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Surface Water Drainage Report Submission for Compliance

Proposed Construction of 5 Warehouse/Logistics, 3 Office Blocks and a Café/Restaurant Development

to site at

Calmount Road and Ballymount Avenue,
Ballymount Industrial Estate, Dublin 12

Report DFK/23002-01-2

Project No.		23002		Document Ref:		Drainage Services Report 23002-01.doc
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1.0 INTRODUCTION

GRANTED PERMISSION

Planning has been granted under Reg. Ref.: SD22A/0099 and relates to:

inter alia the construction of five no. warehouse/logistics units, 3 no. own door office buildings, a café unit, and all associated development, as permitted by SDDC on the 3rd of February 2023 (final grant date) and subject to 25 no. conditions.

As illustrated on DFK **Drg. No. 23002-01C**, the drainage details included in this compliance submission relates primarily to the southern part of the permitted development, i.e. Unit 1, 6, office buildings 5A to 5C, the café unit and the north-south road up to and the roundabout at the northern boundary of the site, for which compliance with Condition 11 (a) to (c) is sought. The surface water discharge to the rear of Units 3 & 4 will form part of this compliance, subject to slight adjustments of the cover and invert levels. The context to the proposals submitted is described below, followed by the details of the proposals submitted for compliance with Condition 11.

DETAILED DESIGN AND SURFACE WATER MANAGEMENT APPROACH

The drainage design and the surface water management for Unit 1, 6, office buildings 5A to 5C, the café unit and the main north-south road from the site entrance off Calmount Road as far as and including the roundabout towards the northern boundary of the site has been updated. The site investigations completed on site, post planning decision, confirmed infiltration is available and therefore infiltration has been prioritised as the method of controlling surface water runoff from the proposed development.

Upon detailed design of the development, it has become apparent that a new planning application will be required to alter the floor levels and associated site levels including access road levels of certain buildings, namely Units 2, 3 & 4 to ensure compliance with the current Building Regulations. This is merely a planning exercise to adjust floor levels only and not re-size or significantly alter the proposed locations of the units that might have an effect on the overall drainage design submitted as part of this application. The main north-south road is included in this compliance submission from the site entrance off Calmount Road as far as and including the roundabout towards the northern boundary of the site.

The east-west access road north of Unit 6 will be included in the new planning amendment application for the site level alterations although the surface water discharge to the rear of Units 3 & 4 will form part of this compliance, subject to slight adjustments of the cover and invert levels. The road north of Unit 2 requires slight adjustments also and will be included in this planning amendment.

There is also a site in question north of Unit 2 access road which will form part of a separate planning application and the adjusted road levels included in the proposed Planning Amendment. A colour coded site plan indicating this strategy is included on the attached DFK Engineer's Drg No. **23022-01C – Proposed Site Layout**.

SURFACE WATER MANAGEMENT STRATEGY FOLLOWING DETAILED DESIGN -
DETAILS FOR COMPLIANCE WITH CONDITION 11

The original surface water design completed by DBFL took a conservative approach and infiltration was not considered as outlined in the extract below taken from the engineering service report submitted by DBFL at planning stage as no site investigation/soakaway tests were carried out for this planning application:

Whilst modelling the network to determine attenuation volumes a conservative approach was applied where runoff coefficients were not compounded along the treatment train. In the example of figure 3.2 the runoff for the areas draining to the swale was only reduced by a factor of 0.7 when we would expect a further reduction of 0.7 as the runoff will also be routed through the bioretention area. Consequently we can expect that runoff volumes, and as such attenuation volumes, would be reduced compared to those initially modelled herein. On receipt of detailed site investigation data a determination of the infiltration rate will be made to inform calculations as to the exact reduction in runoff and attenuation that can be achieved.

Site investigations completed on site, post planning decision, confirmed infiltration is available and for this reason the surface water design has been updated and infiltration will be prioritised as the method of controlling surface water runoff from the proposed development site. The relevant extract (relevant elements of the report in relation to planning design requirements) from the site investigation report showing the infiltration rates is included in **Appendix V**. The updated design has retained the SuDs mechanisms where viable and due to the infiltration available the attenuation has been reduced. While it has not been possible to omit the below ground attenuation systems entirely, in line with SDCC development plan IE2 Objective 5, the amended design significantly reduces the attenuation required on site. There is one exception to this, Unit 1 where the SuDs mechanisms along the northern and western boundary were not viable due to the steep slope (1:2) along the northern boundary between Units 1 and 2 and the live ESB cables located along the western boundary as identified on the GPR survey. The updated surface water design is included below in section 2.0 of this report.

A GPR survey was completed along Ballymount Avenue where an existing 300mm surface water drain was identified along the eastern boundary of the subject site, which connects to the public surface water sewer network in Ballymount Road Lower, at the junction with Ballymount Avenue. The existing surface water drain includes a 225mm spur into the subject site, which is located approximately 19m from the northern boundary. The invert level of the existing spur is too high and therefore we propose to replace it, so the crowns of the pipes are kept continuous. This is the preferred connection point. A connection at this location would eliminate the need to extend the existing surface water network from Ballymount Road Lower junction to the subject site and in turn cause a lot less disruption to the existing road network. The exiting 300mm pipe, which is laid at a gradient of approx. 1:55, has the capacity for 150.0l/sec. The maximum permissible discharge for the 1 in 100 year return period is 34.12l/sec which equates to approximately 23% of the pipes capacity.

As outlined above existing ESB cables were identified along the western boundary to the rear of Unit 1 and therefore the SuDs mechanism proposed initially along this green belt are not viable.

The access road levels were amended to ensure access to and from all buildings are compliant with Part M of the building regulations and provide a cut-fill balance for an economical design. Units 2, 3, 4 and the east-west internal roads are subject to an Amendment Planning. The updated site layout is shown on **DFK Drg. No. 23002-01C**.

This report should be read in conjunction with the following drawings; which are enclosed with this submission:

Drawing number	Description
23002-01/C	Proposed Site Layout
23002-02/B	Proposed Drainage Layout for Units
23002-03/B	Proposed Drainage Layout for Internal Roads
23002-04	Proposed Drainage Layout for Units – Storm Water Only
23002-05	Proposed Drainage Layout for Internal Roads – Storm Water Only
23002-10/A	Drainage Details – Sheet 1
23002-11/A	Drainage Details – Sheet 1
23002-12/A	Typical Manhole Details

Table 1 - Drawing Schedule

2.0 SURFACE WATER

DETAILED DESIGN AND FINAL SURFACE WATER STRATEGY

The surface water network will be designed and arranged in accordance with the requirements of the GDSDS and the GDRC in conjunction with “Recommendations for Site Development Works for Housing Areas” (current edition) published by the (DOEHLG). Cognisance has also been taken of the recommendations contained within the Building Regulations Part H – Drainage and Waste Water Disposal.

The GDSDS guidelines require the following main 4 criteria to be provided by the development’s surface water design.

- Criterion 1: River Water Quality Protection
- Criterion 2: River Regime Protection
- Criterion 3: Level of Service (flooding) for the site
- Criterion 4: River flood protection

The surface water network will be laid as a separate system and drains will be laid such as to minimise the risk of misconnections.

The extreme rainfall matrix table for subject site has been used to obtain a rainfall profile for calculation of storage requirements. The rainfall values have been increased by 20% to include for climate change characteristics, which is greater than the 10% required by the GDSDS.

As per the previous design the proposed surface water drainage network will consist of 8 sub-catchments. The sub-catchments are based on the boundaries of the individual logistics and offices (Units 1-6), the café unit at the entrance to the site and the roads drainage catchment (to be taken in charge). The sub-catchments cover the full proposed development footprint and provide discreet drainage, SuDS features and attenuation volume for each individual unit and for the proposed roads servicing the site.

The boundaries of each sub-catchment allow for the unit drainage to be maintained by the eventual unit purchaser/tenant through entering an agreement with a management company. The proposed roads drainage has also been designed to be standalone, collecting only roads and public open space area runoff so that it is suitable for taking in charge by the local authority. The 8 sub-catchments discharge at controlled rates to a collector sewer which in turn will exit the site at the northeast boundary and connect to the surface water sewer in Ballymount Avenue as outlined in Section 1.

Roads:

The surface water run-off from the estate roads will drain to the planted swales via kerb gullies located on each side of the road. The planted swales will include tree planting to the landscape architects’ detail and a 1.0m wide by 0.75m deep trench, constructed using structural soil below. The soil will be mounded locally around some of the trees within the swale and will act as check dams. If one refers to the calculations for the trenches included in **Appendix II** it can be seen that each trench has an overflow discharge and therefore an overflow will be provided from each of the trenches to the drainage network. The overflow from the trenches will be attenuated within the modular arch system using a hydrobrake or similar approved flow control device before discharging to the collector

sewer. The section of road to the west of the roundabout will be collected via gullies and attenuated within the modular arch system proposed.

Units:

In general, the rainwater run-off from the roof areas will discharge to proposed private-side building drainage around the perimeter of the building footprint prior to discharging to the proposed SuDs mechanisms where feasible. Where the SuDs mechanisms have an overflow discharge, a high-level overflow will be provided to the drainage network.

The service yards will drain to the planted swales via kerb gullies where feasible with the remainder of the service yard collected by gullies and attenuated within the modular arch system. The carpark areas of each unit will be constructed using permeable paving/porous asphalt. The stone media below the permeable paving proposed will collect the run-off from the paving surface itself and the adjacent hardstanding areas.

Criterion 1 – River Water Quality Protection

GDSDS Section 6.3.1.2.1 requires that no run-off should directly pass to the receiving watercourse for rainfall depths of 5mm and a treatment volume (Vt) be provided in order to prevent any pollutants or sediments discharging into watercourses / rivers, etc. for rainfall depths of 15mm. The interception and treatment volume, both required and provided, for each sub-catchment is given in Table 2 below:

Location	Interception Volume		Treatment Volume	
	Required	*Provided	Required	*Provided
Roads	29.98m ³	127.31m ³	89.93m ³	127.31m ³
Unit 1	23.07m ³	191.82m ³	75.20m ³	191.82m ³
Unit 2	30.22m ³	231.73m ³	90.65m ³	231.73m ³
Unit 3	27.60m ³	142.98m ³	82.79m ³	142.98m ³
Unit 4	34.06m ³	137.80m ³	102.17m ³	142.15m ³
Unit 5	23.12m ³	170.49m ³	69.35m ³	193.62m ³
Unit 6	33.04m ³	154.32m ³	99.11m ³	161.82m ³
Unit 7 (Café)	4.54m ³	97.97m ³	13.62m ³	101.92m ³

*Refer to the ‘Attenuation Design Criteria’ calculation sheet included in Appendix I for justification on these figures

Table 2 – Interception and Treatment Volume

In addition to the above the surface water run-off from the hardstanding areas will pass through a suitably sized Class 1 Klarester by-pass Separator or similar approved. All petrol interceptors will be installed upstream of the attenuation systems. The exception to this is the internal estate roads, as the run-off passes through SuDs features, where it will be treated, prior to entering the attenuation. The section of road to the west of the roundabout, where the surface water run-off is collected via gullies will include a by-pass separator upstream of the attenuation system.

Criterion 2 - River Regime Protection

The allowable outflow, QBAR, for the whole site has been calculated as 13.12l/sec. Applying the growth curve factors in accordance with Table 6.6 of the GDSDS the allowable outflow for the 1 in 30 year return period and the 1 in 100 year return period is 27.56l/sec and 34.12l/sec respectively. The QBAR calculation is based on a SOIL factor of 0.3 which corresponds with Soil Type 2 in the Flood Studies Report.

The allowable outflow from each sub-catchment is given in Table 3 below:

Location	Allowable Outflow		
	QBAR	30 years	100 years
Growth Factor	1.0	2.1	2.6
Roads	2.19l/sec	4.59l/sec	5.69l/sec
Unit 1	1.47l/sec	3.09l/sec	3.82l/sec
Unit 2	1.85l/sec	3.88l/sec	4.80l/sec
Unit 3	2.50l/sec	3.14l/sec	3.89l/sec
Unit 4	2.28l/sec	4.79l/sec	5.92l/sec
Unit 5	1.52l/sec	3.19l/sec	3.95l/sec
Unit 6	1.89l/sec	3.96l/sec	4.91l/sec
Unit 7 (Café)	0.44l/sec	0.92l/sec	1.14l/sec

Table 3 – Sub-catchment allowable outflows.

The surface water runoff from each sub-catchment will be restricted using a hydro brake flow control devices or similar approved. The surface water run-off generated from Unit 7 (café) for the 1 in 100 year return period is dealt with onsite using infiltration and only flows in excess of the 1 in 100 year return period will leave the site.

This is similar for Unit 4 where the SuDs features have been designed where the overflow from them is less than the allowable outflow given in Table 3 above and therefore, a flow control device is not required for these units.

Units 2, 3 and 6 have been designed where the SuDs features have an overflow and therefore the allowable outflow for the attenuation calculations have been reduced to reflect this.

As per Criterion 2 the attenuation volume required for each sub-catchment, for 1 in 30 year return period and the 1 in 100 year return period which includes the additional increment in accordance with GDSDS requirements, is given in Table 4 below.

Location	Attenuation Volume		
	30 Year	100 Year	Provided
Roads	25.70m ³	62.90m ³	108.10m ³
Unit 1	259.20m ³	368.50m ³	378.00m ³
Unit 2	133.70m ³	189.70m ³	191.50m ³
Unit 3	268.00m ³	358.90m ³	364.30m ³
*Unit 4	0.00m ³	0.00m ³	0.00m ³
Unit 5	34.90m ³	53.00m ³	53.60m ³
Unit 6	146.90m ³	180.80m ³	183.20m ³
*Unit 7 (Café)	0.00m ³	0.00m ³	0.00m ³

*No attenuation required

Table 4 – Attenuation Volumes.

As outlined above the amended design has retained the SuDs mechanisms where viable and due to the infiltration available the below ground attenuation has been reduced with the exception of Unit 1. The reduction is outlined in Table 5 below:

Location	Below ground Attenuation		
	Granted under Reg. Ref.: SD22A/0099	Amended Design - Proposed	Difference
Roads	435.00m ³	108.1m ³	- 326.90m ³
Unit 1	327.00m ³	378.00m ³	+ 51.00m ³
Unit 2	512.04m ³	191.50m ³	- 320.54m ³
Unit 3	512.00m ³	364.30m ³	- 147.70m ³
Unit 4	461.00m ³	0.00m ³	- 461.00m ³
Unit 5	209.00m ³	53.60m ³	- 155.40m ³
Unit 6	431.88m ³	183.20m ³	- 248.68m ³
Unit 7 (Café)	51.79m ³	0.00m ³	- 51.79m ³

Table 5 – Reduction in below ground Attenuation Volumes.

The calculations for the permeable paving proposed for the carparks are included in **Appendix II**. The overall depth of drainage stone provided below the permeable paving and grass paving is 350mm which is greater than the Hmax calculated. A factor of safety has been applied to the infiltration rate calculated on site in accordance with CIRIA 156.

Criterion 3: Level of Service (flooding) for the site

The SuDS mechanisms outlined within this report have been designed for a 1 in 100 year return period storm, as required by GDSDS “Regional Drainage Policies Vol 2 New Development”. Collectively the SuDS mechanisms have been designed to ensure that no flooding will occur within the site up to the 30 year return period storm, as well as being able to deal with events up to a 1 in 100 year return period storm.

A minimum freeboard of 500mm above attenuation top water level for a 1 in 100-year flood event has been provided to all building floor levels and planned flood routing for storms greater than 100-year level have been considered in design and development runoff will be contained within site.

Criterion 4: River flood protection

It is proposed to meet the River Flood protection requirements by providing infiltration storage equal to the long-term storage as per sub-criterion 4.2. The objective is to match the runoff volume discharged to the downstream receiving watercourse after development to that which occurred prior to development. This volume will be calculated by comparing the 100-year 6-hour event for ‘pre’ and ‘post’ development and is referred to as long-term storage.

The long term storage required and provided for each sub-catchment is given in Table 6 below:

Location	Long-Term Storage Volumes	
	Required	*Provided
Roads	39.88m ³	127.31m ³
Unit 1	188.18m ³	191.82m ³
Unit 2	48.83m ³	231.73m ³
Unit 3	137.01m ³	142.98m ³
Unit 4	35.62m ³	137.80m ³
Unit 5	56.29m ³	170.49m ³
Unit 6	†-84.86m ³	154.32m ³
Unit 7 (Café)	†-66.18m ³	97.97m ³

*Refer to the ‘Attenuation Design Criteria’ calculation sheet included in Appendix I for justification on these figures

† The long term storage is a negative figure due to the low percentage of impermeable area (PIMP).

Table 6 – Long term storage.

The revised drainage layout is shown on DFK **Drg. 23002-02/B, 23002-03/B, 23002-04** and **23002-05**. Drainage details and typical details are included on DFK **Drg. 23002-10A, 23022-11/A** and **23002-12A**.

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APPENDIX I

SURFACE WATER + SUD'S CALCULATIONS

SURFACE WATER CALCULATIONS INDEX

- Return Period Rainfall Depths Table
- Site Catchment Characteristics – Whole Site
- Drainage Calculations – Internal Roads
- Drainage Calculations – Unit 1
- Drainage Calculations – Unit 2
- Drainage Calculations – Unit 3
- Drainage Calculations – Unit 4
- Drainage Calculations – Unit 5
- Drainage Calculations – Unit 6
- Drainage Calculations – Unit 7 (Café)



 DFK <i>Structural Engineers</i>	Doherty Finegan Kelly <i>Consulting Structural & Civil Engineers,</i>		Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265				
	Project:		Design:	<input checked="" type="checkbox"/>		Telephone Log:	<input type="checkbox"/>
	Calmount Rd, Ballymount - Internal Roads		Minutes:	<input type="checkbox"/>		Other Record:	<input type="checkbox"/>
	Project No:	Element:				Prepared:	Checked:
23002	Site Catchment Characteristics				NS	SG/CK	

Reference | Output

Site Catchment Characteristics

Total Site Area	10940 m ²
Hardstanding - Road	4648 m ²
Hardstanding - F&C/P	2846 m ²
Permeable area	0 m ²
Landscape	3446 m ²

QBAR	0.092 m ³ /sec
SAAR	707.0 mm
SOIL	0.3
AREA **	0.50 km ²
QBAR/ha (l/s/ha)	2.000

** The area taken in calculating QBAR/ha is 50 ha in accordance with paragraph 6.6.1 of Vol 2 of the GDSDS.

Areas Contributing into Drainage Network:

Areas Contributing into:

Location	Area
TOTAL	0 m²

Location	Area
TOTAL	0 m²

Location	Area
TOTAL	0 m ²

Location	Area
TOTAL	0 m²

Location	Area
TOTAL	0 m ²

Location	Area
TOTAL	0 m ²

Allowable Outflow

Growth Curve	1 years	QBAR	10 years	30 years	100 years
Multiplier	0.85	1	1.7	2.1	2.6
Allowable Outflow (l/s)	1.86	2.19	3.72	4.59	5.69

Calmount Rd, Ballymount - Extreme Rainfall Matrix

RP5 60min= 17.5 mm RP5 2d= 63.5 mm ANNUAL RAINFALL= 707.0 mm

DURATION	RETURN PERIOD (YEARS)								
	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	2.9	4.3	5.2	7.8	10.1	12.7	14.4	17.0	21.1
10 min	4.1	6.0	7.1	10.9	14.0	17.6	20.2	23.6	29.4
15 min	4.8	7.1	8.4	12.8	16.6	20.8	23.6	27.8	34.6
30 min	6.2	9.2	10.9	16.4	20.9	26.2	29.6	34.7	42.8
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	10.9	15.7	18.2	26.9	33.6	41.4	46.6	53.9	65.5
4 hr	14.5	20.5	23.6	34.3	42.6	52.1	58.3	67.1	81.0
6 hr	17.0	23.9	27.6	39.6	49.0	59.5	66.5	76.3	91.7
12 hr	22.6	31.2	35.8	50.6	62.2	75.0	83.4	95.0	113.5
24 hr	29.8	40.7	46.3	64.8	78.7	94.3	104.4	118.4	140.4
48 hr	37.2	49.6	55.9	76.2	91.2	107.8	118.3	133.0	155.5
72 hr	43.2	56.8	63.7	85.4	101.4	118.7	129.8	145.0	168.2

Allowance of 20% for Climate Change in accordance with GDSDS

	<p>Doherty Finegan Kelly Consulting Structural & Civil Engineers, Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265</p>								
	Project: Calmount Rd, Ballymount - Internal Roads				Design: <input checked="" type="checkbox"/>	Minutes: <input type="checkbox"/>	Telephone Log:	<input type="checkbox"/>	
Project No: 23002	Element: Infiltration Trench 1 (Cafe)				Prepared: NS		Checked: CK		
Reference:									Output:
Calmount Rd, Ballymount - Extreme Rainfall Matrix									
RP5 60min= 16.2 mm		RP5 2d= 59.4 mm		ANNUAL RAINFALL= 707.0 mm					
RETURN PERIOD (YEARS)									
DURATION	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3
Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)									
Contributing Area Plan									

	Doherty Finegan Kelly <i>Consulting Structural & Civil Engineers,</i>		Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265																																																	
	Project: Calmount Rd, Ballymount - Internal Roads		Design: <input checked="" type="checkbox"/>	Telephone Log:		<input type="checkbox"/>																																														
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Vertical Sided System																																																				
<p>From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice</p> <table border="1" style="margin-bottom: 10px; border-collapse: collapse;"> <thead> <tr> <th>Description</th> <th>Type</th> <th>Result</th> </tr> </thead> <tbody> <tr> <td>Infiltration Rate</td> <td>Soil</td> <td>53.1 mm/hr</td> </tr> <tr> <td>FOS</td> <td>Minor Inconvenience</td> <td>3.00</td> </tr> <tr> <td>q</td> <td></td> <td>0.018 m/hr</td> </tr> </tbody> </table> <p><u>Equations Applied to Determine hmax</u></p> $h_{\max} = a(e^{(-bD)} - 1) \quad (1)$ <p>where:</p> $b = \frac{Pq}{A_p n} \quad (2)$ <p>and a is given by:</p> $a = \frac{A_b}{P} - \frac{A_p i}{Pq} \quad (3)$ <table border="1" style="margin-top: 10px; border-collapse: collapse;"> <tr> <td>b =</td> <td>0.121</td> </tr> <tr> <td>Ab/P =</td> <td>0.488</td> </tr> </table>							Description	Type	Result	Infiltration Rate	Soil	53.1 mm/hr	FOS	Minor Inconvenience	3.00	q		0.018 m/hr	b =	0.121	Ab/P =	0.488																														
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Doherty Finegan Kelly
Consulting Structural & Civil Engineers,
Botanic Court, 30 Botanic Road, Glasnevin,
Dublin 9
Tel: 8301852 / Fax: 8602265

Project:

Design:

Telephone Log:

Calmount Rd, Ballymount - Internal Roads

Minutes:

Other Record:

Project No:

Element:

Prepared:

Checked:

23002

Infiltration Trench 1 (Unit 1)

NS

CK

Reference:

Output:

Calmount Rd, Ballymount - Extreme Rainfall Matrix

RP5 60min= 16.2 mm RP5 2d= 59.4 mm ANNUAL RAINFALL= 707.0 mm

RETURN PERIOD (YEARS)

DURATION	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3

Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)

Contributing Area Plan



Doherty Finegan Kelly

Consulting Structural & Civil Engineers,

Botanic Court, 30 Botanic Road, Glasnevin,

Dublin 9

Tel: 8301852 / Fax: 8602265

Project:

Calmount Rd, Ballymount - Internal Roads

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Infiltration Trench 1 (Unit 1)

NS

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Reference:

Output:

Vertical Sided System

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	Soil	152.7 mm/hr
FOS	Minor Inconvenience	3.00
q		0.051 m/hr

Equations Applied to Determine hmax

$$h_{\max} = a(e^{(-bD)} - 1) \quad (1)$$

Assume - uniform gravel (n)	0.30
-----------------------------	------

Area to be Drained	
A _D	425 m ²

where:

$$b = \frac{Pq}{A_b n} \quad (2)$$

and a is given by:

$$a = \frac{A_b}{P} - \frac{A_D i}{Pq} \quad (3)$$

b=	0.350
Ab/P=	0.484

H_{max} Calculation

10 Year Return Period

Duration (D)	hmax	a
15.000 min	0.691	-8.240
30.000 min	0.806	-5.016
60.000 min	0.889	-3.008
120.000 min	0.871	-1.728
240.000 min	0.692	-0.918
360.000 min	0.518	-0.590

30 Year Return Period

Duration (D)	hmax	a
15.000 min	1.004	-11.969
30.000 min	1.177	-7.323
60.000 min	1.305	-4.415
120.000 min	1.301	-2.582
240.000 min	1.082	-1.436
360.000 min	0.856	-0.975

50 Year Return Period

Duration (D)	hmax	a
15.000 min	1.189	-14.182
30.000 min	1.390	-8.650
60.000 min	1.539	-5.205
120.000 min	1.544	-3.064
240.000 min	1.300	-1.724
360.000 min	1.045	-1.191

100 Year Return Period

Duration (D)	hmax	a
15.000 min	1.486	-17.722
30.000 min	1.736	-10.800
60.000 min	1.917	-6.485
120.000 min	1.930	-3.830
240.000 min	1.645	-2.183
360.000 min	1.341	-1.528

Vertical Sided System - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{1}{b} \log_e \left[\frac{h_{\max} + \frac{A_b}{P}}{h_{\max} + \frac{A_b}{P}} \right]$$

Event	Time to Empty
1 in 10 years	1.116 hrs
1 in 30 years	1.295 hrs
1 in 50 years	1.367 hrs
1 in 100 years	1.456 hrs

Infiltration System -- Overflow from French Drain

Return Period	Duration	Base Area (A _b)	h _{PROVIDED}	h _{max}	Q _{OVERFLOW} *
10 Years	60.000 min	30.700 m ²	0.750 m	0.889 m	0.031 l/sec
30 Years	60.000 min	30.700 m ²	0.750 m	1.305 m	0.176 l/sec
50 Years	60.000 min	30.700 m ²	0.750 m	1.544 m	0.292 l/sec
100 Years	60.000 min	30.700 m ²	0.750 m	1.930 m	0.532 l/sec

* Q_{OVERFLOW} is the averaged flow for the duration given.

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Calmount Rd, Ballymount - Internal Roads		Minutes:	<input type="checkbox"/>	Other Record:			<input type="checkbox"/>		
Project No:	Element:		Prepared:			Checked:			
23002	Infiltration Trench 1 (Unit 4)		NS			CK			
Reference:								Output:	
Calmount Rd, Ballymount - Extreme Rainfall Matrix									
RP5 60min= 16.2 mm		RP5 2d= 59.4 mm		ANNUAL RAINFALL= 707.0 mm					
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DURATION	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3
Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)									
Contributing Area Plan									



Doherty Finegan Kelly

Consulting Structural & Civil Engineers,

Botanic Court, 30 Botanic Road, Glasnevin,

Dublin 9

Tel: 8301852 / Fax: 8602265

Project:

Calmount Rd, Ballymount - Internal Roads

Design:



Telephone Log:



Minutes:



Other Record:



Project No:

Element:

Prepared:

Checked:

23002

Infiltration Trench 1 (Unit 4)

NS

CK

Reference:

Output:

Vertical Sided System

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	Soil	12.8 mm/hr
FOS	Minor Inconvenience	3.00
q		0.004 m/hr

Equations Applied to Determine hmax

$$h_{\max} = a(e^{(-bD)} - 1) \quad (1)$$

Assume - uniform gravel (n)	0.30
-----------------------------	------

Area to be Drained	
A _D	402 m ²

where:

$$b = \frac{Pq}{A_D n} \quad (2)$$

and a is given by:

$$a = \frac{A_D}{P} - \frac{A_D j}{Pq} \quad (3)$$

b =	0.029
Ab/P =	0.490

Infiltration Trench dimensions

Length	48.00 m
Width	1.00 m
Base Area (A _b)	48.000 m ²
Perimeter (P)	98.000 m

H_{max} Calculation

10 Year Return Period

Duration (D)	hmax	a
15.000 min	0.457	-63.194
30.000 min	0.572	-39.659
60.000 min	0.716	-25.007
120.000 min	0.884	-15.662
240.000 min	1.069	-9.749
360.000 min	1.176	-7.355

30 Year Return Period

Duration (D)	hmax	a
15.000 min	0.654	-90.422
30.000 min	0.814	-56.503
60.000 min	1.010	-35.275
120.000 min	1.235	-21.892
240.000 min	1.483	-13.528
360.000 min	1.625	-10.163

50 Year Return Period

Duration (D)	hmax	a
15.000 min	0.771	-106.573
30.000 min	0.954	-66.194
60.000 min	1.175	-41.043
120.000 min	1.434	-25.411
240.000 min	1.714	-15.633
360.000 min	1.877	-11.739

100 Year Return Period

Duration (D)	hmax	a
15.000 min	0.958	-132.416
30.000 min	1.180	-81.884
60.000 min	1.442	-50.388
120.000 min	1.749	-31.006
240.000 min	2.081	-18.979
360.000 min	2.271	-14.201

Vertical Sided System - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{1}{b} \log_e \left[\frac{h_{\max} + \frac{A_b}{P}}{\frac{h_{\max}}{2} + \frac{A_b}{P}} \right]$$

Event	Time to Empty
1 in 10 years	14.994 hrs
1 in 30 years	16.697 hrs
1 in 50 years	17.394 hrs
1 in 100 years	18.246 hrs

Infiltration System -- Overflow from French Drain

Return Period	Duration	Base Area (A _b)	h _{PROVIDED}	h _{max}	Q _{OVERFLOW} *
10 Years	60.000 min	48.000 m ²	0.750 m	1.176 m	0.151 l/sec
30 Years	60.000 min	48.000 m ²	0.750 m	1.625 m	0.434 l/sec
50 Years	60.000 min	48.000 m ²	0.750 m	1.877 m	0.649 l/sec
100 Years	60.000 min	48.000 m ²	0.750 m	2.271 m	1.073 l/sec

* Q_{OVERFLOW} is the averaged flow for the duration given.

