 'Aquacell	CELLS
Attenuation Surface Storage Outflow from Soakaways during As50= f= D=	4.69 m <sup>3</sup> storm (O) O=As50 x 44.43 m2 1.12E-06 m/s 21600 secs	f x D BIO-RET. Internal surface area o Calculated Adjusted In Duration of storm	of Swale to 50% effecti	ve depth
Outflow = SUDS MEASURE #2 Proposed Infiltration Structure -	1.08 m <sup>3</sup> Dims: BIO-RET	RAINWATER GRDN #4	C 50%	1
Area Perimeter Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water	0.4 m	STONE Infiltration CELLS Infiltration Attenuation	n	
Total Volume of Soakway Net Volume of Soakway	19.13 m <sup>3</sup> 12.37 m <sup>3</sup>	Free volume %	30% 95% [95% for 'Aquacell	CELLS
Attenuation Surface Storage	3.825 m <sup>3</sup>	]		
Outflow from Soakaways during As50= f= D=	storm (O) O=As50 × 31.13 m2 1.12E-06 m/s 21600 secs	f x D BIO-RET. Internal surface area Calculated Adjusted Ir Duration of storm		
Outflow =	0.75 m <sup>3</sup>			
Inflow - Outflow = St	orage Required	[I+O=S] 33	.40 m <sup>3</sup>	Storage Required
Total Swale #A & RWG #C Total Swale #A & RWG			1.1 m <sup>3</sup> 8.5 m <sup>3</sup>	
		3	.74 m <sup>3</sup>	Storage available Storage Deficit
	Attenuation volume	exceeded		E PART SHOW

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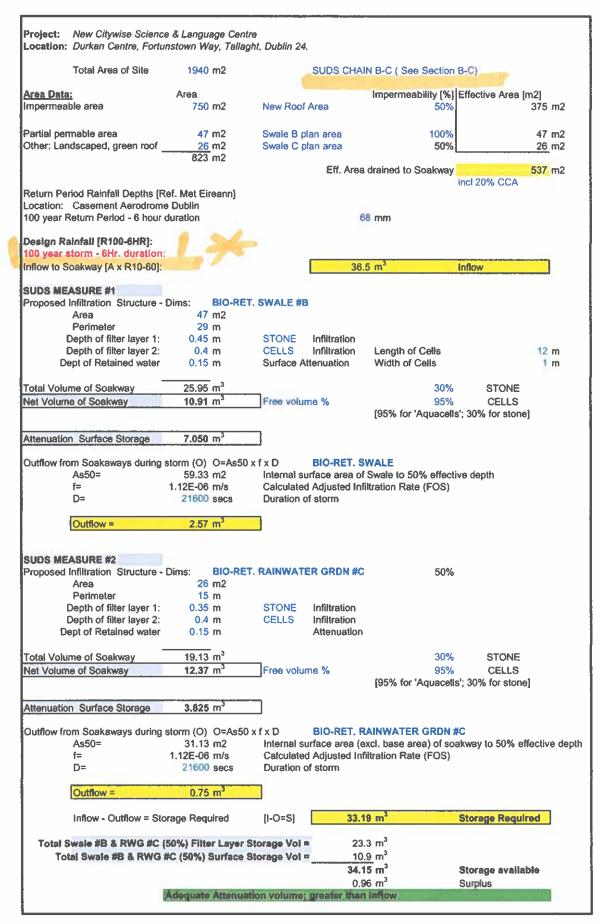
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Project: New Citywise Science					
Location: Durkan Centre, Fort	unstown Way, Tall	aght, Dublin 24.			