	Doherty Finegan Kelly <i>Consulting Structural & Civil Engineers,</i>		Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265						
	Project: Calmount Rd, Ballymount - Internal Roads		Design:	<input checked="" type="checkbox"/>	Telephone Log:	<input type="checkbox"/>			
Project No:	Element:	Minutes:	<input type="checkbox"/>	Other Record:	<input type="checkbox"/>				
23002	Infiltration Trench 1 (Unit 5C)	Prepared:	Checked:						
		NS	CK						
Reference:							Output:		
Calmount Rd, Ballymount - Extreme Rainfall Matrix									
RP5 60min= 16.2 mm		RP5 2d= 59.4 mm		ANNUAL RAINFALL= 707.0 mm					
RETURN PERIOD (YEARS)									
DURATION	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3
Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)									
Contributing Area Plan									



Doherty Finegan Kelly

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Dublin 9

Tel: 8301852 / Fax: 8602265

Project:

Calmount Rd, Ballymount - Internal Roads

Design: Telephone Log: Minutes: Other Record:

Project No:

Element:

Prepared:

Checked:

23002

Infiltration Trench 1 (Unit 5C)

NS

CK

Reference: Output:

Vertical Sided System

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	Soil	555.9 mm/hr
FOS	Minor Inconvenience	3.00
q		0.185 m/hr

Equations Applied to Determine hmax

$$h_{\max} = a(e^{(-bD)} - 1) \quad (1)$$

Assume - uniform gravel (n)	0.30
-----------------------------	------

where:

$$b = \frac{Pq}{A_p n} \quad (2)$$

and a is given by:

$$a = \frac{A_b}{P} - \frac{A_p j}{Pq} \quad (3)$$

b=	1.338
Ab/P=	0.462

Infiltration Trench dimensions

Length	12.00 m
Width	1.00 m
Base Area (A_b)	12.000 m ²
Perimeter (P)	26.000 m

H_{max} Calculation

10 Year Return Period

Duration (D)	hmax	a
15.000 min	1.038	-3.649
30.000 min	1.039	-2.130
60.000 min	0.874	-1.184
120.000 min	0.541	-0.581
240.000 min	0.198	-0.199
360.000 min	0.045	-0.045

30 Year Return Period

Duration (D)	hmax	a
15.000 min	1.538	-5.407
30.000 min	1.570	-3.217
60.000 min	1.363	-1.847
120.000 min	0.916	-0.983
240.000 min	0.441	-0.443
360.000 min	0.226	-0.226

50 Year Return Period

Duration (D)	hmax	a
15.000 min	1.834	-6.450
30.000 min	1.875	-3.843
60.000 min	1.637	-2.220
120.000 min	1.127	-1.210
240.000 min	0.576	-0.579
360.000 min	0.328	-0.328

100 Year Return Period

Duration (D)	hmax	a
15.000 min	2.308	-8.118
30.000 min	2.369	-4.856
60.000 min	2.082	-2.823
120.000 min	1.463	-1.572
240.000 min	0.791	-0.795
360.000 min	0.487	-0.487

Vertical Sided System - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{1}{b} \log_e \left[\frac{h_{\max} + \frac{A_b}{P}}{h_{\max} + \frac{A_b}{P}} \right]$$

Event	Time to Empty
1 in 10 years	0.318 hrs
1 in 30 years	0.365 hrs
1 in 50 years	0.383 hrs
1 in 100 years	0.405 hrs

Infiltration System -- Overflow from French Drain

Return Period	Duration	Base Area (A_b)	h_{PROVIDED}	h_{\max}	Q_{OVERFLOW}^*
10 Years	60.000 min	12.000 m ²	0.750 m	1.039 m	0.026 l/sec
30 Years	60.000 min	12.000 m ²	0.750 m	1.570 m	0.102 l/sec
50 Years	60.000 min	12.000 m ²	0.750 m	1.875 m	0.162 l/sec
100 Years	60.000 min	12.000 m ²	0.750 m	2.369 m	0.286 l/sec

* Q_{OVERFLOW} is the averaged flow for the duration given.



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Project:

Design:

Telephone Log:

Calmount Rd, Ballymount - Internal Roads

Minutes:

Other Record:

Project No:

Element:

Prepared:

Checked:

23002

Infiltration Trench 2 (Cafe)

NS

CK

Reference:

Output:

Calmount Rd, Ballymount - Extreme Rainfall Matrix

RP5 60min= 16.2 mm RP5 2d= 59.4 mm ANNUAL RAINFALL= 707.0 mm

RETURN PERIOD (YEARS)

DURATION	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3

Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)

Contributing Area Plan



Doherty Finegan Kelly

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Dublin 9

Tel: 8301852 / Fax: 8602265

Project:

Calmount Rd, Ballymount - Internal Roads

Design:

Telephone Log:

Minutes:

Other Record:

Project No:

Element:

Prepared:

Checked:

23002

Infiltration Trench 2 (Cafe)

NS

CK

Reference:

Output:

Vertical Sided System

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	Soil	92.9 mm/hr
FOS	Minor Inconvenience	3.00
q		0.031 m/hr

Equations Applied to Determine hmax

$$h_{\max} = a(e^{(-bD)} - 1) \quad (1)$$

where:

$$b = \frac{Pq}{A_b n} \quad (2)$$

and a is given by:

$$a = \frac{A_b - A_d i}{P - Pq} \quad (3)$$

b =	0.220
Ab/P =	0.469

H_{max} Calculation

10 Year Return Period

Duration (D)	hmax	a
15.000 min	0.803	-15.016
30.000 min	0.968	-9.293
60.000 min	1.131	-5.730
120.000 min	1.231	-3.458
240.000 min	1.182	-2.020
360.000 min	1.054	-1.438

30 Year Return Period

Duration (D)	hmax	a
15.000 min	1.158	-21.637
30.000 min	1.394	-13.389
60.000 min	1.624	-8.227
120.000 min	1.770	-4.973
240.000 min	1.720	-2.939
360.000 min	1.554	-2.121

50 Year Return Period

Duration (D)	hmax	a
15.000 min	1.368	-25.564
30.000 min	1.640	-15.745
60.000 min	1.901	-9.630
120.000 min	2.074	-5.829
240.000 min	2.019	-3.451
360.000 min	1.835	-2.504

100 Year Return Period

Duration (D)	hmax	a
15.000 min	1.704	-31.848
30.000 min	2.037	-19.561
60.000 min	2.350	-11.902
120.000 min	2.559	-7.189
240.000 min	2.495	-4.265
360.000 min	2.274	-3.103

Vertical Sided System - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{1}{b} \log_e \left[\frac{h_{\max} + \frac{A_b}{P}}{\frac{h_{\max} + \frac{A_b}{P}}{2}} \right]$$

Event	Time to Empty
1 in 10 years	2.043 hrs
1 in 30 years	2.286 hrs
1 in 50 years	2.382 hrs
1 in 100 years	2.496 hrs

Infiltration System -- Overflow from French Drain

Return Period	Duration	Base Area (A _b)	h _{PROVIDED}	h _{max}	Q _{OVERFLOW} *
10 Years	60.000 min	15.300 m ²	0.750 m	1.231 m	0.054 l/sec
30 Years	60.000 min	15.300 m ²	0.750 m	1.770 m	0.161 l/sec
50 Years	60.000 min	15.300 m ²	0.750 m	2.074 m	0.243 l/sec
100 Years	60.000 min	15.300 m ²	0.750 m	2.559 m	0.407 l/sec

* Q_{OVERFLOW} is the averaged flow for the duration given.



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Project:

Design:

Telephone Log:

Calmount Rd, Ballymount - Internal Roads

Minutes:

Other Record:

Project No:

Element:

Prepared:

Checked:

23002

Infiltration Trench 2 (Unit 1)

NS

CK

Reference:

Output:

Calmount Rd, Ballymount - Extreme Rainfall Matrix

RP5 60min= 16.2 mm RP5 2d= 59.4 mm ANNUAL RAINFALL= 707.0 mm

RETURN PERIOD (YEARS)

DURATION	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3

Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)

Contributing Area Plan



Doherty Finegan Kelly

Consulting Structural & Civil Engineers,

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Dublin 9

Tel: 8301852 / Fax: 8602265

Project:

Calmount Rd, Ballymount - Internal Roads

Design:	<input checked="" type="checkbox"/>	Telephone Log:	<input type="checkbox"/>
Minutes:	<input type="checkbox"/>	Other Record:	<input type="checkbox"/>

Project No:

Element:

Prepared:

Checked:

23002

Infiltration Trench 2 (Unit 1)

NS CK

Reference: Output:

Vertical Sided System

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	Soil	144.8 mm/hr
FOS	Minor Inconvenience	3.00
q		0.048 m/hr

Equations Applied to Determine hmax

$$h_{\max} = a(e^{(-bD)} - 1) \quad (1)$$

Assume - uniform gravel (n)	0.30
-----------------------------	------

where:

$$b = \frac{Pq}{A_b n} \quad (2)$$

and a is given by:

$$a = \frac{A_b}{P} - \frac{A_b i}{Pq} \quad (3)$$

b =	0.337
Ab/P =	0.477

Infiltration Trench dimensions

Length	20.70 m
Width	1.00 m
Base Area (A_b)	20.700 m ²
Perimeter (P)	43.400 m

H_{max} Calculation

10 Year Return Period

Duration (D)	hmax	a
15.000 min	1.565	-19.350
30.000 min	1.866	-12.022
60.000 min	2.136	-7.461
120.000 min	2.233	-4.552
240.000 min	2.008	-2.711
360.000 min	1.706	-1.965

30 Year Return Period

Duration (D)	hmax	a
15.000 min	2.250	-27.826
30.000 min	2.680	-17.267
60.000 min	3.052	-10.658
120.000 min	3.185	-6.491
240.000 min	2.879	-3.887
360.000 min	2.464	-2.839

50 Year Return Period

Duration (D)	hmax	a
15.000 min	2.657	-32.855
30.000 min	3.148	-20.284
60.000 min	3.566	-12.454
120.000 min	3.722	-7.587
240.000 min	3.364	-4.543
360.000 min	2.890	-3.330

100 Year Return Period

Duration (D)	hmax	a
15.000 min	3.308	-40.901
30.000 min	3.906	-25.168
60.000 min	4.399	-15.363
120.000 min	4.577	-9.329
240.000 min	4.136	-5.584
360.000 min	3.555	-4.097

Vertical Sided System - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{1}{b} \log_e \left[\frac{h_{\max} + \frac{A_b}{P}}{\frac{h_{\max}}{2} + \frac{A_b}{P}} \right]$$

Event	Time to Empty
1 in 10 years	1.574 hrs
1 in 30 years	1.692 hrs
1 in 50 years	1.736 hrs
1 in 100 years	1.788 hrs

Infiltration System -- Overflow from French Drain

Return Period	Duration	Base Area (A_b)	h_{PROVIDED}	h_{\max}	Q_{OVERFLOW}^*
10 Years	60.000 min	20.700 m ²	0.750 m	2.233 m	0.226 l/sec
30 Years	60.000 min	20.700 m ²	0.750 m	3.185 m	0.521 l/sec
50 Years	60.000 min	20.700 m ²	0.750 m	3.722 m	0.738 l/sec
100 Years	60.000 min	20.700 m ²	0.750 m	4.577 m	1.165 l/sec

* Q_{OVERFLOW} is the averaged flow for the duration given.

	Doherty Finegan Kelly <i>Consulting Structural & Civil Engineers,</i>		Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265						
	Project:		Design:	<input checked="" type="checkbox"/>	Telephone Log:			<input type="checkbox"/>	
Calmount Rd, Ballymount - Internal Roads		Minutes:	<input type="checkbox"/>	Other Record:			<input type="checkbox"/>		
Project No:	Element:		Prepared:			Checked:			
23002	Infiltration Trench 2 (Unit 2)		NS			CK			
Reference:								Output:	
Calmount Rd, Ballymount - Extreme Rainfall Matrix									
RP5 60min= 16.2 mm		RP5 2d= 59.4 mm		ANNUAL RAINFALL= 707.0 mm					
RETURN PERIOD (YEARS)									
DURATION	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3
Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)									
Contributing Area Plan									



Doherty Finegan Kelly

Consulting Structural & Civil Engineers,

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Dublin 9

Tel: 8301852 / Fax: 8602265

Project:

Calmount Rd, Ballymount - Internal Roads

Design:

Telephone Log:

Minutes:

Other Record:

Project No:

Element:

Prepared:

Checked:

23002

Infiltration Trench 2 (Unit 2)

NS

CK

Reference:

Output:

Vertical Sided System

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	Soil	6.9 mm/hr
FOS	Minor Inconvenience	3.00
q		0.002 m/hr

Equations Applied to Determine hmax

$$h_{\max} = a(e^{(-bD)} - 1) \quad (1)$$

Assume - uniform gravel (n)	0.30
-----------------------------	------

Area to be Drained	
A _d	241 m ²

where:

$$b = \frac{Pq}{A_d n} \quad (2)$$

and a is given by:

$$a = \frac{A_b}{P} - \frac{A_d i}{P q} \quad (3)$$

b=	0.017
Ab/P=	0.463

Infiltration Trench dimensions

Length	12.50 m
Width	1.00 m
Base Area (A _b)	12.500 m ²
Perimeter (P)	27.000 m

H_{max} Calculation

10 Year Return Period

Duration (D)	hmax	a
15.000 min	1.060	-256.604
30.000 min	1.333	-161.601
60.000 min	1.683	-102.457
120.000 min	2.109	-64.735
240.000 min	2.619	-40.868
360.000 min	2.951	-31.205

30 Year Return Period

Duration (D)	hmax	a
15.000 min	1.514	-366.509
30.000 min	1.893	-229.593
60.000 min	2.363	-143.904
120.000 min	2.928	-89.883
240.000 min	3.597	-56.120
360.000 min	4.023	-42.537

50 Year Return Period

Duration (D)	hmax	a
15.000 min	1.784	-431.707
30.000 min	2.216	-268.712
60.000 min	2.746	-167.189
120.000 min	3.391	-104.087
240.000 min	4.142	-64.619
360.000 min	4.625	-48.901

100 Year Return Period

Duration (D)	hmax	a
15.000 min	2.215	-536.024
30.000 min	2.738	-332.047
60.000 min	3.365	-204.911
120.000 min	4.127	-126.673
240.000 min	5.007	-78.124
360.000 min	5.565	-58.836

Vertical Sided System - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{1}{b} \log_e \left[\frac{h_{\max} + \frac{A_b}{P}}{h_{\max} + \frac{A_b}{P}} \right]$$

Event	Time to Empty
1 in 10 years	34.178 hrs
1 in 30 years	35.926 hrs
1 in 50 years	36.598 hrs
1 in 100 years	37.388 hrs

Infiltration System -- Overflow from French Drain

Return Period	Duration	Base Area (A _b)	h _{PROVIDED}	h _{max}	Q _{OVERFLOW} *
10 Years	60.000 min	12.500 m ²	0.750 m	2.951 m	0.203 l/sec
30 Years	60.000 min	12.500 m ²	0.750 m	4.023 m	0.423 l/sec
50 Years	60.000 min	12.500 m ²	0.750 m	4.625 m	0.581 l/sec
100 Years	60.000 min	12.500 m ²	0.750 m	5.565 m	0.885 l/sec

* Q_{OVERFLOW} is the averaged flow for the duration given.



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Project:

Design:

Telephone Log:

Calmount Rd, Ballymount - Internal Roads

Minutes:

Other Record:

Project No:

Element:

Prepared:

Checked:

23002

Infiltration Trench 2 (Unit 3)

NS

CK

Reference:

Output:

Calmount Rd, Ballymount - Extreme Rainfall Matrix

RP5 60min= 16.2 mm RP5 2d= 59.4 mm ANNUAL RAINFALL= 707.0 mm

RETURN PERIOD (YEARS)

DURATION	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3

Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)

Contributing Area Plan



Doherty Finegan Kelly

Consulting Structural & Civil Engineers,

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Dublin 9

Tel: 8301852 / Fax: 8602265

Project:

Calmount Rd, Ballymount - Internal Roads

Design:

Telephone Log:

Minutes:

Other Record:

Project No:

Element:

Prepared:

Checked:

23002

Infiltration Trench 2 (Unit 3)

NS

CK

Reference:

Output:

Vertical Sided System

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	Soil	6.6 mm/hr
FOS	Minor Inconvenience	3.00
q		0.002 m/hr

Equations Applied to Determine hmax

$$h_{\max} = a(e^{(-bD)} - 1) \quad (1)$$

where:

$$b = \frac{Pq}{A_b n} \quad (2)$$

and a is given by:

$$a = \frac{A_b - A_d i}{P - Pq} \quad (3)$$

b=	0.016
Ab/P=	0.464

Infiltration Trench dimensions

Length	12.90 m
Width	1.00 m
Base Area (A_b)	12.900 m ²
Perimeter (P)	27.800 m

H_{max} Calculation

10 Year Return Period

Duration (D)	hmax	a
15.000 min	1.143	-289.796
30.000 min	1.437	-182.526
60.000 min	1.815	-115.745
120.000 min	2.276	-73.153
240.000 min	2.830	-46.204
360.000 min	3.193	-35.293

30 Year Return Period

Duration (D)	hmax	a
15.000 min	1.632	-413.893
30.000 min	2.041	-259.298
60.000 min	2.549	-162.544
120.000 min	3.159	-101.548
240.000 min	3.885	-63.425
360.000 min	4.350	-48.088

50 Year Return Period

Duration (D)	hmax	a
15.000 min	1.922	-487.510
30.000 min	2.388	-303.468
60.000 min	2.961	-188.836
120.000 min	3.658	-117.586
240.000 min	4.473	-73.021
360.000 min	5.000	-55.274

100 Year Return Period

Duration (D)	hmax	a
15.000 min	2.387	-605.297
30.000 min	2.951	-374.981
60.000 min	3.629	-231.429
120.000 min	4.452	-143.089
240.000 min	5.407	-88.270
360.000 min	6.015	-66.492

Vertical Sided System - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{1}{b} \log_e \left[\frac{h_{\max} + \frac{A_b}{P}}{\frac{h_{\max}}{2} + \frac{A_b}{P}} \right]$$

Event	Time to Empty
1 in 10 years	36.301 hrs
1 in 30 years	38.037 hrs
1 in 50 years	38.703 hrs
1 in 100 years	39.483 hrs

Infiltration System -- Overflow from French Drain

Return Period	Duration	Base Area (A_b)	h_{PROVIDED}	h_{\max}	Q_{OVERFLOW}^*
10 Years	60.000 min	12.900 m ²	0.750 m	3.193 m	0.232 l/sec
30 Years	60.000 min	12.900 m ²	0.750 m	4.350 m	0.480 l/sec
50 Years	60.000 min	12.900 m ²	0.750 m	5.000 m	0.658 l/sec
100 Years	60.000 min	12.900 m ²	0.750 m	6.015 m	0.998 l/sec

* Q_{OVERFLOW} is the averaged flow for the duration given.

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	Project: Calmount Rd, Ballymount - Internal Roads			Design:	<input checked="" type="checkbox"/>	Telephone Log:	<input type="checkbox"/>		
Project No:	Element: Infiltration Trench 2 (Unit 4)			Minutes:	<input type="checkbox"/>	Other Record:	<input type="checkbox"/>		
23002				Prepared: NS		Checked: CK			
Reference:								Output:	
Calmount Rd, Ballymount - Extreme Rainfall Matrix									
RP5 60min= 16.2 mm		RP5 2d= 59.4 mm		ANNUAL RAINFALL= 707.0 mm					
RETURN PERIOD (YEARS)									
DURATION	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3
Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)									
Contributing Area Plan									



Doherty Finegan Kelly

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Project:

Calmount Rd, Ballymount - Internal Roads

Design:

Telephone Log:

Minutes:

Other Record:

Project No:

Element:

Prepared:

Checked:

23002

Infiltration Trench 2 (Unit 4)

NS

CK

Reference:

Output:

Vertical Sided System

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	Soil	830.6 mm/hr
FOS	Minor Inconvenience	3.00
q		0.277 m/hr

Equations Applied to Determine hmax

$$h_{\max} = a(e^{(-bD)} - 1) \quad (1)$$

Assume - uniform gravel (n)	0.30
-----------------------------	------

Area to be Drained	
A _D	136 m ²

where:

$$b = \frac{Pq}{A_D n} \quad (2)$$

and a is given by:

$$a = \frac{A_D}{P} - \frac{A_D j}{Pq} \quad (3)$$

b=	2.109
Ab/P=	0.438

Infiltration Trench dimensions

Length	7.00 m
Width	1.00 m
Base Area (A _b)	7.000 m ²
Perimeter (P)	16.000 m

H_{max} Calculation

10 Year Return Period

Duration (D)	hmax	a
15.000 min	0.654	-1.596
30.000 min	0.550	-0.845
60.000 min	0.331	-0.377
120.000 min	0.077	-0.078
240.000 min	0.000	0.111
360.000 min	0.000	0.187

30 Year Return Period

Duration (D)	hmax	a
15.000 min	1.010	-2.466
30.000 min	0.901	-1.382
60.000 min	0.619	-0.705
120.000 min	0.273	-0.277
240.000 min	0.010	-0.010
360.000 min	0.000	0.097

50 Year Return Period

Duration (D)	hmax	a
15.000 min	1.222	-2.981
30.000 min	1.103	-1.692
60.000 min	0.781	-0.889
120.000 min	0.384	-0.390
240.000 min	0.077	-0.077
360.000 min	0.000	0.047

100 Year Return Period

Duration (D)	hmax	a
15.000 min	1.560	-3.807
30.000 min	1.429	-2.193
60.000 min	1.043	-1.187
120.000 min	0.560	-0.568
240.000 min	0.184	-0.184
360.000 min	0.032	-0.032

Vertical Sided System - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{1}{b} \log_e \left[\frac{h_{\max} + \frac{A_b}{P}}{\frac{h_{\max}}{2} + \frac{A_b}{P}} \right]$$

Event	Time to Empty
1 in 10 years	0.169 hrs
1 in 30 years	0.203 hrs
1 in 50 years	0.218 hrs
1 in 100 years	0.235 hrs

Infiltration System -- Overflow from French Drain

Return Period	Duration	Base Area (A _b)	h _{PROVIDED}	h _{max}	Q _{OVERFLOW} *
10 Years	60.000 min	7.000 m ²	0.750 m	0.654 m	0.000 l/sec
30 Years	60.000 min	7.000 m ²	0.750 m	1.010 m	0.019 l/sec
50 Years	60.000 min	7.000 m ²	0.750 m	1.222 m	0.040 l/sec
100 Years	60.000 min	7.000 m ²	0.750 m	1.560 m	0.083 l/sec

* Q_{OVERFLOW} is the averaged flow for the duration given.



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Project:

Design:

Telephone Log:

Calmount Rd, Ballymount - Internal Roads

Minutes:

Other Record:

Project No:

Element:

Prepared:

Checked:

23002

Infiltration Trench 2 (Unit 6)

NS

CK

Reference:

Output:

Calmount Rd, Ballymount - Extreme Rainfall Matrix

RP5 60min= 16.2 mm RP5 2d= 59.4 mm ANNUAL RAINFALL= 707.0 mm

RETURN PERIOD (YEARS)

DURATION	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3

Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)

Contributing Area Plan



Doherty Finegan Kelly

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Tel: 8301852 / Fax: 8602265

Project:

Calmount Rd, Ballymount - Internal Roads

Design:



Telephone Log:



Minutes:



Other Record:



Project No:

Element:

Prepared:

Checked:

23002

Infiltration Trench 2 (Unit 6)

NS

CK

Reference:

Output:

Vertical Sided System

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	Soil	144.8 mm/hr
FOS	Minor Inconvenience	3.00
q		0.048 m/hr

Equations Applied to Determine hmax

$$h_{\max} = a(e^{(-bD)} - 1) \quad (1)$$

where:

$$b = \frac{Pq}{A_b n} \quad (2)$$

and a is given by:

$$a = \frac{A_b - A_d i}{P - Pq} \quad (3)$$

b=	0.331
Ab/P=	0.485

Infiltration Trench dimensions

Length	33.10 m
Width	1.00 m
Base Area (A_b)	33.100 m ²
Perimeter (P)	68.200 m

H_{max} Calculation

10 Year Return Period

Duration (D)	hmax	a
15.000 min	0.696	-8.751
30.000 min	0.815	-5.338
60.000 min	0.906	-3.213
120.000 min	0.900	-1.857
240.000 min	0.734	-1.000
360.000 min	0.563	-0.652

30 Year Return Period

Duration (D)	hmax	a
15.000 min	1.010	-12.700
30.000 min	1.188	-7.781
60.000 min	1.327	-4.702
120.000 min	1.338	-2.761
240.000 min	1.137	-1.548
360.000 min	0.915	-1.060

50 Year Return Period

Duration (D)	hmax	a
15.000 min	1.196	-15.042
30.000 min	1.403	-9.186
60.000 min	1.563	-5.538
120.000 min	1.585	-3.271
240.000 min	1.361	-1.853
360.000 min	1.112	-1.288

100 Year Return Period

Duration (D)	hmax	a
15.000 min	1.494	-18.791
30.000 min	1.751	-11.462
60.000 min	1.945	-6.894
120.000 min	1.979	-4.083
240.000 min	1.717	-2.338
360.000 min	1.420	-1.645

Vertical Sided System - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{1}{b} \log_e \left[\frac{h_{\max} + \frac{A_b}{P}}{\frac{h_{\max}}{2} + \frac{A_b}{P}} \right]$$

Event	Time to Empty
1 in 10 years	1.189 hrs
1 in 30 years	1.379 hrs
1 in 50 years	1.456 hrs
1 in 100 years	1.549 hrs

Infiltration System -- Overflow from French Drain

Return Period	Duration	Base Area (A_b)	h_{PROVIDED}	h_{\max}	Q_{OVERFLOW}^*
10 Years	60.000 min	33.100 m ²	0.750 m	0.906 m	0.038 l/sec
30 Years	60.000 min	33.100 m ²	0.750 m	1.338 m	0.201 l/sec
50 Years	60.000 min	33.100 m ²	0.750 m	1.585 m	0.332 l/sec
100 Years	60.000 min	33.100 m ²	0.750 m	1.979 m	0.598 l/sec

* Q_{OVERFLOW} is the averaged flow for the duration given.

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Project: Calmount Rd, Ballymount - Internal Roads				Design: <input checked="" type="checkbox"/>	<input type="checkbox"/>	Telephone Log:		<input type="checkbox"/>	
				Minutes: <input type="checkbox"/>	<input type="checkbox"/>	Other Record:		<input type="checkbox"/>	
Project No: 23002	Element: Infiltration Trench 3 (Unit 2)			Prepared: NS			Checked: CK		
Reference:									Output:
Calmount Rd, Ballymount - Extreme Rainfall Matrix									
RP5 60min= 16.2 mm		RP5 2d= 59.4 mm		ANNUAL RAINFALL= 707.0 mm					
RETURN PERIOD (YEARS)									
DURATION	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3
Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)									
Contributing Area Plan									



Doherty Finegan Kelly

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Tel: 8301852 / Fax: 8602265

Project:

Calmount Rd, Ballymount - Internal Roads

Design:



Telephone Log:



Minutes:



Other Record:



Project No:

Element:

Prepared:

Checked:

23002

Infiltration Trench 3 (Unit 2)

NS

CK

Reference: Output:

Vertical Sided System

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	Soil	6.9 mm/hr
FOS	Minor Inconvenience	3.00
q		0.002 m/hr

Equations Applied to Determine hmax

$$h_{\max} = a(e^{(-bD)} - 1) \quad (1)$$

where:

$$b = \frac{Pq}{A_p n} \quad (2)$$

and a is given by:

$$a = \frac{A_b}{P} - \frac{A_p i}{P q} \quad (3)$$

b=	0.016
Ab/P=	0.468

Infiltration Trench dimensions

Length	14.40 m
Width	1.00 m
Base Area (A_b)	14.400 m ²
Perimeter (P)	30.800 m

H_{max} Calculation

10 Year Return Period

Duration (D)	hmax	a
15.000 min	1.482	-362.338
30.000 min	1.864	-228.257
60.000 min	2.355	-144.786
120.000 min	2.954	-91.548
240.000 min	3.674	-57.864
360.000 min	4.144	-44.226

30 Year Return Period

Duration (D)	hmax	a
15.000 min	2.117	-517.450
30.000 min	2.647	-324.217
60.000 min	3.306	-203.282
120.000 min	4.099	-127.040
240.000 min	5.040	-79.389
360.000 min	5.643	-60.219

50 Year Return Period

Duration (D)	hmax	a
15.000 min	2.493	-609.466
30.000 min	3.098	-379.426
60.000 min	3.841	-236.145
120.000 min	4.746	-147.086
240.000 min	5.802	-91.384
360.000 min	6.484	-69.202

100 Year Return Period

Duration (D)	hmax	a
15.000 min	3.096	-756.691
30.000 min	3.828	-468.813
60.000 min	4.707	-289.382
120.000 min	5.774	-178.963
240.000 min	7.012	-110.444
360.000 min	7.798	-83.223

Vertical Sided System - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{1}{b} \log_e \left[\frac{h_{\max} + \frac{A_b}{P}}{h_{\max} + \frac{A_b}{P}} \right]$$

Event	Time to Empty
1 in 10 years	36.381 hrs
1 in 30 years	37.774 hrs
1 in 50 years	38.301 hrs
1 in 100 years	38.915 hrs

Infiltration System -- Overflow from French Drain

Return Period	Duration	Base Area (A_b)	h_{PROVIDED}	h_{\max}	Q_{OVERFLOW}^*
10 Years	60.000 min	14.400 m ²	0.750 m	4.144 m	0.360 l/sec
30 Years	60.000 min	14.400 m ²	0.750 m	5.643 m	0.728 l/sec
50 Years	60.000 min	14.400 m ²	0.750 m	6.484 m	0.991 l/sec
100 Years	60.000 min	14.400 m ²	0.750 m	7.798 m	1.492 l/sec

* Q_{OVERFLOW} is the averaged flow for the duration given.



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Project:

Design:

Telephone Log:

Calmount Rd, Ballymount - Internal Roads

Minutes:

Other Record:

Project No:

Element:

Prepared:

Checked:

23002

Infiltration Trench 3 (Unit 3)

NS

CK

Reference:

Output:

Calmount Rd, Ballymount - Extreme Rainfall Matrix

RP5 60min= 16.2 mm RP5 2d= 59.4 mm ANNUAL RAINFALL= 707.0 mm

RETURN PERIOD (YEARS)

DURATION	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3

Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)

Contributing Area Plan



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Project:

Calmount Rd, Ballymount - Internal Roads

Design:

Telephone Log:

Minutes:

Other Record:

Project No:

Element:

Prepared:

Checked:

23002

Infiltration Trench 3 (Unit 3)

NS

CK

Reference:

Output:

Vertical Sided System

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	Soil	6.9 mm/hr
FOS	Minor Inconvenience	3.00
q		0.002 m/hr

Equations Applied to Determine hmax

$$h_{\max} = a(e^{(-bD)} - 1) \quad (1)$$

where:

$$b = \frac{Pq}{A_b n} \quad (2)$$

and a is given by:

$$a = \frac{A_b - A_d i}{P - Pq} \quad (3)$$

b=	0.016
Ab/P=	0.482

Infiltration Trench dimensions

Length	27.10 m
Width	1.00 m
Base Area (A_b)	27.100 m ²
Perimeter (P)	56.200 m

H_{max} Calculation

10 Year Return Period

Duration (D)	hmax	a
15.000 min	0.787	-198.351
30.000 min	0.989	-124.869
60.000 min	1.248	-79.123
120.000 min	1.563	-49.946
240.000 min	1.940	-31.486
360.000 min	2.185	-24.012

30 Year Return Period

Duration (D)	hmax	a
15.000 min	1.124	-283.359
30.000 min	1.405	-177.459
60.000 min	1.754	-111.181
120.000 min	2.172	-69.397
240.000 min	2.667	-43.283
360.000 min	2.982	-32.777

50 Year Return Period

Duration (D)	hmax	a
15.000 min	1.324	-333.787
30.000 min	1.645	-207.716
60.000 min	2.038	-129.191
120.000 min	2.516	-80.384
240.000 min	3.072	-49.856
360.000 min	3.430	-37.699

100 Year Return Period

Duration (D)	hmax	a
15.000 min	1.644	-414.473
30.000 min	2.033	-256.704
60.000 min	2.498	-158.368
120.000 min	3.063	-97.854
240.000 min	3.716	-60.302
360.000 min	4.129	-45.384

Vertical Sided System - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{1}{b} \log_e \left[\frac{h_{\max} + \frac{A_b}{P}}{\frac{h_{\max}}{2} + \frac{A_b}{P}} \right]$$

Event	Time to Empty
1 in 10 years	33.143 hrs
1 in 30 years	35.400 hrs
1 in 50 years	36.286 hrs
1 in 100 years	37.341 hrs

Infiltration System -- Overflow from French Drain

Return Period	Duration	Base Area (A_b)	h_{PROVIDED}	h_{\max}	Q_{OVERFLOW}^*
10 Years	60.000 min	27.100 m ²	0.750 m	2.185 m	0.286 l/sec
30 Years	60.000 min	27.100 m ²	0.750 m	2.982 m	0.625 l/sec
50 Years	60.000 min	27.100 m ²	0.750 m	3.430 m	0.872 l/sec
100 Years	60.000 min	27.100 m ²	0.750 m	4.129 m	1.346 l/sec

* Q_{OVERFLOW} is the averaged flow for the duration given.



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Project:

Design:

Telephone Log:

Calmount Rd, Ballymount - Internal Roads

Minutes:

Other Record:

Project No:

Element:

Prepared:

Checked:

23002

Infiltration Trench 3 (Unit 6)

NS

CK

Reference:

Output:

Calmount Rd, Ballymount - Extreme Rainfall Matrix

RP5 60min= 16.2 mm RP5 2d= 59.4 mm ANNUAL RAINFALL= 707.0 mm

RETURN PERIOD (YEARS)

DURATION	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3

Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)

Contributing Area Plan



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Project:

Calmount Rd, Ballymount - Internal Roads

Design:

Telephone Log:

Minutes:

Other Record:

Project No:

Element:

Prepared:

Checked:

23002

Infiltration Trench 3 (Unit 6)

NS

CK

Reference:

Output:

Vertical Sided System

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	Soil	74.9 mm/hr
FOS	Minor Inconvenience	3.00
q		0.025 m/hr

Equations Applied to Determine hmax

$$h_{\max} = a(e^{(-bD)} - 1) \quad (1)$$

Assume - uniform gravel (n)	0.30
-----------------------------	------

Area to be Drained	
A _b	385 m ²

where:

$$b = \frac{Pq}{A_b n} \quad (2)$$

and a is given by:

$$a = \frac{A_b - A_d i}{P - Pq} \quad (3)$$

b=	0.177
Ab/P=	0.469

H_{max} Calculation

10 Year Return Period

Duration (D)	hmax	a
15.000 min	1.338	-30.864
30.000 min	1.636	-19.284
60.000 min	1.962	-12.075
120.000 min	2.233	-7.477
240.000 min	2.321	-4.568
360.000 min	2.220	-3.391

30 Year Return Period

Duration (D)	hmax	a
15.000 min	1.919	-44.260
30.000 min	2.339	-27.571
60.000 min	2.783	-17.127
120.000 min	3.148	-10.543
240.000 min	3.265	-6.427
360.000 min	3.125	-4.772

50 Year Return Period

Duration (D)	hmax	a
15.000 min	2.264	-52.207
30.000 min	2.744	-32.340
60.000 min	3.244	-19.965
120.000 min	3.665	-12.274
240.000 min	3.791	-7.463
360.000 min	3.633	-5.548

100 Year Return Period

Duration (D)	hmax	a
15.000 min	2.815	-64.921
30.000 min	3.399	-40.059
60.000 min	3.991	-24.563
120.000 min	4.487	-15.027
240.000 min	4.628	-9.109
360.000 min	4.426	-6.758

Vertical Sided System - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{1}{b} \log_e \left[\frac{h_{\max} + \frac{A_b}{P}}{\frac{h_{\max}}{2} + \frac{A_b}{P}} \right]$$

Event	Time to Empty
1 in 10 years	3.032 hrs
1 in 30 years	3.241 hrs
1 in 50 years	3.320 hrs
1 in 100 years	3.412 hrs

Infiltration System -- Overflow from French Drain

Return Period	Duration	Base Area (A _b)	h _{PROVIDED}	h _{max}	Q _{OVERFLOW} *
10 Years	60.000 min	15.300 m ²	0.750 m	2.321 m	0.177 l/sec
30 Years	60.000 min	15.300 m ²	0.750 m	3.265 m	0.398 l/sec
50 Years	60.000 min	15.300 m ²	0.750 m	3.791 m	0.558 l/sec
100 Years	60.000 min	15.300 m ²	0.750 m	4.628 m	0.872 l/sec

* Q_{OVERFLOW} is the averaged flow for the duration given.



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Project:

Design:

Telephone Log:

Calmount Rd, Ballymount - Internal Roads

Minutes:

Other Record:

Project No:

Element:

Prepared:

Checked:

23002

Infiltration Trench 4 (Unit 2)

NS

CK

Reference:

Output:

Calmount Rd, Ballymount - Extreme Rainfall Matrix

RP5 60min= 16.2 mm RP5 2d= 59.4 mm ANNUAL RAINFALL= 707.0 mm

RETURN PERIOD (YEARS)

DURATION	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3

Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)

Contributing Area Plan



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Project:

Calmount Rd, Ballymount - Internal Roads

Design:

Telephone Log:

Minutes:

Other Record:

Project No:

Element:

Prepared:

Checked:

23002

Infiltration Trench 4 (Unit 2)

NS

CK

Reference:

Output:

Vertical Sided System

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	Soil	77.1 mm/hr
FOS	Minor Inconvenience	3.00
q		0.026 m/hr

Equations Applied to Determine hmax

$$h_{\max} = a(e^{(-bD)} - 1) \quad (1)$$

Assume - uniform gravel (n)	0.30
-----------------------------	------

Area to be Drained	
A _b	366 m ²

where:

$$b = \frac{Pq}{A_b n} \quad (2)$$

and a is given by:

$$a = \frac{A_b - A_d i}{P - Pq} \quad (3)$$

b=	0.181
Ab/P=	0.473

H_{max} Calculation

10 Year Return Period

Duration (D)	hmax	a
15.000 min	1.089	-24.615
30.000 min	1.327	-15.343
60.000 min	1.584	-9.571
120.000 min	1.788	-5.890
240.000 min	1.834	-3.560
360.000 min	1.734	-2.617

30 Year Return Period

Duration (D)	hmax	a
15.000 min	1.563	-35.342
30.000 min	1.901	-21.979
60.000 min	2.254	-13.616
120.000 min	2.534	-8.344
240.000 min	2.601	-5.049
360.000 min	2.466	-3.723

50 Year Return Period

Duration (D)	hmax	a
15.000 min	1.845	-41.705
30.000 min	2.232	-25.797
60.000 min	2.630	-15.889
120.000 min	2.955	-9.730
240.000 min	3.028	-5.878
360.000 min	2.878	-4.344

100 Year Return Period

Duration (D)	hmax	a
15.000 min	2.295	-51.886
30.000 min	2.766	-31.978
60.000 min	3.239	-19.570
120.000 min	3.624	-11.935
240.000 min	3.707	-7.196
360.000 min	3.520	-5.314

Vertical Sided System - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{1}{b} \log_e \left[\frac{h_{\max} + \frac{A_b}{P}}{\frac{h_{\max}}{2} + \frac{A_b}{P}} \right]$$

Event	Time to Empty
1 in 10 years	2.799 hrs
1 in 30 years	3.039 hrs
1 in 50 years	3.130 hrs
1 in 100 years	3.238 hrs

Infiltration System -- Overflow from French Drain

Return Period	Duration	Base Area (A _b)	h _{PROVIDED}	h _{max}	Q _{OVERFLOW} *
10 Years	60.000 min	17.800 m ²	0.750 m	1.834 m	0.142 l/sec
30 Years	60.000 min	17.800 m ²	0.750 m	2.601 m	0.340 l/sec
50 Years	60.000 min	17.800 m ²	0.750 m	3.028 m	0.487 l/sec
100 Years	60.000 min	17.800 m ²	0.750 m	3.707 m	0.774 l/sec

* Q_{OVERFLOW} is the averaged flow for the duration given.



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Project:

Design:

Telephone Log:

Calmount Rd, Ballymount - Internal Roads

Minutes:

Other Record:

Project No:

Element:

Prepared:

Checked:

23002

Infiltration Trench 4 (Unit 3)

NS

CK

Reference:

Output:

Calmount Rd, Ballymount - Extreme Rainfall Matrix

RP5 60min= 16.2 mm RP5 2d= 59.4 mm ANNUAL RAINFALL= 707.0 mm

RETURN PERIOD (YEARS)

DURATION	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3

Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)

Contributing Area Plan



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Project:

Calmount Rd, Ballymount - Internal Roads

Design:



Telephone Log:



Minutes:



Other Record:



Project No:

Element:

Prepared:

Checked:

23002

Infiltration Trench 4 (Unit 3)

NS

CK

Reference:

Output:

Vertical Sided System

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	Soil	105.0 mm/hr
FOS	Minor Inconvenience	3.00
q		0.035 m/hr

Equations Applied to Determine hmax

$$h_{\max} = a(e^{(-bD)} - 1) \quad (1)$$

Assume - uniform gravel (n)	0.30
-----------------------------	------

Area to be Drained	
A _b	559 m ²

where:

$$b = \frac{Pq}{A_b n} \quad (2)$$

and a is given by:

$$a = \frac{A_b - A_d i}{P - Pq} \quad (3)$$

b=	0.239
Ab/P=	0.488

H_{max} Calculation

10 Year Return Period

Duration (D)	hmax	a
15.000 min	0.693	-11.958
30.000 min	0.829	-7.358
60.000 min	0.955	-4.495
120.000 min	1.014	-2.668
240.000 min	0.931	-1.513
360.000 min	0.796	-1.045

30 Year Return Period

Duration (D)	hmax	a
15.000 min	1.002	-17.280
30.000 min	1.199	-10.650
60.000 min	1.382	-6.502
120.000 min	1.476	-3.886
240.000 min	1.386	-2.251
360.000 min	1.214	-1.594

50 Year Return Period

Duration (D)	hmax	a
15.000 min	1.185	-20.436
30.000 min	1.413	-12.544
60.000 min	1.622	-7.629
120.000 min	1.738	-4.574
240.000 min	1.639	-2.663
360.000 min	1.448	-1.902

100 Year Return Period

Duration (D)	hmax	a
15.000 min	1.478	-25.487
30.000 min	1.758	-15.611
60.000 min	2.010	-9.455
120.000 min	2.153	-5.667
240.000 min	2.041	-3.317
360.000 min	1.815	-2.383

Vertical Sided System - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{1}{b} \log_e \left[\frac{h_{\max} + \frac{A_b}{P}}{\frac{h_{\max}}{2} + \frac{A_b}{P}} \right]$$

Event	Time to Empty
1 in 10 years	1.723 hrs
1 in 30 years	1.972 hrs
1 in 50 years	2.071 hrs
1 in 100 years	2.191 hrs

Infiltration System -- Overflow from French Drain

Return Period	Duration	Base Area (A _b)	h _{PROVIDED}	h _{max}	Q _{OVERFLOW} *
10 Years	60.000 min	41.500 m ²	0.750 m	1.014 m	0.081 l/sec
30 Years	60.000 min	41.500 m ²	0.750 m	1.476 m	0.312 l/sec
50 Years	60.000 min	41.500 m ²	0.750 m	1.738 m	0.492 l/sec
100 Years	60.000 min	41.500 m ²	0.750 m	2.153 m	0.856 l/sec

* Q_{OVERFLOW} is the averaged flow for the duration given.

	Doherty Finegan Kelly <i>Consulting Structural & Civil Engineers,</i>		Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265						
	Project: Calmount Rd, Ballymount - Internal Roads			Design:	<input checked="" type="checkbox"/>	Telephone Log:	<input type="checkbox"/>		
Project No:	Element:			Minutes:	<input type="checkbox"/>	Other Record:	<input type="checkbox"/>		
23002	Infiltration Trench 4 (Unit 6)			Prepared:		Checked:			
Reference:	NS						CK		
							Output:		
Calmount Rd, Ballymount - Extreme Rainfall Matrix									
RP5 60min=		16.2 mm	RP5 2d=		59.4 mm	ANNUAL RAINFALL=			707.0 mm
RETURN PERIOD (YEARS)									
DURATION	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3
Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)									
Contributing Area Plan									



Doherty Finegan Kelly
Consulting Structural & Civil Engineers,
Botanic Court, 30 Botanic Road, Glasnevin,
Dublin 9
Tel: 8301852 / Fax: 8602265

Project:

Design:

Telephone Log:

Calmount Rd, Ballymount - Internal Roads

Minutes:

Other Record:

Project No:

Element:

Prepared:

Checked:

23002

Infiltration Trench 4 (Unit 6)

NS

CK

Reference:

Output:

Vertical Sided System

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	Soil	54.4 mm/hr
FOS	Minor Inconvenience	3.00
q		0.018 m/hr

Equations Applied to Determine hmax

$$h_{\max} = a(e^{(-bD)} - 1) \quad (1)$$

Assume - uniform gravel (n)	0.30
-----------------------------	------

where:

$$b = \frac{Pq}{A_p n} \quad (2)$$

and a is given by:

$$a = \frac{A_b}{P} - \frac{A_p i}{P q} \quad (3)$$

b=	0.124
Ab/P=	0.487

Infiltration Trench dimensions

Length	36.90 m
Width	1.00 m
Base Area (A_b)	36.900 m ²
Perimeter (P)	75.800 m

H_{max} Calculation

10 Year Return Period

Duration (D)	hmax	a
15.000 min	0.776	-25.392
30.000 min	0.953	-15.828
60.000 min	1.153	-9.874
120.000 min	1.336	-6.077
240.000 min	1.438	-3.674
360.000 min	1.419	-2.701

30 Year Return Period

Duration (D)	hmax	a
15.000 min	1.114	-36.456
30.000 min	1.365	-22.673
60.000 min	1.640	-14.047
120.000 min	1.893	-8.608
240.000 min	2.039	-5.209
360.000 min	2.018	-3.842

50 Year Return Period

Duration (D)	hmax	a
15.000 min	1.315	-43.020
30.000 min	1.602	-26.611
60.000 min	1.914	-16.391
120.000 min	2.207	-10.038
240.000 min	2.374	-6.065
360.000 min	2.355	-4.483

100 Year Return Period

Duration (D)	hmax	a
15.000 min	1.636	-53.522
30.000 min	1.986	-32.987
60.000 min	2.357	-20.188
120.000 min	2.707	-12.312
240.000 min	2.906	-7.425
360.000 min	2.880	-5.483

Vertical Sided System - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{1}{b} \log_e \left[\frac{h_{\max} + \frac{A_b}{P}}{h_{\max} + \frac{A_b}{P}} \right]$$

Event	Time to Empty
1 in 10 years	3.767 hrs
1 in 30 years	4.163 hrs
1 in 50 years	4.317 hrs
1 in 100 years	4.503 hrs

Infiltration System -- Overflow from French Drain

Return Period	Duration	Base Area (A_b)	h_{PROVIDED}	h_{\max}	Q_{OVERFLOW}^*
10 Years	60.000 min	36.900 m ²	0.750 m	1.438 m	0.187 l/sec
30 Years	60.000 min	36.900 m ²	0.750 m	2.039 m	0.492 l/sec
50 Years	60.000 min	36.900 m ²	0.750 m	2.374 m	0.719 l/sec
100 Years	60.000 min	36.900 m ²	0.750 m	2.906 m	1.170 l/sec

* Q_{OVERFLOW} is the averaged flow for the duration given.

	<p>Doherty Finegan Kelly Consulting Structural & Civil Engineers, Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265</p>								
	Project: Calmount Rd, Ballymount - Internal Roads				Design: <input checked="" type="checkbox"/> <input type="checkbox"/>	Telephone Log: <input type="checkbox"/>			
Project No: 23002	Element: Infiltration Trench 5 (Unit 3)				Minutes: <input type="checkbox"/>	Other Record: <input type="checkbox"/>			
Reference:	Prepared: NS							Checked: CK	
								Output:	
Calmount Rd, Ballymount - Extreme Rainfall Matrix									
RP5 60min= 16.2 mm		RP5 2d= 59.4 mm		ANNUAL RAINFALL= 707.0 mm					
RETURN PERIOD (YEARS)									
DURATION	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3
Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)									
Contributing Area Plan									



Doherty Finegan Kelly

Consulting Structural & Civil Engineers,

Botanic Court, 30 Botanic Road, Glasnevin,

Dublin 9

Tel: 8301852 / Fax: 8602265

Project:

Calmount Rd, Ballymount - Internal Roads

Design:



Telephone Log:



Minutes:



Other Record:



Project No:

Element:

Prepared:

Checked:

23002

Infiltration Trench 5 (Unit 3)

NS

CK

Reference:

Output:

Vertical Sided System

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	Soil	409.7 mm/hr
FOS	Minor Inconvenience	3.00
q		0.137 m/hr

Equations Applied to Determine hmax

$$h_{\max} = a(e^{(-bD)} - 1) \quad (1)$$

Assume - uniform gravel (n)	0.30
-----------------------------	------

Area to be Drained	
A _D	653 m ²

where:

$$b = \frac{Pq}{A_D n} \quad (2)$$

and a is given by:

$$a = \frac{A_b}{P} - \frac{A_b j}{Pq} \quad (3)$$

b=	0.929
Ab/P=	0.490

H_{max} Calculation

10 Year Return Period

Duration (D)	hmax	a
15.000 min	0.569	-2.742
30.000 min	0.575	-1.548
60.000 min	0.487	-0.804
120.000 min	0.278	-0.330
240.000 min	0.029	-0.030
360.000 min	0.000	0.092

30 Year Return Period

Duration (D)	hmax	a
15.000 min	0.855	-4.124
30.000 min	0.893	-2.403
60.000 min	0.802	-1.325
120.000 min	0.545	-0.646
240.000 min	0.216	-0.222
360.000 min	0.051	-0.051

50 Year Return Period

Duration (D)	hmax	a
15.000 min	1.025	-4.944
30.000 min	1.076	-2.894
60.000 min	0.979	-1.618
120.000 min	0.696	-0.825
240.000 min	0.320	-0.328
360.000 min	0.130	-0.131

100 Year Return Period

Duration (D)	hmax	a
15.000 min	1.297	-6.255
30.000 min	1.372	-3.691
60.000 min	1.266	-2.092
120.000 min	0.936	-1.109
240.000 min	0.486	-0.498
360.000 min	0.255	-0.256

Vertical Sided System - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{1}{b} \log_e \left[\frac{h_{\max} + \frac{A_b}{P}}{\frac{h_{\max}}{2} + \frac{A_b}{P}} \right]$$

Event	Time to Empty
1 in 10 years	0.339 hrs
1 in 30 years	0.420 hrs
1 in 50 years	0.453 hrs
1 in 100 years	0.494 hrs

Infiltration System -- Overflow from French Drain

Return Period	Duration	Base Area (A _b)	h _{PROVIDED}	h _{max}	Q _{OVERFLOW} *
10 Years	60.000 min	48.000 m ²	0.750 m	0.575 m	0.000 l/sec
30 Years	60.000 min	48.000 m ²	0.750 m	0.893 m	0.071 l/sec
50 Years	60.000 min	48.000 m ²	0.750 m	1.076 m	0.188 l/sec
100 Years	60.000 min	48.000 m ²	0.750 m	1.372 m	0.439 l/sec

* Q_{OVERFLOW} is the averaged flow for the duration given.

	<p>Doherty Finegan Kelly Consulting Structural & Civil Engineers, Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265</p>								
Project: Calmount Rd, Ballymount - Internal Roads				Design: <input checked="" type="checkbox"/> <input type="checkbox"/>	Telephone Log: <input type="checkbox"/>				
				Minutes: <input type="checkbox"/>	Other Record: <input type="checkbox"/>				
Project No: 23002	Element: Infiltration Trench 5 (Unit 6)			Prepared: NS			Checked: CK		
Reference:								Output:	
Calmount Rd, Ballymount - Extreme Rainfall Matrix									
RP5 60min= 16.2 mm		RP5 2d= 59.4 mm		ANNUAL RAINFALL= 707.0 mm					
RETURN PERIOD (YEARS)									
DURATION	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3
Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)									
Contributing Area Plan									



Doherty Finegan Kelly

Consulting Structural & Civil Engineers,

Botanic Court, 30 Botanic Road, Glasnevin,

Dublin 9

Tel: 8301852 / Fax: 8602265

Project:

Calmount Rd, Ballymount - Internal Roads

Design: Telephone Log: Minutes: Other Record:

Project No:

Element:

Prepared:

Checked:

23002

Infiltration Trench 5 (Unit 6)

NS

CK

Reference: Output:

Vertical Sided System

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	Soil	285.2 mm/hr
FOS	Minor Inconvenience	3.00
q		0.095 m/hr

Equations Applied to Determine hmax

$$h_{\max} = a(e^{(-bD)} - 1) \quad (1)$$

Assume - uniform gravel (n)	0.30
-----------------------------	------

where:

$$b = \frac{Pq}{A_p n} \quad (2)$$

and a is given by:

$$a = \frac{A_b}{P} - \frac{A_b j}{Pq} \quad (3)$$

b=	0.644
Ab/P=	0.492

Infiltration Trench dimensions

Length	60.00 m
Width	1.00 m
Base Area (A_b)	60.000 m ²
Perimeter (P)	122.000 m

H_{max} Calculation

10 Year Return Period

Duration (D)	hmax	a
15.000 min	0.562	-3.775
30.000 min	0.605	-2.198
60.000 min	0.578	-1.216
120.000 min	0.428	-0.590
240.000 min	0.179	-0.194
360.000 min	0.033	-0.034

30 Year Return Period

Duration (D)	hmax	a
15.000 min	0.833	-5.599
30.000 min	0.916	-3.326
60.000 min	0.904	-1.904
120.000 min	0.730	-1.008
240.000 min	0.413	-0.447
360.000 min	0.217	-0.222

50 Year Return Period

Duration (D)	hmax	a
15.000 min	0.994	-6.681
30.000 min	1.095	-3.975
60.000 min	1.088	-2.291
120.000 min	0.901	-1.243
240.000 min	0.544	-0.588
360.000 min	0.321	-0.327

100 Year Return Period

Duration (D)	hmax	a
15.000 min	1.252	-8.412
30.000 min	1.384	-5.027
60.000 min	1.385	-2.917
120.000 min	1.172	-1.618
240.000 min	0.751	-0.812
360.000 min	0.482	-0.492

Vertical Sided System - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{1}{b} \log_e \left[\frac{h_{\max} + \frac{A_b}{P}}{\frac{h_{\max}}{2} + \frac{A_b}{P}} \right]$$

Event	Time to Empty
1 in 10 years	0.501 hrs
1 in 30 years	0.611 hrs
1 in 50 years	0.657 hrs
1 in 100 years	0.715 hrs

Infiltration System -- Overflow from French Drain

Return Period	Duration	Base Area (A_b)	h_{PROVIDED}	h_{\max}	Q_{OVERFLOW}^*
10 Years	60.000 min	60.000 m ²	0.750 m	0.605 m	0.000 l/sec
30 Years	60.000 min	60.000 m ²	0.750 m	0.916 m	0.103 l/sec
50 Years	60.000 min	60.000 m ²	0.750 m	1.095 m	0.248 l/sec
100 Years	60.000 min	60.000 m ²	0.750 m	1.385 m	0.560 l/sec

* Q_{OVERFLOW} is the averaged flow for the duration given.