Total Area of Site	1940 m2		SUDS CHAIN	B-C (See Section B-C)	
Area Data:	Area			Impermeability [%] Effect	tive Area [m2]
Impermeable area	750 m2	New Roof	Area	50%	375 m2
Destal accordence -	17 0	A	lan aver	1000	-
Partial permable area Other: Landscaped, green roof	47 m2 26 m2	Swale B p Swale C p	lan area lan area (50%)	100% 50%	47 m2 26 m2
	823 m2				
			Eff. Area	drained to Soakway	537 m2
Return Period Rainfall Depths [F	Ref. Met Eireann)			inça 2	078 CCA
Location: Casement Aerodrom			20.0	S	
10 year Return Period - 60 min	duration		20.8	mm	
Design Rainfall [R10-60MIN]:					
10 year storm - 60 min duration Inflow to Soakway (A x R10-60):			11.2	en al anti-	
Tillow to Soakway [A X K TO-OO].			11.4	! m <sup>3</sup> Inflov	v
SUDS MEASURE #1	Dis				
Proposed Infiltration Structure - Area	Dims: BIO-R 47 m2	RET, SWALE #8			
Perimeter	29 m				
Depth of filter layer 1: Depth of filter layer 2:		STONE CELLS	Infiltration	Length of Cells	11 m
Dept of Retained water		OLLIS	Attenuation	Width of Cells	1 m
Total Volume of Soakway Net Volume of Soakway	25.55 m <sup>3</sup> 10.525 m <sup>3</sup>	Free volur	mo %	30% 95%	STONE
	10.525 111		110 /0	[95% for 'Aquacells'; 30%	
Attenuation Surface Storage	7.050 m <sup>3</sup>				
Outflow from Soakaways during			BIO-RET. SV		
As50= f=	59.33 m2 1.12E-06 m/s			Swale to 50% effective de Iration Rate (FOS)	pth
D=	3600 secs	Duration of			
Outflow =	0.43 m <sup>3</sup>				
Country -	0.45 10				
SUDS MEASURE #2					
Proposed Infiltration Structure - Area	DIO 0		50 000N #0	500/	
		RET. RAINWATE	ER GRDN #C	50%	
Perimeter	- Dims: 810-R 26 m2 15 m	IET. RAINWATI	ER GRDN #C	50%	
Depth of filter layer 1:	26 m2 15 m : 0.35 m	STONE	Infiltration	50%	
	26 m2 15 m : 0.35 m : 0.4 m			50%	
Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water	26 m2 15 m 0.35 m 0.4 m 0.15 m	STONE	Infiltration Infiltration		
Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water Total Volume of Soakway	26 m2 15 m 0.35 m 0.4 m 0.15 m 19.13 m <sup>3</sup>	STONE CELLS	Infiltration Infiltration Attenuation	30%	STONE
Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water Total Volume of Soakway	26 m2 15 m 0.35 m 0.4 m 0.15 m	STONE	Infiltration Infiltration Attenuation		CELLS
Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water Total Volume of Soakway Net Volume of Soakway	26 m2 15 m 0.35 m 0.4 m 0.15 m 19.13 m <sup>3</sup> 12.37 m <sup>3</sup>	STONE CELLS	Infiltration Infiltration Attenuation	30% 95%	CELLS
Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water Total Volume of Soakway Net Volume of Soakway	26 m2 15 m 0.35 m 0.4 m 0.15 m 19.13 m <sup>3</sup>	STONE CELLS	Infiltration Infiltration Attenuation	30% 95%	CELLS
Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water Total Volume of Soakway Net Volume of Soakway Attenuation Surface Storage Outflow from Soakaways during	26 m2 15 m 0.35 m 0.4 m 0.15 m 19.13 m <sup>3</sup> 12.37 m <sup>3</sup> 3.825 m <sup>3</sup> storm (O) O=As:	STONE CELLS Free volur 50 x f x D	Infiltration Infiltration Attenuation me % BIO-RET. R/	30% 95% (95% for 'Aquacells'; 309 NINWATER GRDN #C	CELLS % for stone]
Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water Total Volume of Soakway Net Volume of Soakway Attenuation Surface Storage Outflow from Soakaways during As50=	26 m2 15 m 0.35 m 0.4 m 0.15 m 19.13 m <sup>3</sup> 12.37 m <sup>3</sup> 3.825 m <sup>3</sup> storm (O) O=As: 31.13 m2	STONE CELLS Free volur 50 x f x D Internal su	Infiltration Infiltration Attenuation me % BIO-RET. R/ urface area (ex	30% 95% (95% for 'Aquacelis'; 309 AINWATER GRDN #C cl. base area) of soakway	CELLS % for stone]
Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water Total Volume of Soakway Net Volume of Soakway Attenuation Surface Storage Outflow from Soakaways during	26 m2 15 m 0.35 m 0.4 m 0.15 m 19.13 m <sup>3</sup> 12.37 m <sup>3</sup> 3.825 m <sup>3</sup> storm (O) O=As:	STONE CELLS Free volur 50 x f x D Internal su	Infiltration Infiltration Attenuation me % BIO-RET. R/ urface area (ex d Adjusted Infil	30% 95% (95% for 'Aquacells'; 309 NINWATER GRDN #C	CELLS % for stone]
Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water <u>Total Volume of Soakway</u> <u>Net Volume of Soakway</u> <u>Attenuation Surface Storage</u> Outflow from Soakaways during As50= f= D=	26 m2 15 m 0.35 m 0.4 m 0.15 m 19.13 m <sup>3</sup> 12.37 m <sup>3</sup> 3.825 m <sup>3</sup> storm (O) O=As: 31.13 m2 1.12E-06 m/s 3600 secs	STONE CELLS Free volur 50 x f x D Internal su Calculated	Infiltration Infiltration Attenuation me % BIO-RET. R/ urface area (ex d Adjusted Infil	30% 95% (95% for 'Aquacelis'; 309 AINWATER GRDN #C cl. base area) of soakway	CELLS % for stone]
Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water <u>Total Volume of Soakway</u> <u>Net Volume of Soakway</u> <u>Attenuation Surface Storage</u> Outflow from Soakaways during As50= f= D= <u>Outflow =</u>	26 m2 15 m 0.35 m 0.4 m 0.15 m 19.13 m <sup>3</sup> 12.37 m <sup>3</sup> 3.825 m <sup>3</sup> storm (O) O=As: 31.13 m2 1.12E-06 m/s 3600 secs 0.13 m <sup>3</sup>	STONE CELLS Free volur 50 x f x D Internal su Calculater Duration c	Infiltration Infiltration Attenuation me % BIO-RET. RA BIO-RET. RA unface area (ex d Adjusted Infil of storm	30% 95% (95% for 'Aquacells'; 30% NINWATER GRDN #C cl. base area) of soakway Iration Rate (FOS)	CELLS % for stone] to 50% effective dep
Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water Total Volume of Soakway Net Volume of Soakway Attenuation Surface Storage Outflow from Soakaways during As50= f= D=	26 m2 15 m 0.35 m 0.4 m 0.15 m 19.13 m <sup>3</sup> 12.37 m <sup>3</sup> 3.825 m <sup>3</sup> storm (O) O=As: 31.13 m2 1.12E-06 m/s 3600 secs 0.13 m <sup>3</sup>	STONE CELLS Free volur 50 x f x D Internal su Calculated	Infiltration Infiltration Attenuation me % BIO-RET. R/ urface area (ex d Adjusted Infil	30% 95% (95% for 'Aquacells'; 30% NINWATER GRDN #C cl. base area) of soakway Iration Rate (FOS)	CELLS % for stone]
Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water <u>Total Volume of Soakway</u> <u>Net Volume of Soakway</u> <u>Attenuation Surface Storage</u> Outflow from Soakaways during As50= f= D= <u>Outflow =</u>	26 m2 15 m 0.35 m 0.4 m 0.15 m 19.13 m <sup>3</sup> 12.37 m <sup>3</sup> 3.825 m <sup>3</sup> 3.825 m <sup>3</sup> storm (O) O=As: 31.13 m2 1.12E-06 m/s 3600 secs 0.13 m <sup>3</sup> torage Required	STONE CELLS Free volur 50 x f x D Internal su Calculated Duration c [I-O=S]	Infiltration Infiltration Attenuation me % BIO-RET. RA unface area (ex d Adjusted Infil of storm	30% 95% (95% for 'Aquacells'; 30% NINWATER GRDN #C cl. base area) of soakway Iration Rate (FOS)	CELLS % for stone] to 50% effective dep
Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water Total Volume of Soakway Net Volume of Soakway Attenuation Surface Storage Outflow from Soakaways during As50= f= D= Outflow = Inflow - Outflow = St	26 m2 15 m 0.35 m 0.4 m 0.15 m 19.13 m <sup>3</sup> 12.37 m <sup>3</sup> 3.825 m <sup>3</sup> 9 storm (O) O=As: 31.13 m2 1.12E-06 m/s 3600 secs 0.13 m <sup>3</sup> torage Required 2 (50%) Filter Laye	STONE CELLS Free volur 50 x f x D Internal su Calculater Duration c [I-O=S] ar Storage Vol 1	Infiltration Infiltration Attenuation me % BIO-RET. R/ unface area (ex d Adjusted Infil of storm 10.67	30% 95% (95% for 'Aquacells'; 309 AINWATER GRDN #C cl. base area) of soakway tration Rate (FOS) 7 m <sup>3</sup> Stor 3 m <sup>3</sup>	CELLS % for stone] to 50% effective dep age Required