STORMTECH Stormwater Management System Design Tool

ver: Aug15

PROJECT REF: Calmount Rd, Ballymount - Internal Roads

LOCATION: StormTech Trench #1

DATE: 14.09.2023

CREATED BY: SG

SYSTEM PARAMETERS

Required Total Storage		m ³
Stormtech chamber model	SC740	
Filtration Permeable Geo or Impermeable Geo	Filter geo	
Number of Isolator Rows (IR)	1	

SITE PARAMETERS

Stone Porosity	40%	
Excavation Batter Angle (degrees)	60°	Minimum Requirement
Stone Above Chambers	0.2 m	0.15
Stone Below Chambers (Long-Term Storage)	0 m	0.15 <i>Adjust to minimum</i>
In-between Row Spacing	0.15 m	0.15
Additional Storage outside Excavation. E.g manholes, Header Pipe	0 m ³	

HEADER PIPE

Is Header pipe required within excavation	No
Orientation of Header Pipe	Perp to IR
Diameter of Header Pipe	0 m
Length of Header Pipe	0 m

CHAMBER SYSTEM DIMENSIONS

	Calculated	Adopted
Number of Rows	2 ea	
Number of units per Row	22 ea	
System Installed Storage Depth (effective storage depth)	0.960	1.06 m
Tank overall installed Width at base	3.34	3.35 m
Tank overall installed Length at Base	48.44	48.5 m
Total Effective System Storage	107.9	108.1 m ³

STORMTECH SYSTEM DETAIL

StormTech Chamber Model	SC740
Unit Width	1.295 m
Unit Length	2.17 m
Unit Height	0.76 m
Min Cover Over System	0.3 m
Max Cover Over Chamber	2.4 m
Chamber Internal Storage Vol.	1.3 m ³
Header Pipe Internal Storage Vol in Excavation	0.0 m ³

STONE AND EXCAVATION DETAIL

Volume of Dig for System	184 m ³
Width at base	3.35 m
Width at top	4.46 m
Length at base	48.50 m
Length at top	49.61 m
Depth Of System	0.96 m
Area of Dig at Base of System	162 m ²
Area of Dig at Top of System	221 m ²
Void Ratio	59%
Stone Requirement - m ³	126 m ³
Stone Requirement - tonne	207 tonne



Doherty Finegan Kelly
Consulting Structural & Civil Engineers

Project:

Calmount Rd, Ballymount - Internal Roads

Botanic Court, 30 Botanic Road,
Glasnevin, Dublin 9.
Tel: 8301852 / Fax: 8602265

Design:	<input checked="" type="checkbox"/>	Telephone Log:	<input type="checkbox"/>
Minutes	<input type="checkbox"/>	Other Record::	<input type="checkbox"/>
Prepared:		Checked:	
NS		SG/CK	

Project No:

Element:

23002

Overflow From Infiltration Trenches

Output:

Site Catchment Characteristics

Element	Return period=100yr												
	Duration [min]	2	5	10	15	30	60	120	240	360	720	1440	2880
Infiltration Trench 1 (Cafe)	35.31	14.12	7.06	4.71	2.35	1.18	0.59	0.29	0.20	0.10	0.07	0.02	0.02
Infiltration Trench 2 (Cafe)	12.21	4.88	2.44	1.63	0.81	0.41	0.20	0.10	0.07	0.03	0.02	0.01	0.01
Infiltration Trench 1 (Unit 1)	15.96	6.38	3.19	2.13	1.06	0.53	0.27	0.13	0.09	0.04	0.03	0.01	0.01
Infiltration Trench 2 (Unit 1)	34.95	13.98	6.99	4.66	2.33	1.17	0.58	0.29	0.19	0.10	0.06	0.02	0.02
Infiltration Trench 2 (Unit 2)	26.55	10.62	5.31	3.54	1.77	0.89	0.44	0.22	0.15	0.07	0.05	0.02	0.01
Infiltration Trench 3 (Unit 2)	44.76	17.90	8.95	5.97	2.98	1.49	0.75	0.37	0.25	0.12	0.08	0.03	0.02
Infiltration Trench 4 (Unit 2)	23.22	9.29	4.64	3.10	1.55	0.77	0.39	0.19	0.13	0.06	0.04	0.02	0.01
Infiltration Trench 2 (Unit 3)	29.94	11.98	5.99	3.99	2.00	1.00	0.50	0.25	0.17	0.08	0.06	0.02	0.01
Infiltration Trench 3 (Unit 3)	40.38	16.15	8.08	5.38	2.69	1.35	0.67	0.34	0.22	0.11	0.07	0.03	0.02
Infiltration Trench 4 (Unit 3)	25.68	10.27	5.14	3.42	1.71	0.86	0.43	0.21	0.14	0.07	0.05	0.02	0.01
Infiltration Trench 2 (Unit 6)	17.94	7.18	3.59	2.39	1.20	0.60	0.30	0.15	0.10	0.05	0.03	0.01	0.01
Infiltration Trench 3 (Unit 6)	26.16	10.46	5.23	3.49	1.74	0.87	0.44	0.22	0.15	0.07	0.05	0.02	0.01
Infiltration Trench 4 (Unit 6)	35.10	14.04	7.02	4.68	2.34	1.17	0.59	0.29	0.20	0.10	0.07	0.02	0.02
Infiltration Trench 1 TP (Unit 4)	32.19	12.88	6.44	4.29	2.15	1.07	0.54	0.27	0.18	0.09	0.06	0.02	0.01
Infiltration Trench 1 TP (Unit 5C)	8.58	3.43	1.72	1.14	0.57	0.29	0.14	0.07	0.05	0.02	0.02	0.01	0.00
Infiltration Trench 2 TP (Unit 4)	2.49	1.00	0.50	0.33	0.17	0.08	0.04	0.02	0.01	0.01	0.00	0.00	0.00
Infiltration Trench 5 TP (Unit 3)	13.17	5.27	2.63	1.76	0.88	0.44	0.22	0.11	0.07	0.04	0.02	0.01	0.01
Infiltration Trench 5 TP (Unit 6)	16.80	6.72	3.36	2.24	1.12	0.56	0.28	0.14	0.09	0.05	0.03	0.01	0.01
Total Overflow Discharge (Q) [l/sec]	441.39	176.56	88.28	58.85	29.43	14.71	7.36	3.68	2.45	1.23	0.82	0.31	0.20



Doherty Finegan Kelly
Consulting Structural & Civil Engineers

Botanic Court, 30 Botanic Road,
Glasnevin, Dublin 9.
Tel: 8301852 / Fax: 8602265

Project:

Calmount Rd, Ballymount - Roads

Design:



Telephone Log:



Minutes



Other Record::



Project No:

Element:

Prepared:

Checked:

23002**Site Catchment Characteristics****NS****SG/CK**

Ref:

Output:

Site Catchment Characteristics

Element	Return period=30yr												
	2	5	10	15	30	60	120	240	360	720	1440	2880	4320
Infiltration Trench 1 (Cafe)	14.58	5.83	2.92	1.94	0.97	0.49	0.24	0.12	0.08	0.04	0.03	0.01	0.01
Infiltration Trench 2 (Cafe)	4.83	1.93	0.97	0.64	0.32	0.16	0.08	0.04	0.03	0.01	0.01	0.00	0.00
Infiltration Trench 1 (Unit 1)	5.28	2.11	1.06	0.70	0.35	0.18	0.09	0.04	0.03	0.01	0.01	0.00	0.00
Infiltration Trench 2 (Unit 1)	15.63	6.25	3.13	2.08	1.04	0.52	0.26	0.13	0.09	0.04	0.03	0.01	0.01
Infiltration Trench 2 (Unit 2)	12.69	5.08	2.54	1.69	0.85	0.42	0.21	0.11	0.07	0.04	0.02	0.01	0.01
Infiltration Trench 3 (Unit 2)	21.84	8.74	4.37	2.91	1.46	0.73	0.36	0.18	0.12	0.06	0.04	0.02	0.01
Infiltration Trench 4 (Unit 2)	10.20	4.08	2.04	1.36	0.68	0.34	0.17	0.09	0.06	0.03	0.02	0.01	0.00
Infiltration Trench 2 (Unit 3)	14.40	5.76	2.88	1.92	0.96	0.48	0.24	0.12	0.08	0.04	0.03	0.01	0.01
Infiltration Trench 3 (Unit 3)	18.75	7.50	3.75	2.50	1.25	0.63	0.31	0.16	0.10	0.05	0.03	0.01	0.01
Infiltration Trench 4 (Unit 3)	9.36	3.74	1.87	1.25	0.62	0.31	0.16	0.08	0.05	0.03	0.02	0.01	0.00
Infiltration Trench 2 (Unit 6)	6.03	2.41	1.21	0.80	0.40	0.20	0.10	0.05	0.03	0.02	0.01	0.00	0.00
Infiltration Trench 3 (Unit 6)	11.94	4.78	2.39	1.59	0.80	0.40	0.20	0.10	0.07	0.03	0.02	0.01	0.01
Infiltration Trench 4 (Unit 6)	14.76	5.90	2.95	1.97	0.98	0.49	0.25	0.12	0.08	0.04	0.03	0.01	0.01
Infiltration Trench 1 TP (Unit 4)	13.02	5.21	2.60	1.74	0.87	0.43	0.22	0.11	0.07	0.04	0.02	0.01	0.01
Infiltration Trench 1 TP (Unit 5C)	3.06	1.22	0.61	0.41	0.20	0.10	0.05	0.03	0.02	0.01	0.01	0.00	0.00
Infiltration Trench 2 TP (Unit 4)	0.57	0.23	0.11	0.08	0.04	0.02	0.01	0.00	0.00	0.00	0.00	0.00	0.00
Infiltration Trench 5 TP (Unit 3)	2.13	0.85	0.43	0.28	0.14	0.07	0.04	0.02	0.01	0.01	0.00	0.00	0.00
Infiltration Trench 5 TP (Unit 6)	3.09	1.24	0.62	0.41	0.21	0.10	0.05	0.03	0.02	0.01	0.01	0.00	0.00
Total Overflow Discharge (Q) [l/sec]	182.16	72.86	36.43	24.29	12.14	6.07	3.04	1.52	1.01	0.51	0.34	0.13	0.08

TITLE: ATTENUATION

(30 Yr Return Period)

CALCS BY: CHECK'D:

NS

SG/CK

RCD.

ISSUE. 1

REV. 0

**Doherty Finegan Kelly**

30-32 Botanic Road, Glasnevin, Dublin 9

Tel: 830 1852, Fax: 860 2265,

E-mail: mailroom@dfk.ie

SURFACE WATER STORAGE

Storm Return Period =	30	Years
Total Site Area =	1.0940	Hectares (ha)
Areas Contributing to Drainage Network:		
Roof area	0.0000	ha
Hardstanding - Footpath	0.4648	ha
Hardstanding - Road	0.2846	ha
Landscaping	0.3446	ha
Total Impermeable Area =	0.7270	ha

.....@	100%	Impermeable
.....@	80%	Impermeable
.....@	80%	Impermeable
.....@	37%	Impermeable

Site Location:

Ballymount

Allowable Outflow = 4.59 litres/sec

Duration (min)	Discharge* Q (l/s)	Proposed Runoff (m ³)	Contiguous Land Runoff (m ³)	Total ** Runoff (m ³)	Allowable Outflow (m ³)	Storage Req'd (m ³)
2	182.16	22	0	26	1	25.7
5	72.86	22	0	26	1	24.9
10	36.43	22	0	26	3	23.5
15	24.29	22	0	26	4	22.1
30	12.14	22	0	26	8	18.0
60	6.07	22	0	26	17	9.7
120	3.04	22	0	26	33	-6.8
240	1.52	22	0	26	66	-39.9
360	1.01	22	0	26	99	-72.9
720	0.51	22	0	26	198	-172.1
1440	0.34	29	0	35	397	-361.6
2880	0.13	22	0	26	793	-766.9
4320	0.08	22	0	26	1190	-1163.5

** Includes 20% for climate change

Storage required = 25.7 m³ _____ m³

*Refer to 'Overflow from Infiltration Trench' sheet for Discharge, Q figures

TITLE: ATTENUATION

(100 Yr Return Period)

CALCS BY: CHECK'D:

NS

SG/CK

RCD.

ISSUE. 1

REV. 0

**Doherty Finegan Kelly**

30-32 Botanic Road, Glasnevin, Dublin 9

Tel: 830 1852, Fax: 860 2265,

E-mail: mailroom@dfk.ie

SURFACE WATER STORAGE

Storm Return Period =	100	Years
Total Site Area =	1.0940	Hectares (ha)
Areas Contributing to Drainage Network:		
Roof area	0.0000	ha
Hardstanding - Footpath	0.4648	ha
Hardstanding - Road	0.2846	ha
Landscaping	0.3446	ha
Total Impermeable Area =	0.7270	ha

.....@	100%	Impermeable
.....@	80%	Impermeable
.....@	80%	Impermeable
.....@	37%	Impermeable

Site Location:

Ballymount

Allowable Outflow = 5.69 litres/sec

Duration (min)	Discharge* Q (l/s)	Proposed Runoff (m ³)	Contiguous Land Runoff (m ³)	Total ** Runoff (m ³)	Allowable Outflow (m ³)	Storage Req'd (m ³)
2	441.39	53	0	64	1	62.9
5	176.56	53	0	64	2	61.9
10	88.28	0	0	0	3	-3.4
15	58.85	0	0	0	5	-5.1
30	29.43	0	0	0	10	-10.2
60	14.71	0	0	0	20	-20.5
120	7.36	0	0	0	41	-41.0
240	3.68	0	0	0	82	-81.9
360	2.45	0	0	0	123	-122.9
720	1.23	0	0	0	246	-245.8
1440	0.82	0	0	0	492	-491.6
2880	0.31	0	0	0	983	-983.2
4320	0.20	0	0	0	1475	-1474.8

** Includes 20% for climate change

Storage required = 62.9 m³ _____ m³

*Refer to 'Overflow from Infiltration Trench' sheet for Discharge, Q figures

	<p>Doherty Finegan Kelly Consulting Structural & Civil Engineers,</p>		<p>Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265</p>										
<p>Project No:</p> <p>23002</p>		<p>Project: Calmount Rd, Ballymount - Internal Roads</p>			<p>Design: <input checked="" type="checkbox"/></p>	<p>Telephone Log: <input type="checkbox"/></p>							
		<p>Element: Attenuation Design Criteria</p>			<p>Minutes: <input type="checkbox"/></p>	<p>Other Record: <input type="checkbox"/></p>							
<p>Reference:</p>		<p>Prepared:</p>			<p>Checked:</p>								
		<p>NS</p>			<p>SG/CK</p>								
								Output:					
<p>Criterion 1</p>		<p>Calmount Rd, Ballymount - Extreme Rainfall Matrix</p>											
		<p>RP5 60min= 00.0 mm</p>		<p>RP5 2d= 00.0 mm</p>		<p>ANNUAL RAINFALL= 707.0 mm</p>							
		<p>RETURN PERIOD (YEARS)</p>											
		<p>DURATION</p>		<p>0.5</p>	<p>1</p>	<p>2</p>	<p>5</p>	<p>10</p>	<p>20</p>	<p>30</p>	<p>50</p>	<p>100</p>	
		<p>2 min</p>		<p>0.0</p>	<p>0.0</p>	<p>0.0</p>	<p>0.0</p>	<p>0.0</p>	<p>0.0</p>	<p>0.0</p>	<p>0.0</p>	<p>0.0</p>	
		<p>5 min</p>		<p>2.9</p>	<p>4.3</p>	<p>5.2</p>	<p>7.8</p>	<p>10.1</p>	<p>12.7</p>	<p>14.4</p>	<p>17.0</p>	<p>21.1</p>	
		<p>10 min</p>		<p>4.1</p>	<p>6.0</p>	<p>7.1</p>	<p>10.9</p>	<p>14.0</p>	<p>17.6</p>	<p>20.2</p>	<p>23.6</p>	<p>29.4</p>	
		<p>15 min</p>		<p>4.8</p>	<p>7.1</p>	<p>8.4</p>	<p>12.8</p>	<p>16.6</p>	<p>20.8</p>	<p>23.6</p>	<p>27.8</p>	<p>34.6</p>	
		<p>30 min</p>		<p>6.2</p>	<p>9.2</p>	<p>10.9</p>	<p>16.4</p>	<p>20.9</p>	<p>26.2</p>	<p>29.6</p>	<p>34.7</p>	<p>42.8</p>	
		<p>60 min</p>		<p>8.3</p>	<p>12.0</p>	<p>14.0</p>	<p>21.0</p>	<p>26.5</p>	<p>32.9</p>	<p>37.2</p>	<p>43.2</p>	<p>52.9</p>	
<p>2 hr</p>		<p>10.9</p>	<p>15.7</p>	<p>18.2</p>	<p>26.9</p>	<p>33.6</p>	<p>41.4</p>	<p>46.6</p>	<p>53.9</p>	<p>65.5</p>			
<p>4 hr</p>		<p>14.5</p>	<p>20.5</p>	<p>23.6</p>	<p>34.3</p>	<p>42.6</p>	<p>52.1</p>	<p>58.3</p>	<p>67.1</p>	<p>81.0</p>			
<p>6 hr</p>		<p>17.0</p>	<p>23.9</p>	<p>27.6</p>	<p>39.6</p>	<p>49.0</p>	<p>59.5</p>	<p>66.5</p>	<p>76.3</p>	<p>91.7</p>			
<p>12 hr</p>		<p>22.6</p>	<p>31.2</p>	<p>35.8</p>	<p>50.6</p>	<p>62.2</p>	<p>75.0</p>	<p>83.4</p>	<p>95.0</p>	<p>113.5</p>			
<p>24 hr</p>		<p>29.8</p>	<p>40.7</p>	<p>46.3</p>	<p>64.8</p>	<p>78.7</p>	<p>94.3</p>	<p>104.4</p>	<p>118.4</p>	<p>140.4</p>			
<p>48 hr</p>		<p>37.2</p>	<p>49.6</p>	<p>55.9</p>	<p>76.2</p>	<p>91.2</p>	<p>107.8</p>	<p>118.3</p>	<p>133.0</p>	<p>155.5</p>			
<p>72 hr</p>		<p>43.2</p>	<p>56.8</p>	<p>63.7</p>	<p>85.4</p>	<p>101.4</p>	<p>118.7</p>	<p>129.8</p>	<p>145.0</p>	<p>168.2</p>			
		<p>Allowance of 20% for Climate Change in accordance with GDSDS</p>											
		<p>INTERCEPTION STORAGE (First 5mm of rainfall over 80% of the impervious area, see GDSDS Vol2 Cl6.7.1 & Cl6.3.4)</p>											
		<p>Total Site Area</p>		<p>10940 m²</p>								<p>N.B. Interception Storage is where all runoff from at least the first 5mm of rainfall can be prevented from entering the receiving water. i.e. The first 5mm of rainfall is infiltrated/recycled</p>	
		<p>Hardstanding - Road</p>		<p>4648 m²</p>									
		<p>Hardstanding - F&C/P</p>		<p>2846 m²</p>									
		<p>Permeable area</p>		<p>0 m²</p>									
		<p>Landscape</p>		<p>3446 m²</p>									
		<p>Interception Volume Required (0.005 * 0.8 * Impervious Area)</p>		<p>Hardstanding - Road</p>		<p>Hardstanding - F&C/F</p>		<p>Paved Area</p>		<p>Total</p>			
				<p>18.59 m³</p>		<p>11.38 m³</p>		<p>0.00 m³</p>		<p>29.98 m³</p>			
		<p>Treatment Volume Provided</p>		<p>Infiltration Trenches</p>		<p>StormTech</p>				<p>Total</p>			
				<p>111.06 m³</p>		<p>16.25 m³</p>				<p>127.31 m³</p>			
		<p>NOTES:</p> <p>Infiltration Trenchs/Tree Pits = 493.60m x 1.0m x 0.75m dp) x 0.3 = 111.06m³</p> <p>StormTech Trench (Below IL Chambers): (3.35m x 48.5 x 0.25m) x 0.4 = 16.25m³</p>											
		<p>TREATMENT STORAGE (First 15mm of rainfall over 80% of the impervious area, see GDSDS Cl6.7.1 & Cl6.3.4)</p>											
		<p>Total Site Area</p>		<p>10940 m²</p>								<p>N.B. Interception and Treatment Storage are both part of Criterion 1. Therefore if interception storage is provided, then treatment storage is only required to provide for the remainder of the</p>	
		<p>Hardstanding - Road</p>		<p>4648 m²</p>									
		<p>Hardstanding - F&C/P</p>		<p>2846 m²</p>									
		<p>Permeable area</p>		<p>0 m²</p>									
		<p>Landscape</p>		<p>3446 m²</p>									
		<p>Treatment Volume Required (0.015 * 0.8 * Impervious Area)</p>		<p>Hardstanding - Road</p>		<p>Hardstanding - F&C/F</p>		<p>Paved Area</p>		<p>Total</p>			
				<p>55.78 m³</p>		<p>34.15 m³</p>		<p>0.00 m³</p>		<p>89.93 m³</p>			
		<p>Treatment Volume Provided</p>		<p>Infiltration Trenches</p>		<p>StormTech</p>				<p>Total</p>			
				<p>111.06 m³</p>		<p>16.25 m³</p>				<p>127.31 m³</p>			
		<p>NOTES:</p> <p>As outlined above</p>											
		<p>OK</p>											

	Doherty Finegan Kelly <i>Consulting Structural & Civil Engineers,</i>		Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265																											
	Project: Calmount Rd, Ballymount - Internal Roads		Design: <input checked="" type="checkbox"/> Telephone Log: <input type="checkbox"/>	Minutes: <input type="checkbox"/> Other Record: <input type="checkbox"/>																										
Project No: 23002	Element: Attenuation Design Criteria	Prepared: NS		Checked: SG/CK																										
Reference:						Output: <div style="background-color: #002060; color: white; padding: 5px; text-align: center;"> ATTENUATION STORAGE (see GDSDS CI6.3.4) </div> <table border="1" style="width: 100%; border-collapse: collapse; margin-top: 5px;"> <tr> <td style="width: 30%; padding: 2px;">100 year Attenuation Volume Required</td> <td style="width: 70%; padding: 2px; text-align: right;">62.90 m³</td> </tr> <tr> <td colspan="2" style="padding: 2px;"> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th style="width: 20%;">Attenuation Volume Provided</th> <th style="width: 80%;">StormTech Trench</th> </tr> <tr> <td style="text-align: center;">108.30 m³</td> <td style="text-align: center;">Total 108.30</td> </tr> </table> </td> </tr> </table> <p style="margin-top: 10px;">NOTES: 100 Year Attenuation Volume based on Extreme rainfall matrix with 20% allowance for climate change added.</p>	100 year Attenuation Volume Required	62.90 m³	<table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th style="width: 20%;">Attenuation Volume Provided</th> <th style="width: 80%;">StormTech Trench</th> </tr> <tr> <td style="text-align: center;">108.30 m³</td> <td style="text-align: center;">Total 108.30</td> </tr> </table>		Attenuation Volume Provided	StormTech Trench	108.30 m ³	Total 108.30																
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<div style="background-color: #002060; color: white; padding: 5px; text-align: center;"> LONG TERM STORAGE (See GDSDS CI6.3.4) </div> <table border="1" style="width: 100%; border-collapse: collapse; margin-top: 5px;"> <tr> <td style="width: 30%; padding: 2px;">Rainfall depth for 100 year, 6 hour event</td> <td style="width: 10%; padding: 2px; text-align: center;">RD</td> <td style="width: 60%; padding: 2px; text-align: center;">92 mm</td> </tr> <tr> <td>Percentage of Impermeable area</td> <td style="text-align: center;">PIMP</td> <td style="text-align: center;">0.685</td> </tr> <tr> <td>Site Area</td> <td style="text-align: center;">A</td> <td style="text-align: center;">10940 m²</td> </tr> <tr> <td>Soil Index (Soil Type 2)</td> <td style="text-align: center;">SOIL</td> <td style="text-align: center;">0.3</td> </tr> <tr> <td>Percentage of impervious area draining to the network or directly to the river</td> <td style="text-align: center;">α</td> <td style="text-align: center;">0.62</td> </tr> <tr> <td>Percentage of pervious areas draining to the network or directly to the river</td> <td style="text-align: center;">β</td> <td style="text-align: center;">0.0</td> </tr> <tr> <td style="text-align: center;">Long Term Storage Required</td> <td style="text-align: center;">Volxs</td> <td style="text-align: center;">39.88 m³</td> </tr> <tr> <td style="text-align: center;">Long Term Storage Provided</td> <td></td> <td style="text-align: center;">127.31 m³</td> </tr> </table> <p style="margin-top: 10px;">NOTES: Volxs is the extra runoff volume for the 100 year 6 hour storm over that of the original greenfield runoff volume for the same storm. Should sufficient long term storage not be provided that can prevent all or some of this volume (Volxs) from entering the receiving waters, then the throttle should be reduced to Qbar or 2l/s for all events and the runoff should be attenuated accordingly. (see GDSDS CI6.3.4 Sub-Criterion4.3)</p>						Rainfall depth for 100 year, 6 hour event	RD	92 mm	Percentage of Impermeable area	PIMP	0.685	Site Area	A	10940 m ²	Soil Index (Soil Type 2)	SOIL	0.3	Percentage of impervious area draining to the network or directly to the river	α	0.62	Percentage of pervious areas draining to the network or directly to the river	β	0.0	Long Term Storage Required	Volxs	39.88 m³	Long Term Storage Provided		127.31 m³	OK
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Long Term Storage Provided		127.31 m³																												
<div style="background-color: #002060; color: white; padding: 5px; text-align: center;"> COMMENTS </div>						OK																								



Project:

Calmount Rd, Ballymount - Unit 1

Design: Telephone Log: Minutes: Other Record:

Project No:

23002

Infiltration Drainage - Perm Paving

Prepared:

Checked:

NS

SG/CK

Reference:

Output:

Calmount Rd, Ballymount - Extreme Rainfall Matrix

RP5 60min= 16.2 mm RP5 2d= 59.4 mm ANNUAL RAINFALL= 707.0 mm

DURATION	RETURN PERIOD (YEARS)								
	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3

Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)

Plane Infiltration - Permeable Paving

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	clay	128.9 mm/hr
FOS	Minor Inconvenience	3.00
q		0.043 m/hr

Assume - uniform gravel (n)	0.35
-----------------------------	------

Equations Applied to Determine h_{max}

$$h_{max} = \frac{D}{n} (Ri - q) \quad (1)$$

Where:

R= $A_D/A_b=$ 1.00

Area to be Drained

A_D	700 m ²
-------	--------------------

Area to be drained --

Infiltration system dimensions

Width	-
Length	-
Base Area (A_b)	700 m ²

H_{max} Calculation

10 Year Return Period

Duration (D)	h_{max}
15 min	0.017
30 min	0.000
60 min	0.000
120 min	0.000
240 min	0.000
360 min	0.000

30 Year Return Period

Duration (D)	h_{max}
15 min	0.037
30 min	0.023
60 min	0.000
120 min	0.000
240 min	0.000
360 min	0.000

50 Year Return Period

Duration (D)	h_{max}
15 min	0.049
30 min	0.038
60 min	0.001
120 min	0.000
240 min	0.000
360 min	0.000

100 Year Return Period

Duration (D)	h_{max}
15 min	0.068
30 min	0.061
60 min	0.028
120 min	0.000
240 min	0.000
360 min	0.000

Plane Infiltration - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{nh_{max}}{q} \quad (2)$$

$$q = \frac{nh_{max}}{T_{empty}} \quad (3)$$

Event	Time to Empty
1 in 10 years	0.135 hrs
1 in 30 years	0.300 hrs
1 in 50 years	0.398 hrs
1 in 100 years	0.554 hrs

Event	Min feasible (q)
1 in 10 years	0.0001 m/hr
1 in 30 years	0.0005 m hr
1 in 50 years	0.0007 m hr
1 in 100 years	0.0010 m hr



		Doherty Finegan Kelly Consulting Structural & Civil Engineers, Project:		Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265			
		Calmount Rd, Ballymount - Unit 1		Design:	<input checked="" type="checkbox"/>	Telephone Log:	<input type="checkbox"/>
				Minutes:	<input type="checkbox"/>	Other Record:	<input type="checkbox"/>
Project No:	Element:		Prepared:		Checked:		
23002	Bio-retention Area		NS		SG/CK		

Reference:		Output:																																																																																																																																												
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Doherty Finegan Kelly

Consulting Structural & Civil Engineers,

Botanic Court, 30 Botanic Road, Glasnevin,

Dublin 9

Tel: 8301852 / Fax: 8602265

Project:

Calmount Rd, Ballymount - Unit 1

Design: Telephone Log: Minutes: Other Record:

Project No:

Element:

Prepared: Checked:

23002

Bio-retention Area

NS SG/CK

Reference: Output:

Vertical Sided System

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	Soil	143.6 mm/hr
FOS	Minor Inconvenience	3.00
q		0.048 m/hr

Equations Applied to Determine hmax

$$h_{\max} = a(e^{(-bD)} - 1) \quad (1)$$

where:

$$b = \frac{Pq}{A_b n} \quad (2)$$

and a is given by:

$$a = \frac{A_b - A_b i}{P - Pq} \quad (3)$$

b=	0.335
Ab/P=	0.476

Infiltration Trench dimensions

Length	20.00 m
Width	1.00 m
Base Area (A_b)	20.000 m ²
Perimeter (P)	42.000 m

H_{max} Calculation

10 Year Return Period

Duration (D)	hmax	a
15.000 min	0.306	-3.806
30.000 min	0.343	-2.223
60.000 min	0.353	-1.238
120.000 min	0.298	-0.610
240.000 min	0.157	-0.212
360.000 min	0.044	-0.051

30 Year Return Period

Duration (D)	hmax	a
15.000 min	0.453	-5.637
30.000 min	0.518	-3.356
60.000 min	0.549	-1.929
120.000 min	0.503	-1.029
240.000 min	0.344	-0.466
360.000 min	0.208	-0.240

50 Year Return Period

Duration (D)	hmax	a
15.000 min	0.540	-6.723
30.000 min	0.618	-4.008
60.000 min	0.660	-2.317
120.000 min	0.618	-1.265
240.000 min	0.449	-0.608
360.000 min	0.300	-0.346

100 Year Return Period

Duration (D)	hmax	a
15.000 min	0.680	-8.460
30.000 min	0.781	-5.063
60.000 min	0.839	-2.945
120.000 min	0.802	-1.642
240.000 min	0.615	-0.833
360.000 min	0.443	-0.512

Vertical Sided System - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{1}{b} \log_e \left[\frac{h_{\max} + \frac{A_b}{P}}{\frac{h_{\max}}{2} + \frac{A_b}{P}} \right]$$

Event	Time to Empty
1 in 10 years	0.714 hrs
1 in 30 years	0.930 hrs
1 in 50 years	1.023 hrs
1 in 100 years	1.146 hrs

Infiltration System -- Overflow from French Drain

Return Period	Duration	Base Area (A_b)	h_{PROVIDED}	h_{\max}	Q_{OVERFLOW}^*
10 Years	60.000 min	20.000 m ²	0.850 m	0.353 m	0.000 l/sec
30 Years	60.000 min	20.000 m ²	0.850 m	0.549 m	0.000 l/sec
50 Years	60.000 min	20.000 m ²	0.850 m	0.660 m	0.000 l/sec
100 Years	60.000 min	20.000 m ²	0.850 m	0.839 m	0.000 l/sec

* Q_{OVERFLOW} is the averaged flow for the duration given.

TITLE: ATTENUATION
(30 Yr Return Period)

CALCS BY: NS **CHECK'D:** SG/CK

RCD.

ISSUE. 1

REV. 0



Doherty Finegan Kelly
30-32 Botanic Road, Glasnevin, Dublin 9
Tel: 830 1852, Fax: 860 2265,
E-mail: mailroom@dfk.ie

SURFACE WATER STORAGE

Storm Return Period =	30	Years
Total Site Area =	0.7351	Hectares (ha)
Areas Contributing to Drainage Network:		
Roof	0.2935	ha
Hardstanding	0.2363	ha
	ha	
Total Impermeable Area =	0.4825	ha

.....@	100%	Impermeable
.....@	80%	Impermeable
.....@	0%	Impermeable
.....@	0%	Impermeable
.....@	0%	Impermeable

Site Location:

Ballymount

Allowable Outflow = 3.09 litres/sec

Duration (min)	Rainfall 30 Year (mm)	Intensity (mm/hr)	Discharge Q (= 2.71Ai) (l/s)	Proposed Runoff (m³)	Contiguous Land Runoff (m³)	Total ** Runoff (m³)	Allowable Outflow (m³)	Storage Req'd (m³)
2	0.0	0.0	0	0	0	0	0	-0.4
5	12.0	144.0	188	56	0	68	1	66.9
10	16.8	100.8	132	79	0	95	2	93.1
15	19.7	78.8	103	93	0	111	3	108.5
30	24.7	49.4	65	116	0	140	6	134.0
60	31.0	31.0	41	146	0	175	11	164.0
120	38.8	19.4	25	183	0	219	22	197.0
240	48.6	12.2	16	229	0	275	44	230.1
360	55.4	9.2	12	261	0	313	67	246.3
720	69.5	5.8	8	327	0	393	133	259.2
1440	87.0	3.6	5	410	0	491	267	224.7
2880	98.6	2.1	3	464	0	557	534	23.5
4320	108.2	1.5	2	509	0	611	800	-189.0

** Includes 20% for climate change

Storage required = 259.2 m³

TITLE: ATTENUATION
(100 Yr Return Period)

CALCS BY: NS **CHECK'D:** SG/CK

RCD.

ISSUE. 1

REV. 0



Doherty Finegan Kelly
30-32 Botanic Road, Glasnevin, Dublin 9
Tel: 830 1852, Fax: 860 2265,
E-mail: mailroom@dfk.ie

SURFACE WATER STORAGE

Storm Return Period =	100	Years
Total Site Area =	0.7351	Hectares (ha)
Areas Contributing to Drainage Network:		
Roof	0.2935	ha
Hardstanding	0.2353	ha
	ha	
Total Impermeable Area =	0.4817	ha

.....@	100%	Impermeable
.....@	80%	Impermeable
.....@	0%	Impermeable
.....@	0%	Impermeable
.....@	0%	Impermeable

Site Location:

Ballymount

Allowable Outflow =	3.82	litres/sec
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Duration (min)	Rainfall 100 Year (mm)	Intensity (mm/hr)	Discharge Q (= 2.71Ai) (l/s)	Proposed Runoff (m³)	Contiguous Land Runoff (m³)	Total ** Runoff (m³)	Allowable Outflow (m³)	Storage Req'd (m³)
2	0.0	0.0	0	0	0	0	0	-0.5
5	17.6	211.2	276	83	0	99	1	98.1
10	24.5	147.0	192	115	0	138	2	135.9
15	28.8	115.2	150	135	0	162	3	159.0
30	35.7	71.4	93	168	0	201	7	194.5
60	44.1	44.1	58	207	0	249	14	235.0
120	54.6	27.3	36	257	0	308	28	280.4
240	67.5	16.9	22	317	0	381	55	325.7
360	76.4	12.7	17	359	0	431	83	348.4
720	94.6	7.9	10	445	0	534	165	368.5
1440	117.0	4.9	6	550	0	660	330	329.8
2880	129.6	2.7	4	609	0	731	660	70.8
4320	140.2	1.9	3	659	0	791	990	-199.4

** Includes 20% for climate change

Storage required =	368.5	m³			m³
--------------------	-------	----	--	--	----

STORMTECH Stormwater Management System Design Tool

ver: Aug15

PROJECT REF: 23002 - Calmount Rd, Ballymount - Unit 1

LOCATION: Attenuation SC740 - Sheet 1

DATE: 15.03.2023

CREATED BY: SG

SYSTEM PARAMETERS

Required Total Storage		m ³
Stormtech chamber model	SC740	
Filtration Permeable Geo or Impermeable Geo	Filter geo	
Number of Isolator Rows (IR)	1	

SITE PARAMETERS

Stone Porosity	40%	
Excavation Batter Angle (degrees)	60°	Minimum Requirement
Stone Above Chambers	0.3 m	0.15
Stone Below Chambers (Long-Term Storage)	0 m	0.15 <i>Adjust to minimum</i>
In-between Row Spacing	0.15 m	0.15
Additional Storage outside Excavation. E.g manholes, Header Pipe	0 m ³	

HEADER PIPE

Is Header pipe required within excavation	No
Orientation of Header Pipe	Perp to IR
Diameter of Header Pipe	0 m
Length of Header Pipe	0 m

CHAMBER SYSTEM DIMENSIONS

	Calculated	Adopted
Number of Rows	12 ea	
Number of units per Row	10 ea	
System Installed Storage Depth (effective storage depth)	1.060	1.06 m
Tank overall installed Width at base	17.79	17.8 m
Tank overall installed Length at Base	22.4	22.5 m
Total Effective System Storage	274.8	275.7 m ³

STORMTECH SYSTEM DETAIL

StormTech Chamber Model	SC740
Unit Width	1.295 m
Unit Length	2.17 m
Unit Height	0.76 m
Min Cover Over System	0.3 m
Max Cover Over Chamber	2.4 m
Chamber Internal Storage Vol.	1.3 m ³
Header Pipe Internal Storage Vol in Excavation	0.0 m ³

STONE AND EXCAVATION DETAIL

Volume of Dig for System	451 m ³
Width at base	17.80 m
Width at top	19.02 m
Length at base	22.50 m
Length at top	23.72 m
Depth Of System	1.06 m
Area of Dig at Base of System	401 m ²
Area of Dig at Top of System	451 m ²
Void Ratio	61%
Stone Requirement - m ³	293 m ³
Stone Requirement - tonne	481 tonne

STORMTECH Stormwater Management System Design Tool

ver: Aug15

PROJECT REF: 23002 - Calmount Rd, Ballymount - Unit 1

LOCATION: Attenuation SC740 - Sheet 2

DATE: 15.03.2023

CREATED BY: SG

SYSTEM PARAMETERS

Required Total Storage		m ³
Stormtech chamber model	SC740	
Filtration Permeable Geo or Impermeable Geo	Filter geo	
Number of Isolator Rows (IR)	1	

SITE PARAMETERS

Stone Porosity	40%	
Excavation Batter Angle (degrees)	60°	Minimum Requirement
Stone Above Chambers	0.3 m	0.15
Stone Below Chambers (Long-Term Storage)	0 m	0.15 <i>Adjust to minimum</i>
In-between Row Spacing	0.15 m	0.15
Additional Storage outside Excavation. E.g manholes, Header Pipe	0 m ³	

HEADER PIPE

Is Header pipe required within excavation	No
Orientation of Header Pipe	Perp to IR
Diameter of Header Pipe	0 m
Length of Header Pipe	0 m

CHAMBER SYSTEM DIMENSIONS

	Calculated	Adopted
Number of Rows	7 ea	
Number of units per Row	6 ea	
System Installed Storage Depth (effective storage depth)	1.060	1.06 m
Tank overall installed Width at base	10.57	10.6 m
Tank overall installed Length at Base	13.72	13.8 m
Total Effective System Storage	101.7	102.3 m ³

STORMTECH SYSTEM DETAIL

StormTech Chamber Model	SC740
Unit Width	1.295 m
Unit Length	2.17 m
Unit Height	0.76 m
Min Cover Over System	0.3 m
Max Cover Over Chamber	2.4 m
Chamber Internal Storage Vol.	1.3 m ³
Header Pipe Internal Storage Vol in Excavation	0.0 m ³

STONE AND EXCAVATION DETAIL

Volume of Dig for System	172 m ³
Width at base	10.60 m
Width at top	11.82 m
Length at base	13.80 m
Length at top	15.02 m
Depth Of System	1.06 m
Area of Dig at Base of System	146 m ²
Area of Dig at Top of System	178 m ²
Void Ratio	60%
Stone Requirement - m ³	116 m ³
Stone Requirement - tonne	190 tonne



 Doherty Finegan Kelly <i>Consulting Structural & Civil Engineers,</i>	Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265			
	Project: Calmount Rd, Ballymount - Unit 1	Design: <input checked="" type="checkbox"/>	Telephone Log:	
Project No: 23002	Element: Attenuation Design Criteria	Minutes: <input type="checkbox"/>	Other Record:	
		Prepared:	Checked:	
		SG	CK	



Doherty Finegan Kelly <i>Consulting Structural & Civil Engineers,</i>		Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265			
Project:		Design:		Telephone Log:	
Calmount Rd, Ballymount - Unit 1		Minutes:		Other Record:	
Project No:	Element:	Prepared:		Checked:	
23002	Attenuation Design Criteria	SG		CK	

Reference			Output
	ATTENUATION STORAGE (see GDSDS CI6.3.4)		
	10 year Attenuation Volume Required	368.50 m³	
	Attenuation Volume Provided	StormTech	Total
		378.00 m³	378.00
			OK
	NOTES: 100 Year Attenuation Volume based on Extreme rainfall matrix with 20% allowance for climate change added		
	LONG TERM STORAGE (See GDSDS CI6.3.4)		
	rainfall depth for 100 year, 6 hour eve	RD	92 mm
	Percentage of Impermeable area	PIMP	0.757
	Site Area	A	7351 m²
	Soil Index (Soil Type 3)	SOIL	0.3
	Percentage of impervious area draining to the network or directly to	α	0.92
	Percentage of pervious area draining to the network or directly	β	0.3
	Long Term Storage Required	Volxs	188.18 m³
	Long Term Storage Provided		191.82 m³
	$\text{Vol}_{\text{xs}} = \text{RD} \cdot \text{A} \cdot 10 \left[\frac{\text{PIMP}}{100} (\alpha \cdot 0.8) + \left(1 - \frac{\text{PIMP}}{100} \right) \beta \cdot \text{SOIL} \right] - \text{SOIL}$ <p>N.B. Long term storage only represents runoff that will be infiltrated or recycled. i.e. soakaway, infiltration trench, water butt/harvesting etc. Attenuation that does not have the option to be infiltrated is not considered as long term storage.</p>		
Criterion 4			OK
	COMMENTS		



Project:

Calmount Rd, Ballymount - Unit 2

Design:

Telephone Log:

Minutes:

Other Record:

Project No:

23002

Infiltration Drainage - Perm Paving

Prepared:

Checked:

NS

SG/CK

Reference:

Output:

Calmount Rd, Ballymount - Extreme Rainfall Matrix

RP5 60min= 16.2 mm RP5 2d= 59.4 mm ANNUAL RAINFALL= 707.0 mm

DURATION	RETURN PERIOD (YEARS)								
	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3

Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)

Plane Infiltration - Permeable Paving

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	clay	28.1 mm/hr
FOS	Minor Inconvenience	5.00
q		0.006 m/hr

Equations Applied to Determine h_{max}

$$h_{\max} = \frac{D}{n} (Ri - q) \quad (I)$$

Where:

R= A_D/A_b= 1.37Assume - uniform gravel (n) 0.35Area to be DrainedA_D 1140 m²

Area to be drained --

Infiltration system dimensions

Width	-
Length	-
Base Area (A _b)	835 m ²

H_{max} Calculation

10 Year Return Period

Duration (D)	h _{max}
15 min	0.061
30 min	0.073
60 min	0.087
120 min	0.099
240 min	0.102
360 min	0.095

30 Year Return Period

Duration (D)	h _{max}
15 min	0.088
30 min	0.108
60 min	0.129
120 min	0.149
240 min	0.163
360 min	0.163

50 Year Return Period

Duration (D)	h _{max}
15 min	0.105
30 min	0.127
60 min	0.152
120 min	0.178
240 min	0.197
360 min	0.201

100 Year Return Period

Duration (D)	h _{max}
15 min	0.131
30 min	0.159
60 min	0.190
120 min	0.223
240 min	0.252
360 min	0.261

Plane Infiltration - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{nh_{\max}}{q} \quad (2)$$

Event	Time to Empty
1 in 10 years	6.334 hrs
1 in 30 years	10.148 hrs
1 in 50 years	12.514 hrs
1 in 100 years	16.240 hrs

Event	Min feasible (q)
1 in 10 years	0.0007 m/hr
1 in 30 years	0.0024 m hr
1 in 50 years	0.0029 m hr
1 in 100 years	0.0038 m hr



Doherty Finegan Kelly
Consulting Structural & Civil Engineers,
Botanic Court, 30 Botanic Road, Glasnevin,
Dublin 9
Tel: 8301852 / Fax: 8602265

Project:

Design:

Telephone Log:

Calmount Rd, Ballymount - Unit 1

Minutes:

Other Record:

Project No:

Element:

Prepared:

Checked:

23002

Bio-retention Area

NS

CK

Reference:

Output:

Calmount Rd, Ballymount - Extreme Rainfall Matrix

RP5 60min= 16.2 mm RP5 2d= 59.4 mm ANNUAL RAINFALL= 707.0 mm

RETURN PERIOD (YEARS)

DURATION	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3

Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)

Contributing Area Plan



Doherty Finegan Kelly

Consulting Structural & Civil Engineers,

Botanic Court, 30 Botanic Road, Glasnevin,

Dublin 9

Tel: 8301852 / Fax: 8602265

Project:

Calmount Rd, Ballymount - Unit 1

Design: Telephone Log: Minutes: Other Record:

Project No:

Element:

Prepared:

Checked:

23002

Bio-retention Area

NS

CK

Reference:

Output:

Vertical Sided System

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	Soil	48.3 mm/hr
FOS	Minor Inconvenience	5.00
q		0.010 m/hr

Equations Applied to Determine hmax

$$h_{\max} = a(e^{(-bD)} - 1) \quad (1)$$

where:

$$b = \frac{Pq}{A_b n} \quad (2)$$

and a is given by:

$$a = \frac{A_b}{P} - \frac{A_d}{Pq} \quad (3)$$

b=	0.019
Ab/P=	1.705

H_{max} Calculation

10 Year Return Period

Duration (D)	hmax	a
15.000 min	0.386	-81.928
30.000 min	0.479	-51.020
60.000 min	0.594	-31.779
120.000 min	0.723	-19.506
240.000 min	0.854	-11.741
360.000 min	0.920	-8.598

30 Year Return Period

Duration (D)	hmax	a
15.000 min	0.554	-117.684
30.000 min	0.687	-73.141
60.000 min	0.846	-45.263
120.000 min	1.026	-27.688
240.000 min	1.215	-16.703
360.000 min	1.315	-12.284

50 Year Return Period

Duration (D)	hmax	a
15.000 min	0.654	-138.896
30.000 min	0.806	-85.867
60.000 min	0.988	-52.838
120.000 min	1.197	-32.309
240.000 min	1.416	-19.468
360.000 min	1.537	-14.355

100 Year Return Period

Duration (D)	hmax	a
15.000 min	0.814	-172.834
30.000 min	1.000	-106.473
60.000 min	1.217	-65.111
120.000 min	1.469	-39.657
240.000 min	1.735	-23.862
360.000 min	1.883	-17.587

Vertical Sided System - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{1}{b} \log_e \left[\frac{h_{\max} + \frac{A_b}{P}}{\frac{h_{\max}}{2} + \frac{A_b}{P}} \right]$$

Event	Time to Empty
1 in 10 years	10.212 hrs
1 in 30 years	13.011 hrs
1 in 50 years	14.334 hrs
1 in 100 years	16.126 hrs

Infiltration System -- Overflow from French Drain

Return Period	Duration	Base Area (A _b)	h _{PROVIDED}	h _{max}	Q _{OVERFLOW} *
10 Years	360.000 min	370.000 m ²	1.000 m	0.920 m	0.000 l/sec
30 Years	360.000 min	370.000 m ²	1.000 m	1.315 m	0.201 l/sec
50 Years	360.000 min	370.000 m ²	1.000 m	1.537 m	0.397 l/sec
100 Years	360.000 min	370.000 m ²	1.000 m	1.883 m	0.800 l/sec

* Q_{OVERFLOW} is the averaged flow for the duration given.

TITLE: ATTENUATION
(30 Yr Return Period)

CALCS BY: NS **CHECK'D:** SG/CK

RCD.

ISSUE. 1

REV. 0



Doherty Finegan Kelly
30-32 Botanic Road, Glasnevin, Dublin 9
Tel: 830 1852, Fax: 860 2265,
E-mail: mailroom@dfk.ie

SURFACE WATER STORAGE

Storm Return Period =	30	Years
Total Site Area =	0.9254	Hectares (ha)
Areas Contributing to Drainage Network:		
Roof	0.0855	ha
Hardstanding	0.2790	ha
	ha	
Total Impermeable Area =	0.3087	ha

.....@	100%	Impermeable
.....@	80%	Impermeable
.....@	0%	Impermeable
.....@	0%	Impermeable
.....@	0%	Impermeable

Site Location:

Ballymount

Allowable Outflow = 3.08 litres/sec

Duration (min)	Rainfall 30 Year (mm)	Intensity (mm/hr)	Discharge Q (= 2.71Ai) (l/s)	Proposed Runoff (m³)	Contiguous Land Runoff (m³)	Total ** Runoff (m³)	Allowable Outflow (m³)	Storage Req'd (m³)
2	0.0	0.0	0	0	0	0	0	-0.4
5	12.0	144.0	120	36	0	43	1	42.4
10	16.8	100.8	84	51	0	61	2	58.9
15	19.7	78.8	66	59	0	71	3	68.4
30	24.7	49.4	41	74	0	89	6	83.7
60	31.0	31.0	26	93	0	112	11	100.9
120	38.8	19.4	16	117	0	140	22	118.0
240	48.6	12.2	10	146	0	176	44	131.3
360	55.4	9.2	8	167	0	200	67	133.7
720	69.5	5.8	5	209	0	251	133	118.1
1440	87.0	3.6	3	262	0	314	266	48.3
2880	98.6	2.1	2	297	0	356	532	-175.9
4320	108.2	1.5	1	326	0	391	798	-407.3

** Includes 20% for climate change

Storage required = 133.7 m³

TITLE: ATTENUATION

(100 Yr Return Period)

CALCS BY: CHECK'D:

NS

SG/CK

RCD.

ISSUE. 1

REV. 0

**Doherty Finegan Kelly**

30-32 Botanic Road, Glasnevin, Dublin 9

Tel: 830 1852, Fax: 860 2265,

E-mail: mailroom@dfk.ie

SURFACE WATER STORAGE

Storm Return Period =	100	Years
Total Site Area =	0.9254	Hectares (ha)
Areas Contributing to Drainage Network:		
Roof	0.0855	ha
Hardstanding	0.2790	ha
	ha	
Total Impermeable Area =	0.3087	ha

.....@	100%	Impermeable
.....@	80%	Impermeable
.....@	0%	Impermeable
.....@	0%	Impermeable
.....@	0%	Impermeable

Site Location:

Ballymount

Allowable Outflow = 4.00 litres/sec

Duration (min)	Rainfall 100 Year (mm)	Intensity (mm/hr)	Discharge Q (= 2.71Ai) (l/s)	Proposed Runoff (m³)	Contiguous Land Runoff (m³)	Total ** Runoff (m³)	Allowable Outflow (m³)	Storage Req'd (m³)
2	0.0	0.0	0	0	0	0	0	-0.5
5	17.6	211.2	177	53	0	64	1	62.4
10	24.5	147.0	123	74	0	89	2	86.1
15	28.8	115.2	96	87	0	104	4	100.5
30	35.7	71.4	60	108	0	129	7	121.8
60	44.1	44.1	37	133	0	159	14	145.0
120	54.6	27.3	23	164	0	197	29	168.5
240	67.5	16.9	14	203	0	244	58	186.3
360	76.4	12.7	11	230	0	276	86	189.7
720	94.6	7.9	7	285	0	342	173	169.1
1440	117.0	4.9	4	352	0	423	346	77.2
2880	129.6	2.7	2	390	0	468	691	-222.8
4320	140.2	1.9	2	422	0	507	1037	-530.1

** Includes 20% for climate change

Storage required = 189.7 m³

STORMTECH Stormwater Management System Design Tool

ver: Aug15

PROJECT REF: 23002 - Calmount Rd, Ballymount - Unit 2

LOCATION: StormTech Trench

DATE: 09-Mar-23

CREATED BY: NS

SYSTEM PARAMETERS

Required Total Storage	189.7 m ³
Stormtech chamber model	SC740
Filtration Permeable Geo or Impermeable Geo	Filter geo
Number of Isolator Rows (IR)	1

SITE PARAMETERS

Stone Porosity	40%	
Excavation Batter Angle (degrees)	60 °	Minimum Requirement
Stone Above Chambers	0.15 m	0.15
Stone Below Chambers (Long-Term Storage)	0 m	0.15 <i>Adjust to minimum</i>
In-between Row Spacing	0.15 m	0.15
Additional Storage outside Excavation. E.g manholes, Header Pipe	0 m ³	

HEADER PIPE

Is Header pipe required within excavation	No
Orientation of Header Pipe	Perp to IR
Diameter of Header Pipe	0 m
Length of Header Pipe	0 m

CHAMBER SYSTEM DIMENSIONS

	Calculated	Adopted
Number of Rows	7 ea	
Number of units per Row	13 ea	
System Installed Storage Depth (effective storage depth)	0.910 m	
Tank overall installed Width at base	10.57 m	10.6 m
Tank overall installed Length at Base	28.91 m	29 m
Total Effective System Storage	190.8 m ³	191.5 m ³

STORMTECH SYSTEM DETAIL

StormTech Chamber Model	SC740
Unit Width	1.295 m
Unit Length	2.17 m
Unit Height	0.76 m
Min Cover Over System	0.3 m
Max Cover Over Chamber	2.4 m
Chamber Internal Storage Vol.	1.3 m ³
Header Pipe Internal Storage Vol in Excavation	0.0 m ³

STONE AND EXCAVATION DETAIL

Volume of Dig for System	299 m ³
Width at base	10.60 m
Width at top	11.65 m
Length at base	29.00 m
Length at top	30.05 m
Depth Of System	0.91 m
Area of Dig at Base of System	307 m ²
Area of Dig at Top of System	350 m ²
Void Ratio	64%
Stone Requirement - m ³	180 m ³
Stone Requirement - tonne	295 tonne



 DFK <i>Consulting Structural & Civil Engineers,</i>	Doherty Finegan Kelly		Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265		
	Project: Calmount Rd, Ballymount - Unit 2		Design: <input checked="" type="checkbox"/>	Telephone Log:	
			Minutes: <input type="checkbox"/>	Other Record:	
Project No:	Element:		Prepared:		Checked:
23002	Attenuation Design Criteria		SG		CK



Doherty Finegan Kelly <i>Consulting Structural & Civil Engineers,</i>		Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265			
Project:		Design:		Telephone Log:	
Calmount Rd, Ballymount - Unit 2		Minutes:		Other Record:	
Project No:	Element:	Prepared:		Checked:	
23002	Attenuation Design Criteria	SG		CK	

Reference			Output
	ATTENUATION STORAGE (see GDSDS CI6.3.4)		
	10 year Attenuation Volume Required	189.70 m³	
	Attenuation Volume Provided	StormTech	Total
		191.50 m³	191.50
			OK
	NOTES: 100 Year Attenuation Volume based on Extreme rainfall matrix with 20% allowance for climate change added		
	LONG TERM STORAGE (See GDSDS CI6.3.4)		
	rainfall depth for 100 year, 6 hour eve	RD	92 mm
	Percentage of Impermeable area	PIMP	0.728
	Site Area	A	9232 m²
	Soil Index (Soil Type 3)	SOIL	0.3
	Percentage of impervious area draining to the network or directly to	α	0.54
	Percentage of pervious area draining to the network or directly	β	0.53
	Long Term Storage Required	Volxs	48.83 m³
	Long Term Storage Provided		231.73 m³
	$Vol_{xs} = RDA \cdot 10 \left[\frac{PIMP}{100} (\alpha \cdot 0.8) + \left(1 - \frac{PIMP}{100} \right) (\beta \cdot SOIL) - SOIL \right]$		
	N.B. Long term storage only represents runoff that will be infiltrated or recycled. i.e. soakaway, infiltration trench, water butt/harvesting etc. Attenuation that does not have the option to be infiltrated is not considered as long term storage.		
Criterion 4			OK
	COMMENTS		



Doherty Finegan Kelly
Consulting Structural & Civil Engineers,
Botanic Court, 30 Botanic Road, Glasnevin,
Dublin 9
Tel: 8301852 / Fax: 8602265

Project:		Design:	<input checked="" type="checkbox"/>	Telephone Log:	<input type="checkbox"/>
Calmount Rd, Ballymount - Unit 3		Minutes:	<input type="checkbox"/>	Other Record:	<input type="checkbox"/>
Project No:	Element:	Prepared:		Checked:	
23002	Site Catchment Characteristics	NS		SG/CK	

Reference	Output																																																																																																																																																				
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Project:

Calmount Rd, Ballymount - Unit 3

Design:

Telephone Log:

Minutes:

Other Record:

Project No:

23002

Infiltration Drainage - Perm Paving

Prepared:

Checked:

NS

SG/CK

Reference:

Output:

Calmount Rd, Ballymount - Extreme Rainfall Matrix

RP5 60min= 16.2 mm RP5 2d= 59.4 mm ANNUAL RAINFALL= 707.0 mm

DURATION	RETURN PERIOD (YEARS)								
	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3

Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)

Plane Infiltration - Permeable Paving

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	clay	28.1 mm/hr
FOS	Minor Inconvenience	5.00
q		0.006 m/hr

Equations Applied to Determine h_{max}

$$h_{max} = \frac{D}{n} (Ri - q) \quad (1)$$

Where:

R= $A_D/A_b =$

1.17

Assume - uniform gravel (n) 0.35

Area to be Drained

A_D 926 m²

Area to be drained --

Infiltration system dimensions

Width	-
Length	-
Base Area (A _b)	790 m ²

H_{max} Calculation

10 Year Return Period

Duration (D)	h _{max}
15 min	0.051
30 min	0.062
60 min	0.073
120 min	0.080
240 min	0.078
360 min	0.067

30 Year Return Period

Duration (D)	h _{max}
15 min	0.075
30 min	0.091
60 min	0.109
120 min	0.124
240 min	0.131
360 min	0.126

50 Year Return Period

Duration (D)	h _{max}
15 min	0.089
30 min	0.108
60 min	0.129
120 min	0.148
240 min	0.160
360 min	0.159

100 Year Return Period

Duration (D)	h _{max}
15 min	0.112
30 min	0.135
60 min	0.161
120 min	0.187
240 min	0.207
360 min	0.211

Plane Infiltration - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{nh_{max}}{q} \quad (2)$$

$$q = \frac{nh_{max}}{T_{empty}} \quad (3)$$

Event	Time to Empty
1 in 10 years	4.998 hrs
1 in 30 years	8.146 hrs
1 in 50 years	9.971 hrs
1 in 100 years	13.094 hrs

Event	Min feasible (q)
1 in 10 years	0.0006 m/hr
1 in 30 years	0.0019 m hr
1 in 50 years	0.0023 m hr
1 in 100 years	0.0031 m hr



Doherty Finegan Kelly
Consulting Structural & Civil Engineers,
Botanic Court, 30 Botanic Road, Glasnevin,
Dublin 9
Tel: 8301852 / Fax: 8602265

	Project:		Design:	<input checked="" type="checkbox"/>	Telephone Log:	<input type="checkbox"/>
	Calmount Rd, Ballymount - Unit 3		Minutes:	<input type="checkbox"/>	Other Record:	<input type="checkbox"/>
Project No:	Element:		Prepared:		Checked:	
23002	Planted swale			NS	CK	

Reference:		Output:																																																																																																																																												
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Tel: 8301852 / Fax: 8602265

Project:

Calmount Rd, Ballymount - Unit 3

Design:



Telephone Log:



Minutes:



Other Record:



Project No:

Element:

Prepared:

Checked:

23002

Planted swale

NS

CK

Reference:

Output:

Vertical Sided System

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	Soil	193.9 mm/hr
FOS	Minor Inconvenience	5.00
q		0.039 m/hr

Equations Applied to Determine hmax

$$h_{\max} = a(e^{(-bD)} - 1) \quad (1)$$

Assume - uniform gravel (n)	0.30
-----------------------------	------

Area to be Drained	
A _D	1225 m ²

where:

$$b = \frac{Pq}{A_b n} \quad (2)$$

and a is given by:

$$a = \frac{A_b}{P} - \frac{A_D i}{P q} \quad (3)$$

b=	0.265
Ab/P=	0.488

H_{max} Calculation

10 Year Return Period

Duration (D)	hmax	a
15.000 min	1.604	-25.026
30.000 min	1.936	-15.597
60.000 min	2.265	-9.727
120.000 min	2.462	-5.983
240.000 min	2.362	-3.614
360.000 min	2.114	-2.655

30 Year Return Period

Duration (D)	hmax	a
15.000 min	2.304	-35.933
30.000 min	2.773	-22.345
60.000 min	3.222	-13.840
120.000 min	3.489	-8.479
240.000 min	3.352	-5.128
360.000 min	3.009	-3.780

50 Year Return Period

Duration (D)	hmax	a
15.000 min	2.719	-42.404
30.000 min	3.255	-26.227
60.000 min	3.760	-16.151
120.000 min	4.069	-9.889
240.000 min	3.903	-5.971
360.000 min	3.512	-4.411

100 Year Return Period

Duration (D)	hmax	a
15.000 min	3.382	-52.757
30.000 min	4.035	-32.513
60.000 min	4.632	-19.895
120.000 min	4.991	-12.130
240.000 min	4.779	-7.312
360.000 min	4.297	-5.398

Vertical Sided System - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{1}{b} \log_e \left[\frac{h_{\max} + \frac{A_b}{P}}{\frac{h_{\max}}{2} + \frac{A_b}{P}} \right]$$

Event	Time to Empty
1 in 10 years	2.038 hrs
1 in 30 years	2.179 hrs
1 in 50 years	2.232 hrs
1 in 100 years	2.293 hrs

Infiltration System -- Overflow from French Drain

Return Period	Duration	Base Area (A _b)	h _{PROVIDED}	h _{max}	Q _{OVERFLOW} *
10 Years	120.000 min	40.000 m ²	1.000 m	2.462 m	0.215 l/sec
30 Years	120.000 min	40.000 m ²	1.000 m	3.489 m	0.514 l/sec
50 Years	120.000 min	40.000 m ²	1.000 m	4.069 m	0.736 l/sec
100 Years	120.000 min	40.000 m ²	1.000 m	4.991 m	1.173 l/sec

* Q_{OVERFLOW} is the averaged flow for the duration given.