Depth of filter layer 1: Depth of filter layer 2: Dept of Retained water Total Volume of Soakway Net Volume of Soakway Attenuation Surface Storage Outflow from Soakaways during As50= f= D= Outflow = Inflow - Outflow = St Total Swale #8 & RWG #C	26 m2 15 m 0.35 m 0.4 m 0.15 m 19.13 m <sup>3</sup> 12.37 m <sup>3</sup> 3.825 m <sup>3</sup> 9 storm (O) O=As: 31.13 m2 1.12E-06 m/s 3600 secs 0.13 m <sup>3</sup> torage Required 2 (50%) Filter Laye	STONE CELLS Free volur 50 x f x D Internal su Calculater Duration c [I-O=S] ar Storage Vol 1	Infiltration Infiltration Attenuation me % BIO-RET. RA unface area (ex d Adjusted Infil of storm 10.67	30% 95% (95% for 'Aquacells'; 309 AINWATER GRDN #C cl. base area) of soakway tration Rate (FOS) 7 m <sup>3</sup> Stor 3 m <sup>3</sup> 7 m <sup>3</sup> Stor	CELLS % for stone] to 50% effective dep age Required

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#### CITYWISE EDUCATION, FORTUNESTOWN LANE, DUBLIN 24. SUMMARY RECAP OF STORAGE & ATTENUATION CAPACITIES

10 year storm - 60 min duration:	1 1			1
To year storm - ou min duration:				
SUDS CHAIN A-C INFLOW		10.8	m <sup>3</sup>	
SUDS CHAIN B-C INFLOW		10.8	[	
	TAL INCOM			
10		22.1	ញ	
SUDS CHAIN A-C below Ground Void/Soakaway	 Volumo	21.15	3	
SUDS CHAIN A-C below Ground Void/Soakaway		21.15		
SODS CHAIN B-C below Ground Vold/Soakaway		23.21	m	
SUDS CHAIN A-C Above Ground Attenuation Volu	I Imo	8.51	<b>m</b> 3	
SUDS CHAIN A-C Above Ground Attenuation Volt		10.88		
TOTAL Storage &	Attenuaton	03.87	m	
Excess Storage/Attenuation over Inflow		41.75	m <sup>3</sup>	
Excess Storage/Attentiation Over Innow		41.79	104	
· · · · · ·				
100 year storm - 6Hour duration;				
SUDS CHAIN A-C INFLOW		35.2	m <sup>3</sup>	
SUDS CHAIN B-C INFLOW		36.5	m <sup>3</sup>	
то	TAL Inflow	71.7		
e e e e e e e e e e e e e e e e e e e				
INFILTRATION DURING STORM				
SUDS CHAIN A-C INFILTRATION		1.8	m <sup>3</sup>	
SUDS CHAIN B-C INFILTRATION		3.3	m <sup>3</sup>	
Less TOTAL Infiltration du	Iring Storm	5.2	m <sup>3</sup>	
SUDS CHAIN A-C below Ground Void/Soakaway	Volume	21.15	m <sup>3</sup>	
SUDS CHAIN B-C* below Ground Void/Soakaway	Volume	23.27	m <sup>3</sup>	
SUDS CHAIN A-C Above Ground Attenuation Volu	ıme	8.51	m <sup>3</sup>	
SUDS CHAIN B-C* Above Ground Attenuation Vo	lume	10.88	m <sup>3</sup>	
Less TOTAL Storage &	Attenuaton	63.81	m <sup>3</sup>	89%
				of Total inflow
Excess Net Inflow over Storage/Attenuation		2.78	m <sup>3</sup>	
	1		-7	
*= 50% above and below volume of Rain Garden C	used in this	calculation		

#### 26/10/2023

	e & Language Centre Instown Way, Tallaght, Dublin	24.					
Total Flow Capacity of <u>Perforated Riser</u>	Q=Cp.2Ap.(2g)^1/2.(H^3/2)/ 3Hs	m3/s				Ref.: CIRIA C753 28.5.3	
	Q=	0.000164932 1.65E-04	m3/sec m3/sec =	(using input b 0.165			L/sec/Ha
Ap=Cross sectional g= gravity	(0.61 for perforations) area for all holes, m2 radius of holes no of holes per row no. of rows Total no. of holes /2 below the lowest row of		4 3 12 9.81	m2 mm no. no. no. m/s2 mm	0.0045		
S= distance betweer H= effective head, m		=		mm mm	0.075 0.090		
	Allowable flow= Catchment area served = Impermeable & permeable a	880	L/s/ha= m2 = Ds measures on tre	0.0000002 0.088 atment chains	ha		hamber
	Allowable flow for Area=		0.000176 1.76E-04 0.176 OK Perforated Rise	m3/sec L/sec	ax Allowa	ble Flow for Area	