TITLE: ATTENUATION
(30 Yr Return Period)

CALCS BY: NS **CHECK'D:** SG/CK

RCD.

ISSUE. 1

REV. 0

Doherty Finegan Kelly
30-32 Botanic Road, Glasnevin, Dublin 9
Tel: 830 1852, Fax: 860 2265,
E-mail: mailroom@dfk.ie

SURFACE WATER STORAGE

Storm Return Period =	30	Years
Total Site Area =	0.7487	Hectares (ha)
Areas Contributing to Drainage Network:		
Roof	0.3390	ha
Hardstanding	0.1140	ha
	ha	
Total Impermeable Area =	0.4302	ha

.....@	100%	Impermeable
.....@	80%	Impermeable
.....@	0%	Impermeable
.....@	0%	Impermeable
.....@	0%	Impermeable

Site Location:

Ballymount

Allowable Outflow = 1.97 litres/sec

Duration (min)	Rainfall 30 Year (mm)	Intensity (mm/hr)	Discharge Q (= 2.71Ai) (l/s)	Proposed Runoff (m³)	Contiguous Land Runoff (m³)	Total ** Runoff (m³)	Allowable Outflow (m³)	Storage Req'd (m³)
2	0.0	0.0	0	0	0	0	0	-0.2
5	12.0	144.0	168	50	0	60	1	59.8
10	16.8	100.8	118	71	0	85	1	83.4
15	19.7	78.8	92	83	0	99	2	97.4
30	24.7	49.4	58	104	0	124	4	120.9
60	31.0	31.0	36	130	0	156	7	149.0
120	38.8	19.4	23	163	0	195	14	181.2
240	48.6	12.2	14	204	0	245	28	216.4
360	55.4	9.2	11	233	0	279	43	236.5
720	69.5	5.8	7	292	0	350	85	264.9
1440	87.0	3.6	4	365	0	438	170	268.0
2880	98.6	2.1	2	414	0	497	340	156.2
4320	108.2	1.5	2	454	0	545	511	34.3

** Includes 20% for climate change

Storage required = 268.0 m³

TITLE: ATTENUATION

(100 Yr Return Period)

CALCS BY: CHECK'D:

NS SG/CK

RCD.

ISSUE. 1

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Areas Contributing to Drainage Network:		
Roof	0.3390	ha
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	ha	
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.....@	100%	Impermeable
.....@	80%	Impermeable
.....@	0%	Impermeable
.....@	0%	Impermeable
.....@	0%	Impermeable

Site Location:

Ballymount

Allowable Outflow = 2.72 litres/sec

Duration (min)	Rainfall 100 Year (mm)	Intensity (mm/hr)	Discharge Q (= 2.71Ai) (l/s)	Proposed Runoff (m³)	Contiguous Land Runoff (m³)	Total ** Runoff (m³)	Allowable Outflow (m³)	Storage Req'd (m³)
2	0.0	0.0	0	0	0	0	0	-0.3
5	17.6	211.2	246	74	0	89	1	87.8
10	24.5	147.0	171	103	0	123	2	121.8
15	28.8	115.2	134	121	0	145	2	142.6
30	35.7	71.4	83	150	0	180	5	174.9
60	44.1	44.1	51	185	0	222	10	212.3
120	54.6	27.3	32	229	0	275	20	255.4
240	67.5	16.9	20	283	0	340	39	300.8
360	76.4	12.7	15	321	0	385	59	326.0
720	94.6	7.9	9	397	0	476	118	358.9
1440	117.0	4.9	6	491	0	589	235	354.3
2880	129.6	2.7	3	544	0	653	470	182.7
4320	140.2	1.9	2	588	0	706	705	1.1

** Includes 20% for climate change

Storage required = 358.9 m³

STORMTECH Stormwater Management System Design Tool

ver: Aug15

PROJECT REF: 23002 - Calmount Rd, Ballymount - Unit 3

LOCATION: StormTech Trench

DATE: 09-Mar-23

CREATED BY: NS

SYSTEM PARAMETERS

Required Total Storage	359.4 m ³
Stormtech chamber model	SC740
Filtration Permeable Geo or Impermeable Geo	Filter geo
Number of Isolator Rows (IR)	1

SITE PARAMETERS

Stone Porosity	40%	
Excavation Batter Angle (degrees)	60°	Minimum Requirement
Stone Above Chambers	0.2 m	0.15
Stone Below Chambers (Long-Term Storage)	0 m	0.15 <i>Adjust to minimum</i>
In-between Row Spacing	0.15 m	0.15
Additional Storage outside Excavation. E.g manholes, Header Pipe	0 m ³	

HEADER PIPE

Is Header pipe required within excavation	No
Orientation of Header Pipe	Perp to IR
Diameter of Header Pipe	0 m
Length of Header Pipe	0 m

CHAMBER SYSTEM DIMENSIONS

	Calculated	Adopted
Number of Rows	10 ea	
Number of units per Row	17 ea	
System Installed Storage Depth (effective storage depth)	0.960 m	
Tank overall installed Width at base	14.90 m	15 m
Tank overall installed Length at Base	37.59 m	38 m
Total Effective System Storage	360.4 m ³	364.3 m ³

STORMTECH SYSTEM DETAIL

StormTech Chamber Model	SC740
Unit Width	1.295 m
Unit Length	2.17 m
Unit Height	0.76 m
Min Cover Over System	0.3 m
Max Cover Over Chamber	2.4 m
Chamber Internal Storage Vol.	1.3 m ³
Header Pipe Internal Storage Vol in Excavation	0.0 m ³

STONE AND EXCAVATION DETAIL

Volume of Dig for System	576 m ³
Width at base	15.00 m
Width at top	16.11 m
Length at base	38.00 m
Length at top	39.11 m
Depth Of System	0.96 m
Area of Dig at Base of System	570 m ²
Area of Dig at Top of System	630 m ²
Void Ratio	63%
Stone Requirement - m ³	353 m ³
Stone Requirement - tonne	579 tonne



 Doherty Finegan Kelly <i>Consulting Structural & Civil Engineers,</i>	Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265			
	Project:		Design: <input checked="" type="checkbox"/>	Telephone Log:
	Calmount Rd, Ballymount - Unit 3		Minutes: <input type="checkbox"/>	Other Record:
	Project No:	Element:	Prepared:	
	23002	Attenuation Design Criteria	Checked: SG	

Reference	Calmount Rd, Ballymount - Extreme Rainfall Matrix								Output	
	RP5 60min=	17.5 mm	RP5 2d=	63.5 mm	ANNUAL RAINFALL=				707.0 mm	
	RETURN PERIOD (YEARS)									
	DURATION	0.5	1	2	5	10	20	30	50	100
	2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	5 min	2.9	4.3	5.2	7.8	10.1	12.7	14.4	17.0	21.1
	10 min	4.1	6.0	7.1	10.9	14.0	17.6	20.2	23.6	29.4
	15 min	4.8	7.1	8.4	12.8	16.6	20.8	23.6	27.8	34.6
	30 min	6.2	9.2	10.9	16.4	20.9	26.2	29.6	34.7	42.8
	60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
	2 hr	10.9	15.7	18.2	26.9	33.6	41.4	46.6	53.9	65.5
	4 hr	14.5	20.5	23.6	34.3	42.6	52.1	58.3	67.1	81.0
	6 hr	17.0	23.9	27.6	39.6	49.0	59.5	66.5	76.3	91.7
	12 hr	22.6	31.2	35.8	50.6	62.2	75.0	83.4	95.0	113.5
	24 hr	29.8	40.7	46.3	64.8	78.7	94.3	104.4	118.4	140.4
	48 hr	37.2	49.6	55.9	76.2	91.2	107.8	118.3	133.0	155.5
	72 hr	43.2	56.8	63.7	85.4	101.4	118.7	129.8	145.0	168.2
	Allowance of 20% for Climate Change in accordance with GDSDS									
	INTERCEPTION STORAGE (First 5mm of rainfall over 80% of the impervious area, see GDSDS Vol2 Cl6.7.1 & Cl6.3.4)									
	Total Site Area	7487 m ²								
	Roof Drainage	3390 m ²								
	Hardstanding	2719 m ²								
	Porous Surfaces	790 m ²								
	Landscape	588 m ²								
	N.B. Interception Storage is where all runoff from at least the first 5mm of rainfall can be prevented from entering the receiving water. i.e. The first 5mm of rainfall is infiltrated/recycled									
Criterion 1	Interception Volume Required	(0.005 * 0.8 * 7487)	Roof	13.56 m ³	Hardstanding	10.88 m ³	Perm Area	3.16 m ³	Total	27.60 m ³
	Treatment Volume Provided	96.78 m ³	Permeable Paving	12.00 m ³	Planted Swale	34.20 m ³	StormTech		Total	142.98 m ³
	OK									
	NOTES:									
	<ul style="list-style-type: none"> Porous Surfaces: (790.0m² x 0.35m dp) x 0.35 = 96.78m³ Planted Swale: (40.0m x 1.0m x 1.0m dp) x 0.3) = 12.0m³ Stone Below IL StormTech Chambers: (15.0 x 38.0 x 0.15m dp) x 0.4 = 34.20m³ 									
	TREATMENT STORAGE (First 15mm of rainfall over 80% of the impervious area, see GDSDS Cl6.7.1 & Cl6.3.4)									
	Total Site Area	7487 m ²								
	Roof Drainage	3390 m ²								
	Hardstanding	2719 m ²								
	Porous Surfaces	790 m ²								
	Landscape	588 m ²								
	N.B. Interception and Treatment Storage are both part of Criterion 1. Therefore if interception storage is provided, then treatment storage is only required to provide for the remainder of the									
Criterion 1	Treatment Volume Required	(0.015 * 0.8 * 7487)	Roof	40.68 m ³	Hardstanding	32.63 m ³	Perm Area	9.48 m ³	Total	82.79 m ³
	Treatment Volume Provided	96.78 m ³	Permeable Paving	12.00 m ³	Planted Swale	34.20 m ³	StormTech		Total	142.98 m ³
	OK									
	NOTES:									
	As outlined above									



Doherty Finegan Kelly <i>Consulting Structural & Civil Engineers,</i>		Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265			
Project:		Design:		Telephone Log:	
Calmount Rd, Ballymount - Unit 3		Minutes:		Other Record:	
Project No:	Element:	Prepared:		Checked:	
23002	Attenuation Design Criteria	SG		CK	

Reference					Output:																																
	ATTENUATION STORAGE (see GDSDS CI6.3.4)																																				
	10 year Attenuation Volume Required 358.90 m³																																				
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	LONG TERM STORAGE (See GDSDS CI6.3.4)																																				
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	COMMENTS																																				



Doherty Finegan Kelly Consulting Structural & Civil Engineers,		Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265			
Project: Calmount Rd, Ballymount- Unit 4		Design:	<input checked="" type="checkbox"/>	Telephone Log:	<input type="checkbox"/>
Project No: 23002	Element: Site Catchment Characteristics	Minutes:	<input type="checkbox"/>	Other Record:	<input type="checkbox"/>
		Prepared:		Checked:	
		NS		SG/CK	

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<p>** The area taken in calculating QBAR/ha is 50 ha in accordance with paragraph 6.6.1 of Vol 2 of the GDSDS.</p> <p>Site Catchment Characteristics</p> <table border="1"> <tr><td>Total Site Area</td><td>11393 m²</td></tr> <tr><td>Roof</td><td>3433 m²</td></tr> <tr><td>Greenroof</td><td>290 m²</td></tr> <tr><td>Hardstanding</td><td>3911 m²</td></tr> <tr><td>Permeable areas</td><td>880 m²</td></tr> <tr><td>Landscape</td><td>2879 m²</td></tr> </table> <table border="1"> <tr><td>QBAR</td><td>0.092 m³/sec</td></tr> <tr><td>SAAR</td><td>707.0 mm</td></tr> <tr><td>SOIL</td><td>0.3</td></tr> <tr><td>AREA **</td><td>0.50 km²</td></tr> <tr><td>QBAR/ha (l/s/ha)</td><td>2.000</td></tr> </table> <p>Areas Contributing into Drainage Network:</p> <table border="1"> <tr><td>Location</td><td>Length</td><td>Width</td><td>Area</td></tr> <tr><td></td><td></td><td></td><td></td></tr> <tr><td></td><td></td><td></td><td></td></tr> <tr><td></td><td></td><td></td><td></td></tr> <tr><td></td><td></td><td></td><td></td></tr> <tr><td></td><td></td><td></td><td></td></tr> <tr><td>TOTAL</td><td></td><td></td><td>0 m²</td></tr> </table> <p>Areas Contributing into:</p> <table border="1"> <tr><td colspan="2">Permeable Paving</td></tr> <tr><td>Location</td><td>Area</td></tr> <tr><td>Perm Paving</td><td>880 m²</td></tr> <tr><td>Hardstanding</td><td>203 m²</td></tr> <tr><td>TOTAL</td><td>1083 m²</td></tr> </table> <table border="1"> <tr><td colspan="2">Planted Swale</td></tr> <tr><td>Location</td><td>Area</td></tr> <tr><td>Hardstanging</td><td>1740 m²</td></tr> <tr><td>TOTAL</td><td>1740 m²</td></tr> </table> <table border="1"> <tr><td colspan="2">Bio-Retention</td></tr> <tr><td>Location</td><td>Area</td></tr> <tr><td>Roof</td><td>3433 m²</td></tr> <tr><td>Greenroof</td><td>290 m²</td></tr> <tr><td>Hardstanding</td><td>1718 m²</td></tr> <tr><td>TOTAL</td><td>5441 m²</td></tr> </table> <table border="1"> <tr><td>Location</td><td>Area</td></tr> <tr><td></td><td></td></tr> <tr><td></td><td></td></tr> <tr><td></td><td></td></tr> <tr><td></td><td></td></tr> <tr><td>TOTAL</td><td>0 m²</td></tr> </table> <table border="1"> <tr><td>Location</td><td>Area</td></tr> <tr><td></td><td></td></tr> <tr><td></td><td></td></tr> <tr><td></td><td></td></tr> <tr><td></td><td></td></tr> <tr><td>TOTAL</td><td>0 m²</td></tr> </table> <table border="1"> <tr><td>Location</td><td>Area</td></tr> <tr><td></td><td></td></tr> <tr><td></td><td></td></tr> <tr><td></td><td></td></tr> <tr><td></td><td></td></tr> <tr><td>TOTAL</td><td>0 m²</td></tr> </table> <p>Allowable Outflow</p> <table border="1"> <tr><td>Growth Curve</td><td>1 years</td><td>QBAR</td><td>10 years</td><td>30 years</td><td>100 years</td></tr> <tr><td>Multipier</td><td>0.85</td><td>1</td><td>1.7</td><td>2.1</td><td>2.6</td></tr> <tr><td>Allowable Outflow (l/s)</td><td>1.94</td><td>2.28</td><td>3.87</td><td>4.79</td><td>5.92</td></tr> </table> <p>Calmount Rd, Ballymount - 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Project:

Calmount Rd, Ballymount - Unit 4

Design: Telephone Log:

Minutes: Other Record:

Project No:

23002

Infiltration Drainage - Perm Paving

Prepared:

Checked:

NS

SG/CK

Reference:

Output:

Calmount Rd, Ballymount - Extreme Rainfall Matrix

RP5 60min= 16.2 mm RP5 2d= 59.4 mm ANNUAL RAINFALL= 707.0 mm

DURATION	RETURN PERIOD (YEARS)								
	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
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2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3

Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)

Plane Infiltration - Permeable Paving

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	clay	491.0 mm/hr
FOS	Minor Inconvenience	5.00
q		0.098 m/hr

Equations Applied to Determine h_{max}

$$h_{max} = \frac{D}{n} (Ri - q) \quad (1)$$

Where:

R= $A_D/A_b =$ 1.23

Assume - uniform gravel (n) 0.35

Area to be Drained

A_D 1083 m²

Area to be drained --

Infiltration system dimensions

Width	-
Length	-
Base Area (A_b)	880 m ²

H_{max} Calculation

10 Year Return Period

Duration (D)	h_{max}
15 min	0.000
30 min	0.000
60 min	0.000
120 min	0.000
240 min	0.000
360 min	0.000

30 Year Return Period

Duration (D)	h_{max}
15 min	0.013
30 min	0.000
60 min	0.000
120 min	0.000
240 min	0.000
360 min	0.000

50 Year Return Period

Duration (D)	h_{max}
15 min	0.028
30 min	0.000
60 min	0.000
120 min	0.000
240 min	0.000
360 min	0.000

100 Year Return Period

Duration (D)	h_{max}
15 min	0.051
30 min	0.010
60 min	0.000
120 min	0.000
240 min	0.000
360 min	0.000

Plane Infiltration - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{nh_{max}}{q} \quad (2)$$

$$q = \frac{nh_{max}}{T_{empty}} \quad (3)$$

Event	Time to Empty
1 in 10 years	0.000 hrs
1 in 30 years	0.046 hrs
1 in 50 years	0.099 hrs
1 in 100 years	0.183 hrs

Event	Min feasible (q)
1 in 10 years	0.0000 m/hr
1 in 30 years	0.0002 m hr
1 in 50 years	0.0004 m hr
1 in 100 years	0.0007 m hr

	Doherty Finegan Kelly <i>Consulting Structural & Civil Engineers,</i>		Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265						
	Project: Calmount Rd, Ballymount - Unit 4		Design:	<input checked="" type="checkbox"/>	Telephone Log:			<input type="checkbox"/>	
Project No:	Element:	Minutes:	<input type="checkbox"/>	Other Record:			<input type="checkbox"/>		
23002	Bio-retention Area	Prepared:			Checked:				
Reference:		NS			CK			Output:	
Calmount Rd, Ballymount - Extreme Rainfall Matrix									
RP5 60min= 16.2 mm		RP5 2d= 59.4 mm		ANNUAL RAINFALL= 707.0 mm					
RETURN PERIOD (YEARS)									
DURATION	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
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30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3
Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)									
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Project No:	Element: Bio-retention Area			Prepared:	Checked:																	
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H _{max} Calculation																						
10 Year Return Period																						
Duration (D)	hmax	a																				
15.000 min	0.598	-1312.295																				
30.000 min	0.752	-825.468																				
60.000 min	0.952	-522.395																				
120.000 min	1.198	-329.096																				
240.000 min	1.503	-206.793																				
360.000 min	1.712	-157.275																				
30 Year Return Period																						
Duration (D)	hmax	a																				
15.000 min	0.855	-1875.486																				
30.000 min	1.070	-1173.883																				
60.000 min	1.339	-734.785																				
120.000 min	1.668	-457.962																				
240.000 min	2.071	-284.948																				
360.000 min	2.344	-215.345																				
50 Year Return Period																						
Duration (D)	hmax	a																				
15.000 min	1.007	-2209.582																				
30.000 min	1.253	-1374.341																				
60.000 min	1.556	-854.105																				
120.000 min	1.933	-530.748																				
240.000 min	2.388	-328.500																				
360.000 min	2.699	-247.959																				
100 Year Return Period																						
Duration (D)	hmax	a																				
15.000 min	1.251	-2744.137																				
30.000 min	1.549	-1698.892																				
60.000 min	1.909	-1047.404																				
120.000 min	2.354	-646.488																				
240.000 min	2.891	-397.706																				
360.000 min	3.253	-298.869																				
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<p>The time taken to half-empty the system is given by:</p> $\frac{1}{b} \log_e \left[\frac{h_{\max} + \frac{A_b}{P}}{h_{\max} + \frac{A_b}{P}} \right]$ <table border="1" style="margin-top: 10px; border-collapse: collapse;"> <tr> <td style="text-align: center;">Event</td> <td style="text-align: center;">Time to Empty</td> </tr> <tr> <td>1 in 10 years</td> <td>74.792 hrs</td> </tr> <tr> <td>1 in 30 years</td> <td>95.315 hrs</td> </tr> <tr> <td>1 in 50 years</td> <td>105.651 hrs</td> </tr> <tr> <td>1 in 100 years</td> <td>120.340 hrs</td> </tr> </table>							Event	Time to Empty	1 in 10 years	74.792 hrs	1 in 30 years	95.315 hrs	1 in 50 years	105.651 hrs	1 in 100 years	120.340 hrs						
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Infiltration System -- Overflow																						
Return Period	Duration	Base Area (A _b)	h _{PROVIDED}	h _{max}	Q _{OVERFLOW} *																	
10 Years	360.000 min	500.000 m ²	1.000 m	1.712 m	0.437 l/sec																	
30 Years	360.000 min	500.000 m ²	1.000 m	2.344 m	1.157 l/sec																	
50 Years	360.000 min	500.000 m ²	1.000 m	2.699 m	1.699 l/sec																	
100 Years	360.000 min	500.000 m ²	1.000 m	3.253 m	2.760 l/sec																	

* Q_{OVERFLOW} is the averaged flow for the duration given.

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		Calmount Rd, Ballymount - Unit 3			Minutes:	<input type="checkbox"/>	Other Record:		<input type="checkbox"/>	
Project No:		Element:			Prepared:			Checked:		
23002		Planted Swale			NS			CK		
Reference:									Output:	
Calmount Rd, Ballymount - Extreme Rainfall Matrix										
RP5 60min=		16.2 mm		RP5 2d=		59.4 mm		ANNUAL RAINFALL=		707.0 mm
RETURN PERIOD (YEARS)										
DURATION	0.5	1	2	5	10	20	30	50	100	
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4	
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4	
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2	
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7	
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9	
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120.000 min	5.031	-88.614																																																																																																																																																																																					
240.000 min	6.065	-54.976																																																																																																																																																																																					
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Duration (D)	hmax	a																																																																																																																																																																																					
15.000 min	3.325	-456.748																																																																																																																																																																																					
30.000 min	4.104	-282.902																																																																																																																																																																																					
60.000 min	5.027	-174.545																																																																																																																																																																																					
120.000 min	6.124	-107.865																																																																																																																																																																																					
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	Project:		Design: <input checked="" type="checkbox"/>	Telephor. Log:		
	Calmount Rd, Ballymount - Unit 4		Minutes: <input type="checkbox"/>	Other Record:		
	Project No:	Element:	Prepared:		Checked:	
23002	Attenuation Design Criteria	SG		CK		



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Telephone Log:

Minutes:

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Element:

Prepared:

Checked:

23002

Attenuation Design Criteria

SG

CK

Reference

Output:

ATTENUATION STORAGE (see GDSDS CI6.3.4)

100 year Attenuation Volume Required **0.00 m³**

Attenuation Volume Provided				Total
				0.00

NOT OK

NOTES:

100 Year Attenuation Volume based on Extreme rainfall matrix with 20% allowance for climate change added

LONG TERM STORAGE (See GDSDS CI6.3.4)

rainfall depth for 100 year, 6 hour event	RD	92 mm
Percentage of Impermeable area	PIMP	0.369
Site Area	A	11393 m ²
Soil Index (Soil Type 3)	SOIL	0.3
Percentage of impervious area draining to the network or directly to	α	0.94
Percentage of pervious area draining to the network or directly	β	0.30
Long Term Storage Required	Vol _{xs}	35.62 m³
Long Term Storage Provided		137.80 m³

$$Vol_{xs} = RDA10 \left[\frac{PIMP}{100} (\alpha 0.8) + \left(1 - \frac{PIMP}{100} \right) (\beta SOIL) - SOIL \right]$$

N.B. Long term storage only represents runoff that will be infiltrated or recycled. i.e. soakaway, infiltration trench, water butt/harvesting etc. Attenuation that does not have the option to be infiltrated is not considered as long term storage.

Criterion 4

OK

NOTES:

Vol_{xs} is the extra runoff volume for the 100 year 6 hour storm over that of the original greenfield runoff volume for the same storm. Should sufficient long term storage not be provided that can prevent all or some of this volume (Vol_{xs}) from entering the receiving waters, then the throttle should be reduced to Qbar or 2l/s for all events and the runoff should be attenuated accordingly. (see GDSDS CI6.3.4 Sub-

COMMENTS



Doherty Finegan Kelly Consulting Structural & Civil Engineers,		Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265			
Project: Calmount Rd, Ballymount - Units 5A+5B+5C		Design:	<input checked="" type="checkbox"/>	Telephone Log:	<input type="checkbox"/>
Project No: 23002	Element: Site Catchment Characteristics	Minutes:	<input type="checkbox"/>	Other Record:	<input type="checkbox"/>
		Prepared:	Checked:		
		NS	SG/CK		

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10 min	4.1	6.0	7.1	10.9	14.0	17.6	20.2	23.6	29.4																																																																																																																																																																																																																																																																																													
15 min	4.8	7.1	8.4	12.8	16.6	20.8	23.6	27.8	34.6																																																																																																																																																																																																																																																																																													
30 min	6.2	9.2	10.9	16.4	20.9	26.2	29.6	34.7	42.8																																																																																																																																																																																																																																																																																													
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9																																																																																																																																																																																																																																																																																													
2 hr	10.9	15.7	18.2	26.9	33.6	41.4	46.6	53.9	65.5																																																																																																																																																																																																																																																																																													
4 hr	14.5	20.5	23.6	34.3	42.6	52.1	58.3	67.1	81.0																																																																																																																																																																																																																																																																																													
6 hr	17.0	23.9	27.6	39.6	49.0	59.5	66.5	76.3	91.7																																																																																																																																																																																																																																																																																													
12 hr	22.6	31.2	35.8	50.6	62.2	75.0	83.4	95.0	113.5																																																																																																																																																																																																																																																																																													
24 hr	29.8	40.7	46.3	64.8	78.7	94.3	104.4	118.4	140.4																																																																																																																																																																																																																																																																																													
48 hr	37.2	49.6	55.9	76.2	91.2	107.8	118.3	133.0	155.5																																																																																																																																																																																																																																																																																													
72 hr	43.2	56.8	63.7	85.4	101.4	118.7	129.8	145.0	168.2																																																																																																																																																																																																																																																																																													



Project:

Calmount Rd, Ballymount - Unit 5

Design: Telephone Log: Minutes: Other Record:

Project No:

23002

Infiltration Drainage - Perm Paving

Prepared:

Checked:

NS

SG/CK

Reference:

Output:

Calmount Rd, Ballymount - Extreme Rainfall Matrix

RP5 60min= 16.2 mm RP5 2d= 59.4 mm ANNUAL RAINFALL= 707.0 mm

DURATION	RETURN PERIOD (YEARS)								
	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3

Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)

Plane Infiltration - Permeable Paving

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	clay	19.2 mm/hr
FOS	Minor Inconvenience	5.00
q		0.004 m/hr

Equations Applied to Determine h_{max}

$$h_{max} = \frac{D}{n} (Ri - q) \quad (1)$$

Where:

R= $A_D/A_b =$ 1.27Assume - uniform gravel (n) 0.35

Area to be Drained

 A_D 3000 m²

Area to be drained --

Infiltration system dimensions

Width	-
Length	-
Base Area (A_b)	2355 m ²

H_{max} Calculation

10 Year Return Period

Duration (D)	h_{max}
15 min	0.058
30 min	0.071
60 min	0.086
120 min	0.100
240 min	0.111
360 min	0.113

30 Year Return Period

Duration (D)	h_{max}
15 min	0.083
30 min	0.102
60 min	0.124
120 min	0.148
240 min	0.168
360 min	0.176

50 Year Return Period

Duration (D)	h_{max}
15 min	0.099
30 min	0.121
60 min	0.146
120 min	0.174
240 min	0.200
360 min	0.212

100 Year Return Period

Duration (D)	h_{max}
15 min	0.123
30 min	0.150
60 min	0.182
120 min	0.217
240 min	0.251
360 min	0.268

Plane Infiltration - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{nh_{max}}{q} \quad (2)$$

$$q = \frac{nh_{max}}{T_{empty}} \quad (3)$$

Event	Time to Empty
1 in 10 years	10.284 hrs
1 in 30 years	16.112 hrs
1 in 50 years	19.385 hrs
1 in 100 years	24.493 hrs

Event	Min feasible (q)
1 in 10 years	0.0008 m/hr
1 in 30 years	0.0026 m hr
1 in 50 years	0.0031 m hr
1 in 100 years	0.0039 m hr

	Doherty Finegan Kelly <i>Consulting Structural & Civil Engineers,</i>		Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265						
	Project:		Design:	<input checked="" type="checkbox"/>	Telephone Log:			<input type="checkbox"/>	
Calmount Rd, Ballymount - Unit 5A		Minutes:	<input type="checkbox"/>	Other Record:			<input type="checkbox"/>		
Project No:	Element:	Prepared:			Checked:				
23002	Rain Garden	NS			CK/SG				
Reference:								Output:	
Calmount Rd, Ballymount - Extreme Rainfall Matrix									
RP5 60min= 16.2 mm		RP5 2d= 59.4 mm		ANNUAL RAINFALL= 707.0 mm					
RETURN PERIOD (YEARS)									
DURATION	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3
Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)									
Contributing Area Plan									



Doherty Finegan Kelly
Consulting Structural & Civil Engineers,

Botanic Court, 30 Botanic Road, Glasnevin,
Dublin 9
Tel: 8301852 / Fax: 8602265

Project:

Calmount Rd, Ballymount - Unit 5A

Design:	<input checked="" type="checkbox"/>	Telephone Log:	<input type="checkbox"/>
Minutes:	<input type="checkbox"/>	Other Record:	<input type="checkbox"/>

Project No:

Element:

Prepared:

Checked:

23002

Rain Garden

NS

CK/SG

Reference: Output:

Vertical Sided System

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	Soil	19.2 mm/hr
FOS	Minor Inconvenience	5.00
q		0.004 m/hr

Equations Applied to Determine hmax

$$h_{\max} = a(e^{(-bD)} - 1) \quad (1)$$

Assume - uniform gravel (n)	0.30
-----------------------------	------

Area to be Drained	
A _D	250 m ²

where:

$$b = \frac{Pq}{A_b n} \quad (2)$$

Infiltration Trench dimensions

Length	
Width	
Base Area (A _b)	174 m ²
Perimeter (P)	117 m ²

and a is given by:

$$a = \frac{A_b}{P} - \frac{A_D}{Pq} \quad (3)$$

b=	0.009
Ab/P=	1.491

H_{max} Calculation

10 Year Return Period

Duration (D)	hmax	a
15 min	0.076	-35.496
30 min	0.093	-21.827
60 min	0.114	-13.317
120 min	0.134	-7.890
240 min	0.150	-4.456
360 min	0.154	-3.065

30 Year Return Period

Duration (D)	hmax	a
15 min	0.110	-51.309
30 min	0.135	-31.610
60 min	0.164	-19.281
120 min	0.195	-11.508
240 min	0.224	-6.650
360 min	0.235	-4.696

50 Year Return Period

Duration (D)	hmax	a
15 min	0.130	-60.690
30 min	0.159	-37.238
60 min	0.193	-22.631
120 min	0.230	-13.552
240 min	0.265	-7.873
360 min	0.281	-5.612

100 Year Return Period

Duration (D)	hmax	a
15 min	0.162	-75.699
30 min	0.198	-46.351
60 min	0.239	-28.058
120 min	0.285	-16.801
240 min	0.331	-9.816
360 min	0.353	-7.041

Vertical Sided System - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{1}{b} \log_e \left[\frac{h_{\max} + \frac{A_b}{P}}{\frac{h_{\max}}{2} + \frac{A_b}{P}} \right]$$

Event	Time to Empty
1 in 10 years	5.6 hrs
1 in 30 years	8.2 hrs
1 in 50 years	9.6 hrs
1 in 100 years	11.7 hrs

Infiltration System -- Overflow

Return Period	Duration	Base Area (A _b)	h _{PROVIDED}	h _{max}	Q _{OVERFLOW} *
10 Years	360 min	174 m ²	0.600 m	0.154 m	0.000 l/sec
30 Years	360 min	174 m ²	0.600 m	0.235 m	0.000 l/sec
50 Years	360 min	174 m ²	0.600 m	0.281 m	0.000 l/sec
100 Years	360 min	174 m ²	0.600 m	0.353 m	0.000 l/sec

* Q_{OVERFLOW} is the averaged flow for the duration given.

	Doherty Finegan Kelly <i>Consulting Structural & Civil Engineers,</i>		Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265						
	Project:		Design:	<input checked="" type="checkbox"/>	Telephone Log:			<input type="checkbox"/>	
Calmount Rd, Ballymount - Unit 5B		Minutes:	<input type="checkbox"/>	Other Record:			<input type="checkbox"/>		
Project No:	Element:	Prepared:			Checked:				
23002	Rain Garden	NS			CK/SG				
Reference:								Output:	
Calmount Rd, Ballymount - Extreme Rainfall Matrix									
RP5 60min= 16.2 mm		RP5 2d= 59.4 mm		ANNUAL RAINFALL= 707.0 mm					
RETURN PERIOD (YEARS)									
DURATION	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3
Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)									
Contributing Area Plan									



Doherty Finegan Kelly

Consulting Structural & Civil Engineers,

Botanic Court, 30 Botanic Road, Glasnevin,

Dublin 9

Tel: 8301852 / Fax: 8602265

Project:

Calmount Rd, Ballymount - Unit 5B

Design:



Telephone Log:



Minutes:



Other Record:



Project No:

Element:

Prepared:

Checked:

23002

Rain Garden

NS

CK/SG

Reference:

Output:

Vertical Sided System

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	Soil	19.2 mm/hr
FOS	Minor Inconvenience	5.00
q		0.004 m/hr

Equations Applied to Determine hmax

$$h_{\max} = a(e^{(-bD)} - 1) \quad (1)$$

Assume - uniform gravel (n)	0.30
-----------------------------	------

Area to be Drained	
A _D	267 m ²

where:

$$b = \frac{Pq}{A_b n} \quad (2)$$

and a is given by:

$$a = \frac{A_b}{P} - \frac{A_D i}{P q} \quad (3)$$

b=	0.008
Ab/P=	1.557

H_{max} Calculation

10 Year Return Period

Duration (D)	hmax	a
15 min	0.077	-37.776
30 min	0.095	-23.240
60 min	0.116	-14.190
120 min	0.137	-8.418
240 min	0.154	-4.767
360 min	0.158	-3.288

30 Year Return Period

Duration (D)	hmax	a
15 min	0.112	-54.593
30 min	0.138	-33.643
60 min	0.168	-20.532
120 min	0.199	-12.266
240 min	0.229	-7.100
360 min	0.241	-5.022

50 Year Return Period

Duration (D)	hmax	a
15 min	0.132	-64.569
30 min	0.162	-39.629
60 min	0.197	-24.095
120 min	0.235	-14.440
240 min	0.271	-8.401
360 min	0.288	-5.996

100 Year Return Period

Duration (D)	hmax	a
15 min	0.165	-80.530
30 min	0.202	-49.320
60 min	0.244	-29.867
120 min	0.291	-17.896
240 min	0.338	-10.467
360 min	0.361	-7.516

Vertical Sided System - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{1}{b} \log_e \left[\frac{h_{\max} + \frac{A_b}{P}}{\frac{h_{\max}}{2} + \frac{A_b}{P}} \right]$$

Event	Time to Empty
1 in 10 years	5.7 hrs
1 in 30 years	8.5 hrs
1 in 50 years	9.9 hrs
1 in 100 years	12.0 hrs

Infiltration System -- Overflow

Return Period	Duration	Base Area (A _b)	h _{PROVIDED}	h _{max}	Q _{OVERFLOW} *
10 Years	360 min	183 m ²	0.600 m	0.158 m	0.000 l/sec
30 Years	360 min	183 m ²	0.600 m	0.241 m	0.000 l/sec
50 Years	360 min	183 m ²	0.600 m	0.288 m	0.000 l/sec
100 Years	360 min	183 m ²	0.600 m	0.361 m	0.000 l/sec

* Q_{OVERFLOW} is the averaged flow for the duration given.

TITLE: ATTENUATION

(30 Yr Return Period)

CALCS BY: CHECK'D:

NS

SG/CK

RCD.

ISSUE. 1

REV. 0

**Doherty Finegan Kelly**

30-32 Botanic Road, Glasnevin, Dublin 9

Tel: 830 1852, Fax: 860 2265,

E-mail: mailroom@dfk.ie

SURFACE WATER STORAGE

Storm Return Period =	30	Years
Total Site Area =	0.7587	Hectares (ha)
Areas Contributing to Drainage Network:		
Greenroof	0.1023	ha
Hardstanding	0.0570	ha
Permeable area	0.0000	ha
Total Impermeable Area =	0.1274	ha

.....@	80%	Impermeable
.....@	80%	Impermeable
.....@	0%	Impermeable
.....@	0%	Impermeable
.....@	0%	Impermeable

Site Location:

Ballymount

Allowable Outflow = 3.19 litres/sec

Duration (min)	Rainfall 30 Year (mm)	Intensity (mm/hr)	Discharge Q (= 2.71Ai) (l/s)	Proposed Runoff (m³)	Contiguous Land Runoff (m³)	Total ** Runoff (m³)	Allowable Outflow (m³)	Storage Req'd (m³)
2	0.0	0.0	0	0	0	0	0	-0.4
5	12.0	144.0	50	15	0	18	1	16.9
10	16.8	100.8	35	21	0	25	2	23.2
15	19.7	78.8	27	24	0	29	3	26.5
30	24.7	49.4	17	31	0	37	6	31.1
60	31.0	31.0	11	39	0	46	11	34.8
120	38.8	19.4	7	48	0	58	23	34.9
240	48.6	12.2	4	60	0	73	46	26.6
360	55.4	9.2	3	69	0	83	69	13.8
720	69.5	5.8	2	86	0	104	138	-34.1
1440	87.0	3.6	1	108	0	130	276	-145.8
2880	98.6	2.1	1	123	0	147	551	-404.1
4320	108.2	1.5	1	135	0	161	827	-665.4

** Includes 20% for climate change

Storage required = 34.9 m³



TITLE: ATTENUATION
(100 Yr Return Period)

CALCS BY: NS **CHECK'D:** SG/CK

RCD.

ISSUE. 1

REV. 0

Doherty Finegan Kelly
30-32 Botanic Road, Glasnevin, Dublin 9
Tel: 830 1852, Fax: 860 2265,
E-mail: mailroom@dfk.ie

SURFACE WATER STORAGE

Storm Return Period =	100	Years
Total Site Area =	0.7587	Hectares (ha)
Areas Contributing to Drainage Network:		
Greenroof	0.1023	ha
Hardstanding	0.0570	ha
Permeable area	0.0000	ha
Total Impermeable Area =	0.1274	ha

.....@	80%	Impermeable
.....@	80%	Impermeable
.....@	0%	Impermeable
.....@	0%	Impermeable
.....@	0%	Impermeable

Site Location:

Ballymount

Allowable Outflow = 3.95 litres/sec

Duration (min)	Rainfall 100 Year (mm)	Intensity (mm/hr)	Discharge Q (= 2.71Ai) (l/s)	Proposed Runoff (m³)	Contiguous Land Runoff (m³)	Total ** Runoff (m³)	Allowable Outflow (m³)	Storage Req'd (m³)
2	0.0	0.0	0	0	0	0	0	-0.5
5	17.6	211.2	73	22	0	26	1	25.1
10	24.5	147.0	51	30	0	37	2	34.2
15	28.8	115.2	40	36	0	43	4	39.4
30	35.7	71.4	25	44	0	53	7	46.2
60	44.1	44.1	15	55	0	66	14	51.6
120	54.6	27.3	9	68	0	81	28	53.0
240	67.5	16.9	6	84	0	101	57	43.8
360	76.4	12.7	4	95	0	114	85	28.7
720	94.6	7.9	3	118	0	141	171	-29.5
1440	117.0	4.9	2	145	0	175	341	-166.7
2880	129.6	2.7	1	161	0	193	683	-489.2
4320	140.2	1.9	1	174	0	209	1024	-814.7

** Includes 20% for climate change

Storage required = 53.0 m³

STORMTECH Stormwater Management System Design Tool

ver: Aug15

PROJECT REF: 23002 - Calmount Rd, Ballymount - Warehousing

LOCATION: StormTech Trench (Unit 5)

DATE: 09-Mar-23

CREATED BY: NS

SYSTEM PARAMETERS

Required Total Storage	53 m ³
Stormtech chamber model	SC310
Filtration Permeable Geo or Impermeable Geo	Filter geo
Number of Isolator Rows (IR)	1

SITE PARAMETERS

Stone Porosity	40%	
Excavation Batter Angle (degrees)	60 °	Minimum Requirement
Stone Above Chambers	0.15 m	0.15
Stone Below Chambers (Long-Term Storage)	0 m	0.15 <i>Adjust to minimum</i>
In-between Row Spacing	0.15 m	0.15
Additional Storage outside Excavation. E.g manholes, Header Pipe	0 m ³	

HEADER PIPE

Is Header pipe required within excavation	No
Orientation of Header Pipe	Perp to IR
Diameter of Header Pipe	0 m
Length of Header Pipe	0 m

CHAMBER SYSTEM DIMENSIONS

	Calculated	Adopted
Number of Rows	3 ea	
Number of units per Row	20 ea	
System Installed Storage Depth (effective storage depth)	0.555 m	
Tank overall installed Width at base	3.50 m	3.5 m
Tank overall installed Length at Base	44.1 m	45 m
Total Effective System Storage	52.8 m³	53.6 m³

STORMTECH SYSTEM DETAIL

StormTech Chamber Model	SC310
Unit Width	0.865 m
Unit Length	2.17 m
Unit Height	0.405 m
Min Cover Over System	0.25 m
Max Cover Over Chamber	2.4 m
Chamber Internal Storage Vol.	0.42 m ³
Header Pipe Internal Storage Vol in Excavation	0.0 m ³

STONE AND EXCAVATION DETAIL

Volume of Dig for System	96 m ³
Width at base	3.50 m
Width at top	4.14 m
Length at base	45.00 m
Length at top	45.64 m
Depth Of System	0.56 m
Area of Dig at Base of System	158 m ²
Area of Dig at Top of System	189 m ²
Void Ratio	56%
Stone Requirement - m ³	71 m ³
Stone Requirement - tonne	116 tonne



Doherty Finegan Kelly Consulting Structural & Civil Engineers,		Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265			
Project: Calmount Rd, Ballymount - Unit 5		Design: <input checked="" type="checkbox"/>	Telephone Log:		
Project No: 23002	Element: Attenuation Design Criteria	Minutes: <input type="checkbox"/>	Other Record:		
		Prepared: SG	Checked: CK		

Reference					Output:					
Calmount Rd, Ballymount - Extreme Rainfall Matrix										
	RP5 60min= 17.5 mm	RP5 2d= 63.5 mm		ANNUAL RAINFALL= 707.0 mm						
RETURN PERIOD (YEARS)										
	DURATION	0.5	1	2	5	10	20	30	50	100
	2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	5 min	2.9	4.3	5.2	7.8	10.1	12.7	14.4	17.0	21.1
	10 min	4.1	6.0	7.1	10.9	14.0	17.6	20.2	23.6	29.4
	15 min	4.8	7.1	8.4	12.8	16.6	20.8	23.6	27.8	34.6
	30 min	6.2	9.2	10.9	16.4	20.9	26.2	29.6	34.7	42.8
	60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
	2 hr	10.9	15.7	18.2	26.9	33.6	41.4	46.6	53.9	65.5
	4 hr	14.5	20.5	23.6	34.3	42.6	52.1	58.3	67.1	81.0
	6 hr	17.0	23.9	27.6	39.6	49.0	59.5	66.5	76.3	91.7
	12 hr	22.6	31.2	35.8	50.6	62.2	75.0	83.4	95.0	113.5
	24 hr	29.8	40.7	46.3	64.8	78.7	94.3	104.4	118.4	140.4
	48 hr	37.2	49.6	55.9	76.2	91.2	107.8	118.3	133.0	155.5
	72 hr	43.2	56.8	63.7	85.4	101.4	118.7	129.8	145.0	168.2
	Allowance of 20% for Climate Change in accordance with GDSDS									
INTERCEPTION STORAGE (First 5mm of rainfall over 80% of the impervious area, see GDSDS Vol2 Cl6.7.1 & Cl6.3.4)										
Criterion 1	Total Site Area	7587 m ²								
	Roof Drainage	0 m ²								
	Grenroof	1542 m ²								
	Hardstanding	1882 m ²								
	Porous Surfaces	2355 m ²								
	Landscape	1808 m ²								
N.B. Interception Storage is where all runoff from at least the first 5mm of rainfall can be prevented from entering the receiving water. i.e. The first 5mm of rainfall is infiltrated/recycled onsite										
OK										
Interception Volume Required (0.005 * 0.8 *										
Roof 6.17 m ³										
Hardstanding 7.53 m ³										
Perm Area 9.42 m ³										
Total 23.12 m ³										
OK										
Interception Volume Provided										
Permeable Paving 96.78 m ³										
Rain Gardens 64.26 m ³										
StormTech 9.45 m ³										
Total 170.49 m ³										
OK										
NOTES:										
<ul style="list-style-type: none"> • Porous Surfaces: $(790.0\text{m}^2 \times 0.35\text{m dp}) \times 0.35 = 96.78\text{m}^3$ • Rain Garden - Unit 5A: $(174.0\text{m}^2 \times 0.6\text{m dp}) \times 0.3 = 31.32\text{m}^3$ • Rain Garden - Unit 5B: $(183.0\text{m}^2 \times 0.6\text{m dp}) \times 0.3 = 32.94\text{m}^3$ • Stone Below IL StormTech Chambers: $(3.5 \times 45.0 \times 0.15\text{m dp}) \times 0.4 = 9.45\text{m}^3$ 										
TREATMENT STORAGE (First 15mm of rainfall over 80% of the impervious area, see GDSDS Cl6.7.1 & Cl6.3.4)										
Criterion 1	Total Site Area	7587 m ²								
	Roof Drainage	0 m ²								
	Grenroof	1542 m ²								
	Hardstanding	1882 m ²								
	Porous Surfaces	2355 m ²								
	Landscape	1808 m ²								
N.B. Interception and Treatment Storage are both part of Criterion 1. Therefore if interception storage is provided, then treatment storage is only required to provide for the remainder of the										
OK										
Treatment Volume Required (0.015 * 0.8 *										
Roof 18.50 m ³										
Hardstanding 22.58 m ³										
Perm Area 28.26 m ³										
Total 69.35 m ³										
OK										
Treatment Volume Provided										
As Outlined above										
Greenroof 23.13 m ³										
Total 193.62 m ³										
OK										
NOTES:										
As outlined above plus:										
Greenroof (Assumed to treat first 15mm rainfall minimum): $1542.0\text{m}^2 \times 0.015\text{m} = 23.13\text{m}^3$										



Doherty Finegan Kelly <i>Consulting Structural & Civil Engineers,</i>		Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265			
Project:		Design:		Telephone Log:	
Calmount Rd, Ballymount - Unit 5		Minutes:		Other Record:	
Project No:	Element:	Prepared:		Checked:	
23002	Attenuation Design Criteria	SG		CK	

Reference					Output																																
	ATTENUATION STORAGE (see GDSDS CI6.3.4)																																				
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	COMMENTS																																				



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Dublin 9
Tel: 8301852 / Fax: 8602265

		Project:	Design:	<input checked="" type="checkbox"/>	Telephone Log:	<input type="checkbox"/>
Calmount Rd, Ballymount - Warehousing		Minutes:	<input type="checkbox"/>	Other Record:	<input type="checkbox"/>	
Project No:	Element:	Prepared:			Checked:	
23014	Site Catchment Characteristics - Unit 6	NS			SG/CK	

Reference	Output																																																																																																																																																				
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15 min	4.8	7.1	8.4	12.8	16.6	20.8	23.6	27.8	34.6																																																																																																																																												
30 min	6.2	9.2	10.9	16.4	20.9	26.2	29.6	34.7	42.8																																																																																																																																												
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9																																																																																																																																												
2 hr	10.9	15.7	18.2	26.9	33.6	41.4	46.6	53.9	65.5																																																																																																																																												
4 hr	14.5	20.5	23.6	34.3	42.6	52.1	58.3	67.1	81.0																																																																																																																																												
6 hr	17.0	23.9	27.6	39.6	49.0	59.5	66.5	76.3	91.7																																																																																																																																												
12 hr	22.6	31.2	35.8	50.6	62.2	75.0	83.4	95.0	113.5																																																																																																																																												
24 hr	29.8	40.7	46.3	64.8	78.7	94.3	104.4	118.4	140.4																																																																																																																																												
48 hr	37.2	49.6	55.9	76.2	91.2	107.8	118.3	133.0	155.5																																																																																																																																												
72 hr	43.2	56.8	63.7	85.4	101.4	118.7	129.8	145.0	168.2																																																																																																																																												
	Allowance of 20% for Climate Change in accordance with GDSDS																																																																																																																																																				



Project:

Calmount Rd, Ballymount - Unit 6

Design:



Telephone Log:



Minutes:



Other Record:



Project No:

23002

Infiltration Drainage - Perm Paving

Prepared:

Checked:

NS

SG/CK

Reference:

Output:

Calmount Rd, Ballymount - Extreme Rainfall Matrix

RP5 60min= 16.2 mm RP5 2d= 59.4 mm ANNUAL RAINFALL= 707.0 mm

DURATION	RETURN PERIOD (YEARS)								
	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3

Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)

Plane Infiltration - Permeable Paving

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	clay	56.9 mm/hr
FOS	Minor Inconvenience	5.00
q		0.011 m/hr

Equations Applied to Determine h_{max}

$$h_{max} = \frac{D}{n} (Ri - q) \quad (1)$$

Where:

R= $A_D/A_b =$

1.24

Assume - uniform gravel (n) 0.40

Area to be Drained

A_D 1161 m²

Area to be drained --

Infiltration system dimensions

Width	-
Length	-
Base Area (A _b)	935 m ²

H_{max} Calculation

10 Year Return Period

Duration (D)	h _{max}
15 min	0.044
30 min	0.051
60 min	0.054
120 min	0.047
240 min	0.018
360 min	0.000

30 Year Return Period

Duration (D)	h _{max}
15 min	0.066
30 min	0.078
60 min	0.087
120 min	0.088
240 min	0.067
360 min	0.036

50 Year Return Period

Duration (D)	h _{max}
15 min	0.079
30 min	0.093
60 min	0.106
120 min	0.110
240 min	0.094
360 min	0.066

100 Year Return Period

Duration (D)	h _{max}
15 min	0.100
30 min	0.119
60 min	0.136
120 min	0.146
240 min	0.138
360 min	0.114

Plane Infiltration - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{nh_{max}}{q} \quad (2)$$

$$q = \frac{nh_{max}}{T_{empty}} \quad (3)$$

Event	Time to Empty
1 in 10 years	1.894 hrs
1 in 30 years	3.080 hrs
1 in 50 years	3.879 hrs
1 in 100 years	5.149 hrs

Event	Min feasible (q)
1 in 10 years	0.0004 m/hr
1 in 30 years	0.0015 m hr
1 in 50 years	0.0018 m hr
1 in 100 years	0.0024 m hr

	<p>Doherty Finegan Kelly Consulting Structural & Civil Engineers, Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265</p>									
		Project:			Design:	<input checked="" type="checkbox"/>	Telephone Log:		<input type="checkbox"/>	
		Calmount Rd, Ballymount - Unit 6			Minutes:	<input type="checkbox"/>	Other Record:		<input type="checkbox"/>	
Project No:		Element:			Prepared:			Checked:		
23002		Planted Swale			NS			CK		
Reference:									Output:	
Calmount Rd, Ballymount - Extreme Rainfall Matrix										
RP5 60min=		16.2 mm		RP5 2d=		59.4 mm		ANNUAL RAINFALL=		707.0 mm
RETURN PERIOD (YEARS)										
DURATION	0.5	1	2	5	10	20	30	50	100	
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4	
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4	
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2	
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7	
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9	
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8	
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3	
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3	
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5	
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9	
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2	
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3	
Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)										
Contributing Area Plan										

	Doherty Finegan Kelly <i>Consulting Structural & Civil Engineers,</i>		Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265																																													
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* Q _{OVERFLOW} is the averaged flow for the duration given.																																																

TITLE: ATTENUATION
(30 Yr Return Period)

CALCS BY: CHECK'D:

NS SG/CK

RCD.

ISSUE. 1

REV. 0



Doherty Finegan Kelly
30-32 Botanic Road, Glasnevin, Dublin 9
Tel: 830 1852, Fax: 860 2265,
E-mail: mailroom@dfk.ie

SURFACE WATER STORAGE

Storm Return Period =	30	Years
Total Site Area =	0.9435	Hectares (ha)
Areas Contributing to Drainage Network:		
Roof area	0.0000	ha
Greenroof area	0.0000	ha
Hardstanding	0.3186	ha
		ha
		ha
		ha
Total Impermeable Area =	0.2549	ha

.....@	0%	Impermeable
.....@	0%	Impermeable
.....@	80%	Impermeable
.....@	0%	Impermeable
.....@	0%	Impermeable

Site Location:

Ballymount

Allowable Outflow = 1.40 litres/sec

Duration (min)	Rainfall 30 Year (mm)	Intensity (mm/hr)	Discharge Q (= 2.71Ai) (l/s)	Proposed Runoff (m³)	Contiguous Land Runoff (m³)	Total ** Runoff (m³)	Allowable Outflow (m³)	Storage Req'd (m³)
2	0.0	0.0	0	0	0	0	0	-0.2
5	12.0	144.0	99	30	0	36	0	35.4
10	16.8	100.8	70	42	0	50	1	49.3
15	19.7	78.8	54	49	0	59	1	57.5
30	24.7	49.4	34	61	0	74	3	71.2
60	31.0	31.0	21	77	0	93	5	87.5
120	38.8	19.4	13	96	0	116	10	105.7
240	48.6	12.2	8	121	0	145	20	124.9
360	55.4	9.2	6	138	0	165	30	135.1
720	69.5	5.8	4	173	0	207	60	146.9
1440	87.0	3.6	3	216	0	260	121	138.6
2880	98.6	2.1	1	245	0	294	242	52.3
4320	108.2	1.5	1	269	0	323	363	-40.0

** Includes 20% for climate change

Storage required = 146.9 m³

TITLE: ATTENUATION

(100 Yr Return Period)

CALCS BY: CHECK'D:

NS

SG/CK

RCD.

ISSUE. 1

REV. 0

**Doherty Finegan Kelly**

30-32 Botanic Road, Glasnevin, Dublin 9

Tel: 830 1852, Fax: 860 2265,

E-mail: mailroom@dfk.ie

SURFACE WATER STORAGE

Storm Return Period =	100	Years
Total Site Area =	0.9435	Hectares (ha)
Areas Contributing to Drainage Network:		
Roof area	0.0000	ha
Greenroof area	0.0000	ha
Hardstanding	0.3186	ha
		ha
		ha
		ha
Total Impermeable Area =	0.2549	ha

.....@	0%	Impermeable
.....@	0%	Impermeable
.....@	80%	Impermeable
.....@	0%	Impermeable
.....@	0%	Impermeable

Site Location:

Ballymount

Allowable Outflow = 2.35 litres/sec

Duration (min)	Rainfall 100 Year (mm)	Intensity (mm/hr)	Discharge Q (= 2.71Ai) (l/s)	Proposed Runoff (m³)	Contiguous Land Runoff (m³)	Total ** Runoff (m³)	Allowable Outflow (m³)	Storage Req'd (m³)
2	0.0	0.0	0	0	0	0	0	-0.3
5	17.6	211.2	146	44	0	53	1	51.8
10	24.5	147.0	102	61	0	73	1	71.7
15	28.8	115.2	80	72	0	86	2	83.8
30	35.7	71.4	49	89	0	107	4	102.3
60	44.1	44.1	30	110	0	132	8	123.1
120	54.6	27.3	19	136	0	163	17	146.0
240	67.5	16.9	12	168	0	201	34	167.6
360	76.4	12.7	9	190	0	228	51	177.2
720	94.6	7.9	5	235	0	282	102	180.8
1440	117.0	4.9	3	291	0	349	203	146.1
2880	129.6	2.7	2	322	0	387	406	-19.4
4320	140.2	1.9	1	349	0	418	609	-190.8

** Includes 20% for climate change

Storage required = 180.8 m³

STORMTECH Stormwater Management System Design Tool

ver: Aug15

PROJECT REF: 23002 - Calmount Rd, Ballymount - Unit 6

LOCATION: StormTech Trench

DATE: 09-Mar-23

CREATED BY: NS

SYSTEM PARAMETERS

Required Total Storage	180.8 m ³
Stormtech chamber model	SC740
Filtration Permeable Geo or Impermeable Geo	Filter geo
Number of Isolator Rows (IR)	1

SITE PARAMETERS

Stone Porosity	40%	
Excavation Batter Angle (degrees)	60°	Minimum Requirement
Stone Above Chambers	0.2 m	0.15
Stone Below Chambers (Long-Term Storage)	0 m	0.15 <i>Adjust to minimum</i>
In-between Row Spacing	0.15 m	0.15
Additional Storage outside Excavation. E.g manholes, Header Pipe	0 m ³	

HEADER PIPE

Is Header pipe required within excavation	No
Orientation of Header Pipe	Perp to IR
Diameter of Header Pipe	0 m
Length of Header Pipe	0 m

CHAMBER SYSTEM DIMENSIONS

	Calculated	Adopted
Number of Rows	5 ea	
Number of units per Row	16 ea	
System Installed Storage Depth (effective storage depth)	0.960 m	0.96 m
Tank overall installed Width at base	7.68 m	8 m
Tank overall installed Length at Base	35.42 m	36 m
Total Effective System Storage	176.8 m ³	183.2 m ³

STORMTECH SYSTEM DETAIL

StormTech Chamber Model	SC740
Unit Width	1.295 m
Unit Length	2.17 m
Unit Height	0.76 m
Min Cover Over System	0.3 m
Max Cover Over Chamber	2.4 m
Chamber Internal Storage Vol.	1.3 m ³
Header Pipe Internal Storage Vol in Excavation	0.0 m ³

STONE AND EXCAVATION DETAIL

Volume of Dig for System	300 m ³
Width at base	8.00 m
Width at top	9.11 m
Length at base	36.00 m
Length at top	37.11 m
Depth Of System	0.96 m
Area of Dig at Base of System	288 m ²
Area of Dig at Top of System	338 m ²
Void Ratio	61%
Stone Requirement - m ³	195 m ³
Stone Requirement - tonne	321 tonne

	Doherty Finegan Kelly Consulting Structural & Civil Engineers,		Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265				
	Project: Calmount Rd, Ballymount - Unit 6		Design: <input checked="" type="checkbox"/>	Telephone Log:			
Project No: 23002	Element: Attenuation Design Criteria	Minutes: <input type="checkbox"/>	Other Record:				
		Prepared: SG	Checked: CK				

Reference								Output																																																																																																																																																									
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	Doherty Finegan Kelly <i>Consulting Structural & Civil Engineers,</i>	Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265																																				
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N.B. Long term storage only represents runoff that will be infiltrated or recycled. i.e. soakaway, infiltration trench, water butt/harvesting etc. Attenuation that does not have the option to be infiltrated is not considered as long term storage.																																						
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Dublin 9
Tel: 8301852 / Fax: 8602265**

	Project:	Design:	<input checked="" type="checkbox"/>	Telephone Log:	<input type="checkbox"/>
	Calmount Rd, Ballymount - Unit 7 (Cafe)		Minutes:	<input type="checkbox"/>	Other Record:
Project No: 23002	Element:	Prepared:		Checked:	
	Site Catchment Characteristics		NS		SG/CK



Project:

Calmount Rd, Ballymount - Unit 7 (Café)

Design:	<input checked="" type="checkbox"/>	Telephone Log:	<input type="checkbox"/>
Minutes:	<input type="checkbox"/>	Other Record:	<input type="checkbox"/>

Project No:

23002

Infiltration Drainage - Perm Paving

Prepared:

Checked:

NS

SG/CK

Reference:

Output:

Calmount Rd, Ballymount - Extreme Rainfall Matrix

RP5 60min= 16.2 mm RP5 2d= 59.4 mm ANNUAL RAINFALL= 707.0 mm

DURATION	RETURN PERIOD (YEARS)								
	0.5	1	2	5	10	20	30	50	100
2 min	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5 min	34.6	51.8	61.9	93.6	121.0	152.6	172.8	204.5	253.4
10 min	24.5	36.0	42.5	65.5	84.2	105.8	121.0	141.8	176.4
15 min	19.2	28.3	33.6	51.4	66.2	83.0	94.6	111.4	138.2
30 min	12.5	18.5	21.8	32.9	41.8	52.3	59.3	69.4	85.7
60 min	8.3	12.0	14.0	21.0	26.5	32.9	37.2	43.2	52.9
2 hr	5.5	7.9	9.1	13.4	16.8	20.7	23.3	26.9	32.8
4 hr	3.6	5.1	5.9	8.6	10.7	13.0	14.6	16.8	20.3
6 hr	2.8	4.0	4.6	6.6	8.2	9.9	11.1	12.7	15.3
12 hr	1.9	2.6	3.0	4.2	5.2	6.3	7.0	7.9	9.5
24 hr	1.2	1.7	1.9	2.7	3.3	3.9	4.4	4.9	5.9
48 hr	0.8	1.0	1.2	1.6	1.9	2.2	2.5	2.8	3.2
72 hr	0.6	0.8	0.9	1.2	1.4	1.6	1.8	2.0	2.3

Rainfall intensity shown as mm/hr. (includes 20% allowance for climate change)

Plane Infiltration - Permeable Paving

From CIRIA Report No. 156(1996) - Infiltration Drainage Manual of Good Practice

Description	Type	Result
Infiltration Rate	clay	90.4 mm/hr
FOS	Minor Inconvenience	3.00
q		0.030 m/hr

Equations Applied to Determine h_{max}

$$h_{max} = \frac{D}{n} (Ri - q) \quad (1)$$

Where:

R= $A_D/A_b =$

1.21

Assume - uniform gravel (n) 0.30

Area to be Drained

A_D 536 m²

Area to be drained --

Infiltration system dimensions

Width	-
Length	-
Base Area (A _b)	442 m ²

H_{max} Calculation

10 Year Return Period

Duration (D)	h _{max}
15 min	0.042
30 min	0.034
60 min	0.007
120 min	0.000
240 min	0.000
360 min	0.000

30 Year Return Period

Duration (D)	h _{max}
15 min	0.070
30 min	0.070
60 min	0.050
120 min	0.000
240 min	0.000
360 min	0.000

50 Year Return Period

Duration (D)	h _{max}
15 min	0.087
30 min	0.090
60 min	0.074
120 min	0.017
240 min	0.000
360 min	0.000

100 Year Return Period

Duration (D)	h _{max}
15 min	0.115
30 min	0.123
60 min	0.113
120 min	0.064
240 min	0.000
360 min	0.000

Plane Infiltration - Time to Empty

The time taken to half-empty the system is given by:

$$\frac{nh_{max}}{q} \quad (2)$$

$$q = \frac{nh_{max}}{T_{empty}} \quad (3)$$

Event	Time to Empty
1 in 10 years	0.416 hrs
1 in 30 years	0.701 hrs
1 in 50 years	0.896 hrs
1 in 100 years	1.224 hrs

Event	Min feasible (q)
1 in 10 years	0.0003 m/hr
1 in 30 years	0.0009 m hr
1 in 50 years	0.0011 m hr
1 in 100 years	0.0015 m hr

 Doherty Finegan Kelly <i>Consulting Structural & Civil Engineers,</i>	Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265								
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Calmount Rd, Ballymount - Unit 7 (Cafe)				Minutes:	<input type="checkbox"/>	Other Record:			
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23002	Bio-retention Area #1				NS			SG/CK	
Reference:									Output:
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Contributing Area Plan									

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Doherty Finegan Kelly Consulting Structural & Civil Engineers,		Botanic Court, 30 Botanic Road, Glasnevin, Dublin 9 Tel: 8301852 / Fax: 8602265			
Project:		Design: <input checked="" type="checkbox"/>		Telephone Log:	
Calmount Rd, Ballymount - Unit 7 (Café)		Minutes: <input type="checkbox"/>		Other Record:	
Project No:	Element:	Prepared:		Checked:	
23002	Attenuation Design Criteria	SG		CK	

Reference							Output																																																																																																																																																								
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<p>NOTES:</p> <ul style="list-style-type: none"> • Perm Paving: (442.0m² x 0.35m dp) x 0.35 = 54.15m³ • Grasscrete: (75.0m² x 0.2 5m dp) x 0.35 = 6.56m³ • Bio-retention Area #1: (50.0m² x 0.6m dp) x 0.3) = 9.0m³ • Bio-retention Area #2: (157.0m² x 0.6m dp) x 0.3) = 28.26m³ 																																																																																																																																																															
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Project No: 23002		Element: Attenuation Design Criteria	Minutes:		Other Record:			
			Prepared:		Checked:			
			SG		CK			
Reference							Output:	
	ATTENUATION STORAGE (see GDSDS CI6.3.4)							
	100 year Attenuation Volume Required		0.00 m ³					
	Attenuation Volume Provided					Total	NOT OK	
						0.00		
<p>NOTES: 100 Year Attenuation Volume based on Extreme rainfall matrix with 20% allowance for climate change added</p>								
LONG TERM STORAGE (See GDSDS CI6.3.4)								
Criterion 4	rainfall depth for 100 year, 6 hour eve	RD	92 mm					$Vol_{st} = RDA.10 \left[\frac{PIMP}{100} (\alpha 0.8) + \left(1 - \frac{PIMP}{100} \right) \beta SOIL - SOIL \right]$ <p>N.B. Long term storage only represents runoff that will be infiltrated or recycled. i.e. soakaway, infiltration trench, water butt/harvesting etc. Attenuation that does not have the option to be infiltrated is not considered as long term storage.</p>
	Percentage of Impermeable area	PIMP	0.273					
	Site Area	A	2188 m ²					
	Soil Index (Soil Type 3)	SOIL	0.3					
	Percentage of impervious area draining to the network or directly to	α	0.00					
	Percentage of pervious area draining to the network or directly	β	0.00					
	Long Term Storage Required	Vol _{xs}	-60.18 m³					
	Long Term Storage Provided		97.97 m³					
<p>NOTES: Vol_{xs} is the extra runoff volume for the 100 year 6 hour storm over that of the original greenfield runoff volume for the same storm. Should sufficient long term storage not be provided that can prevent all or some of this volume (Vol_{xs}) from entering the receiving waters, then the throttle should be reduced to Qbar or 2l/s for all events and the runoff should be attenuated accordingly. (see GDSDS CI6.3.4 Sub-</p>								
COMMENTS								

APPENDIX II

RELEVANT EXTRACT FROM SITE INVESTIGATION



GroundCheck

WAREHOUSING / LOGISTICS & OFFICES,
CALMOUNT ROAD,
BALLYMOUNT,
DUBLIN

GROUND INVESTIGATION REPORT

CLIENT: Park Developments

JOB REF: 23-3170

ISSUED: February 2023



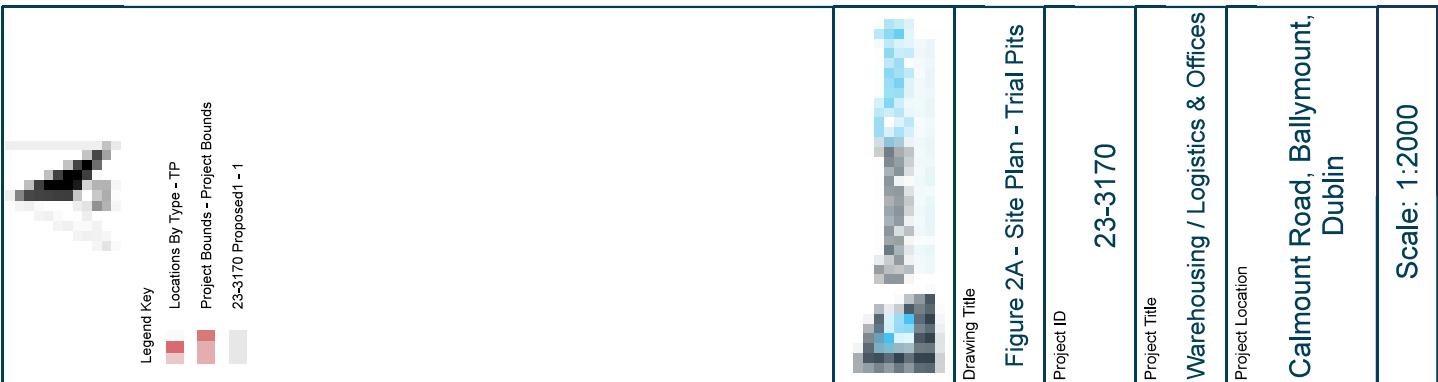
4.3 Soakaway Test Results

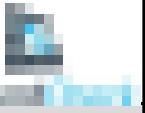
The trial pits observed that the site is mantled by a superficial layer of made ground and glacial deposits composed of a stoney silt, overlying fractured limestone bedrock that was encountered at depths ranging between 0.3 and 1.2m. The variation in the soil properties, rockhead levels and the fractured state of the upper horizons of the bedrock is reflected by the results of the soakaway tests that are presented in Table 4. The percolation values ranged between 1.4 and 212sec/mm (infiltration rate 2.6E-4 to 1.8E-6), with the highest infiltration rates being recorded where fractured rock was encountered in the base of the trial pit.

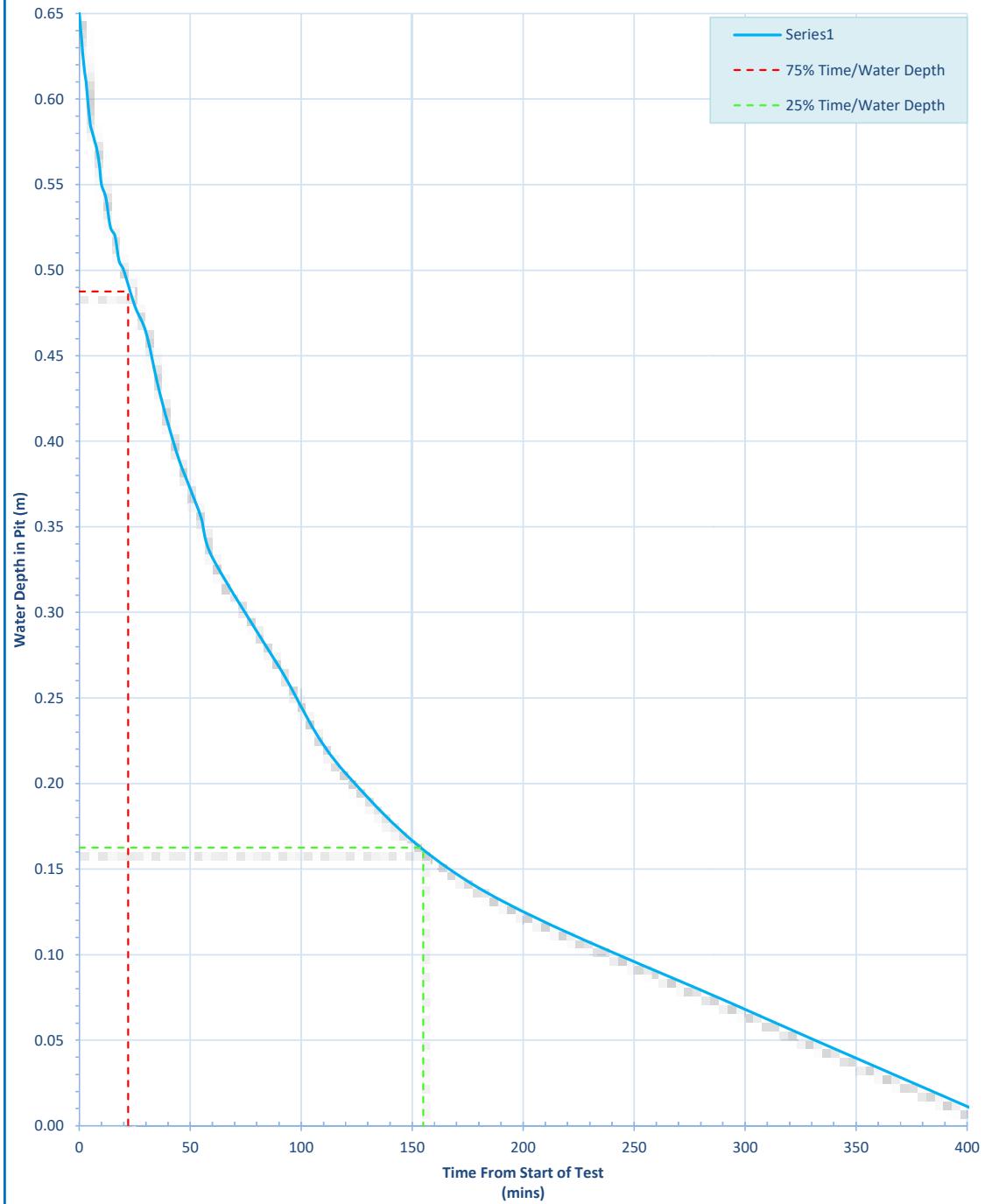
Table 4: Summary of Percolation Test Results

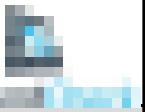
Test No.	Location	Sump Depth (m)	Elapsed Time (mins)		Time Difference between 75 and 25% infiltration (Seconds)	Average Percolation Value* V_p (sec/mm)
			For 75% Infiltration	For 25% infiltration		
PT01	TP01	1.0	22 36	155 136	133 100	47
PT02	TP02	0.8	5 14	19 47	14 33	9
PT03	TP03	0.9	8 12	31 45	23 33	11
PT04	TP04	0.7	11 19 23	40 61 78	29 42 55	16
PT05	TP05	0.8	21 33 35	68 102 109	47 69 74	25
PT06	TP06	0.8	42 97 101	305 201 174	263 104 73	59
PT07	TP07	0.95	6 8 9	19 23 26	13 16 17	6
PT08	TP08	0.8	27 46 75	96 229 865	69 183 790	138
PT09	TP09	0.7	13 27 30	47 98 133	35 71 103	28
PT10	TP10	0.7	10 24 28	37 98 101	27 74 74	23
PT11	TP11	0.8	2 2 2	7 8 8	5 7 7	2.5
PT12	TP12	0.9	6 7 7	18 30 42	12 22 35	9
PT13	TP13	0.8	140	670	530	212
PT14	TP14	1.2	10 19	31 34	21 15	7
PT15	TP15	0.8	2 3	6 5	4 3	1.4
PT16	TP16	1.05	200	1060	860	344
PT17	TP17	0.9	2 7	9 19	6 12	3.6
PT18	TP18	0.9	230	660	430	172
PT19	TP19	0.6	42	260	218	87
PT20	TP20	1.0	145	580	435	174

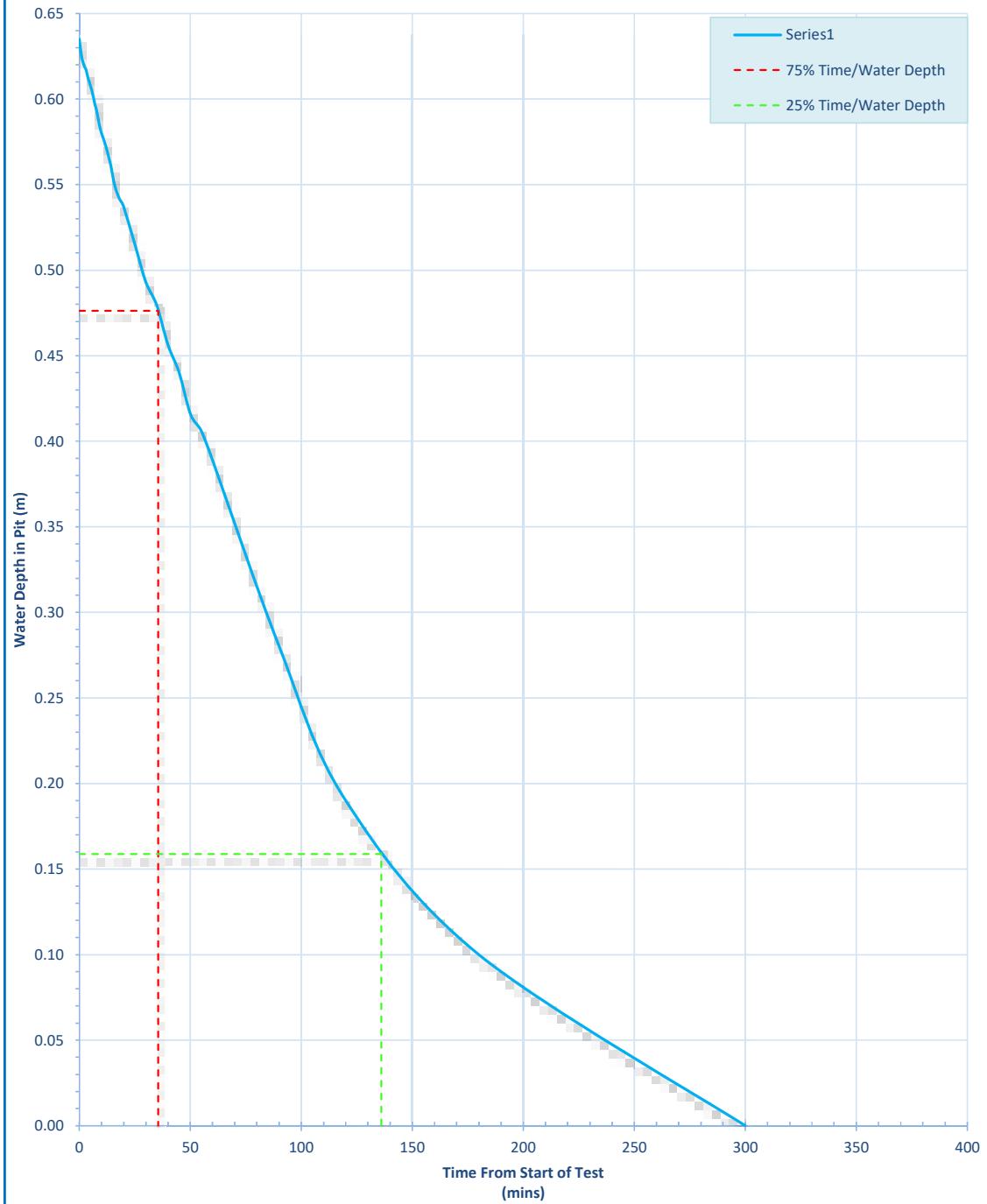
Note * Percolation test value calculated by dividing seconds time difference between 75 and 25% infiltration by 150mm



BRE 365 SOIL INFILTRATION TEST				
JOB No.	23-3170	SITE	Calmount Drive, Dublin	
TEST PIT DEPTH (m)	1	SOIL TYPE	Light brown, silty sandy CLAY	TRIAL PIT No.
TP01				

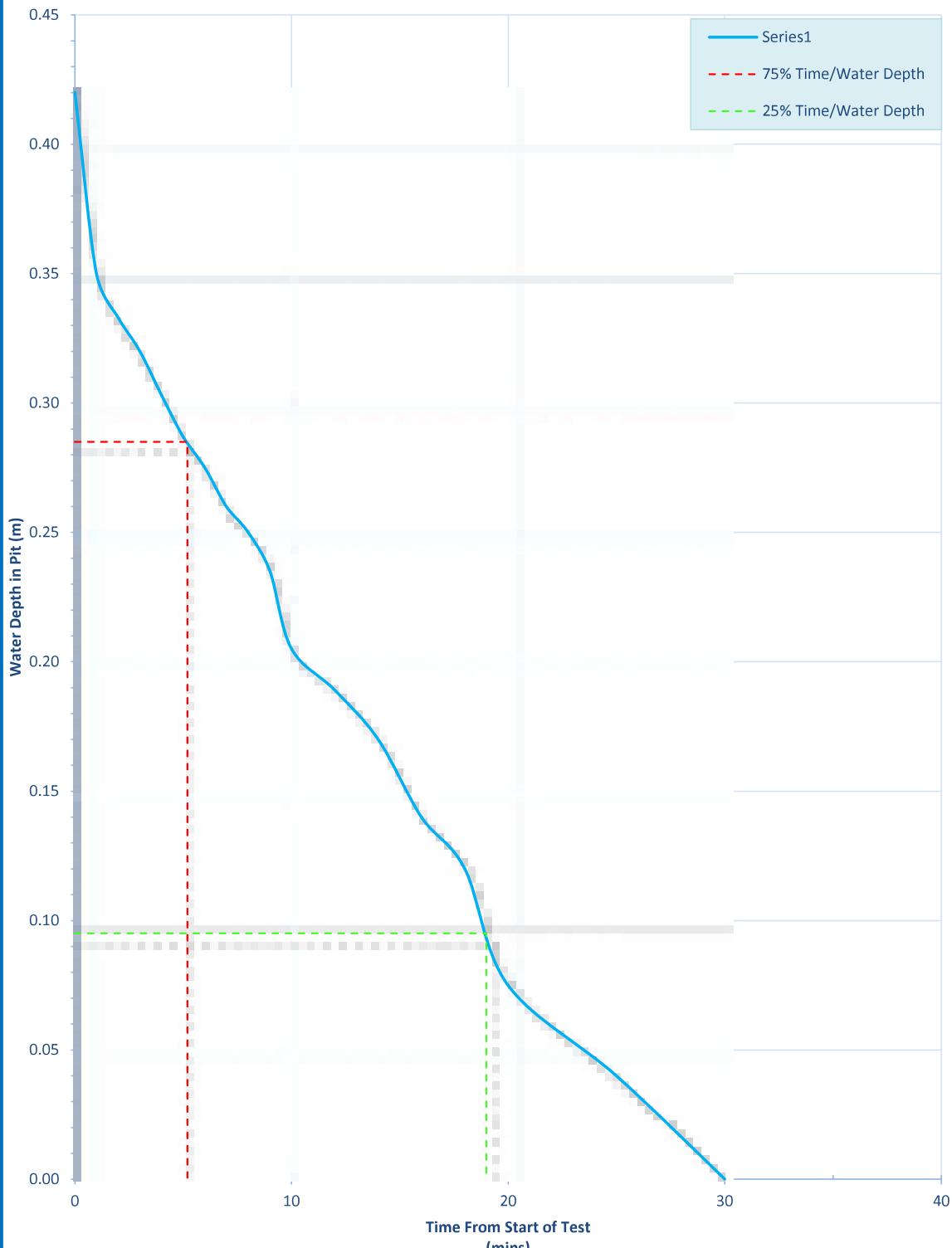


BRE 365 SOIL INFILTRATION TEST							
JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.	TP01		
INFILTRATION TEST No.	2	SOIL TYPE	Light brown, silty sandy CLAY	WEATHER CONDITIONS	DRY		
TEST PIT WIDTH (m)	0.50	TEST PIT LENGTH (m)	1.50	TEST PIT DEPTH (m)	1.00		
WATER SURFACE LEVEL (m)	0.37	GROUNDWATER DEPTH (m)	Dry	HEAD OF WATER IN PIT (m)	0.64		
BASE SURFACE AREA (m ²)	0.75	SIDEWALL SURFACE AREA (m ²)	4.00	a(p50) Internal Surface Area @ 50% Effective Depth (m ²)	2.75		
75% Effective Water Depth (m)	0.47625	25% Effective Water Depth (m)	0.15875	V(p75-25) Volume of Hole Between 75 & 25% Effective Water Depth (m ³)	0.238125		
t(p75) Time for Water Level to Drain to 75% Effective Depth (mins)	35.5	t(p25) Time for Water Level to Drain to 25% Effective Depth (mins)	136	t(p75-25) Time for Water Level to Drain from 75 to 25% Effective Depth (mins)	100.5		
SOIL INFILTRATION RATE	1.44E-05			m/sec			
24 Hr Clock Time hh:mm	Time Elapsed (mins)	Depth of Water in Pit (m)					
09:00	0	0.635					
09:01	1	0.625					
09:02	2	0.620					
09:03	3	0.617					
09:04	4	0.612					
09:05	5	0.608					
09:06	6	0.603					
09:07	7	0.597					
09:08	8	0.592					
09:09	9	0.585					
09:10	10	0.580					
09:15	12	0.572					
09:30	14	0.562					
09:45	16	0.549					
10:00	18	0.542					
10:15	20	0.537					
10:30	25	0.515					
10:45	30	0.493					
	35	0.479					
	40	0.456					
	45	0.440					
	50	0.416					
	55	0.406					
	60	0.389					
	90	0.280					
	120	0.190					
	180	0.100					
	300	0.000					
	420						
							
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JOB No.	23-3170	SITE	Calmount Drive, Dublin				
TEST PIT DEPTH (m)	1.00	SOIL TYPE	Light brown, silty sandy CLAY	TRIAL PIT No.			
TP01							



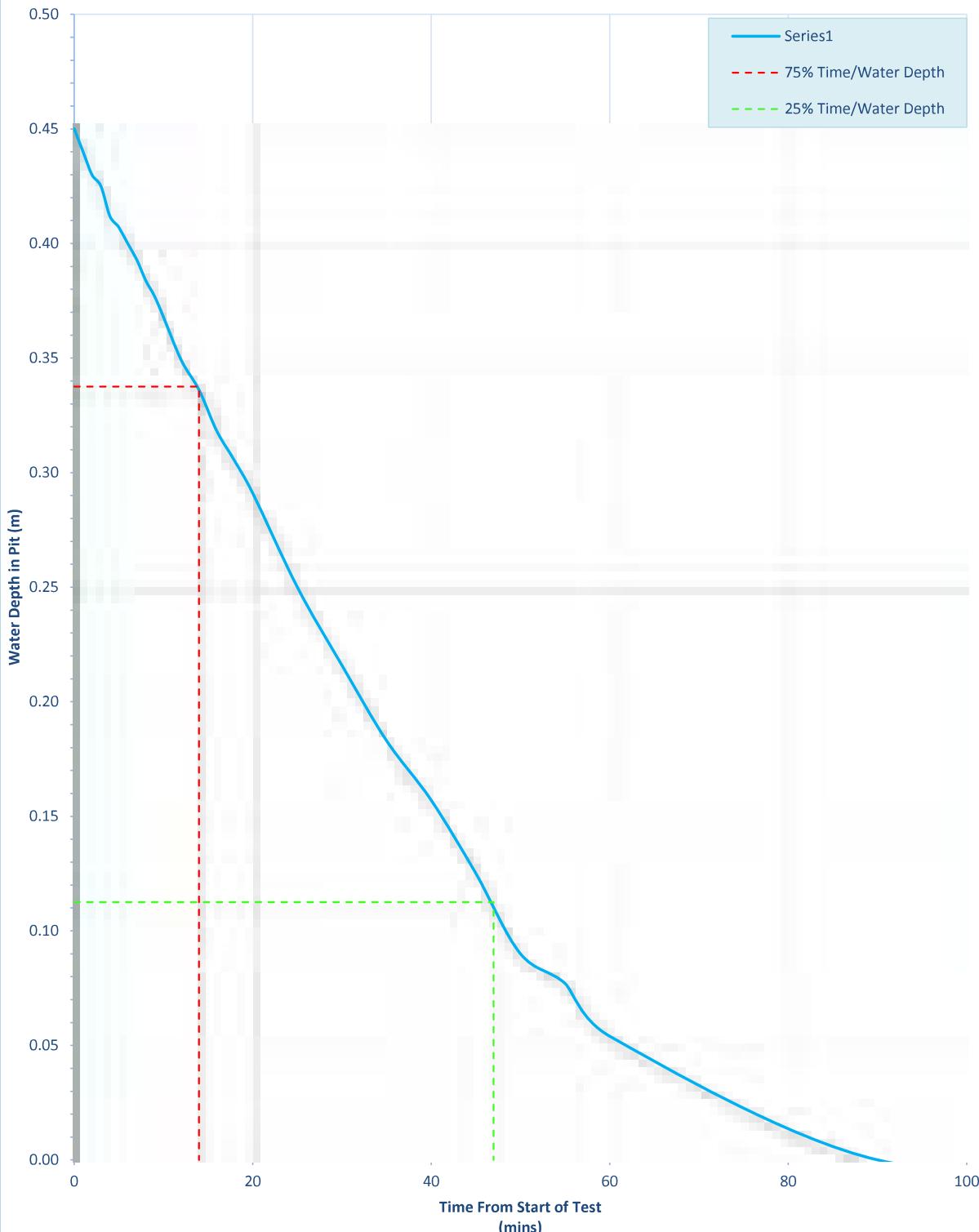
BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	1	SOIL TYPE	Grey, sandy, organic, clayey SILT	TP02



BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.80	SOIL TYPE	Light brown silty, sandy, gravelly CLAY	TP02

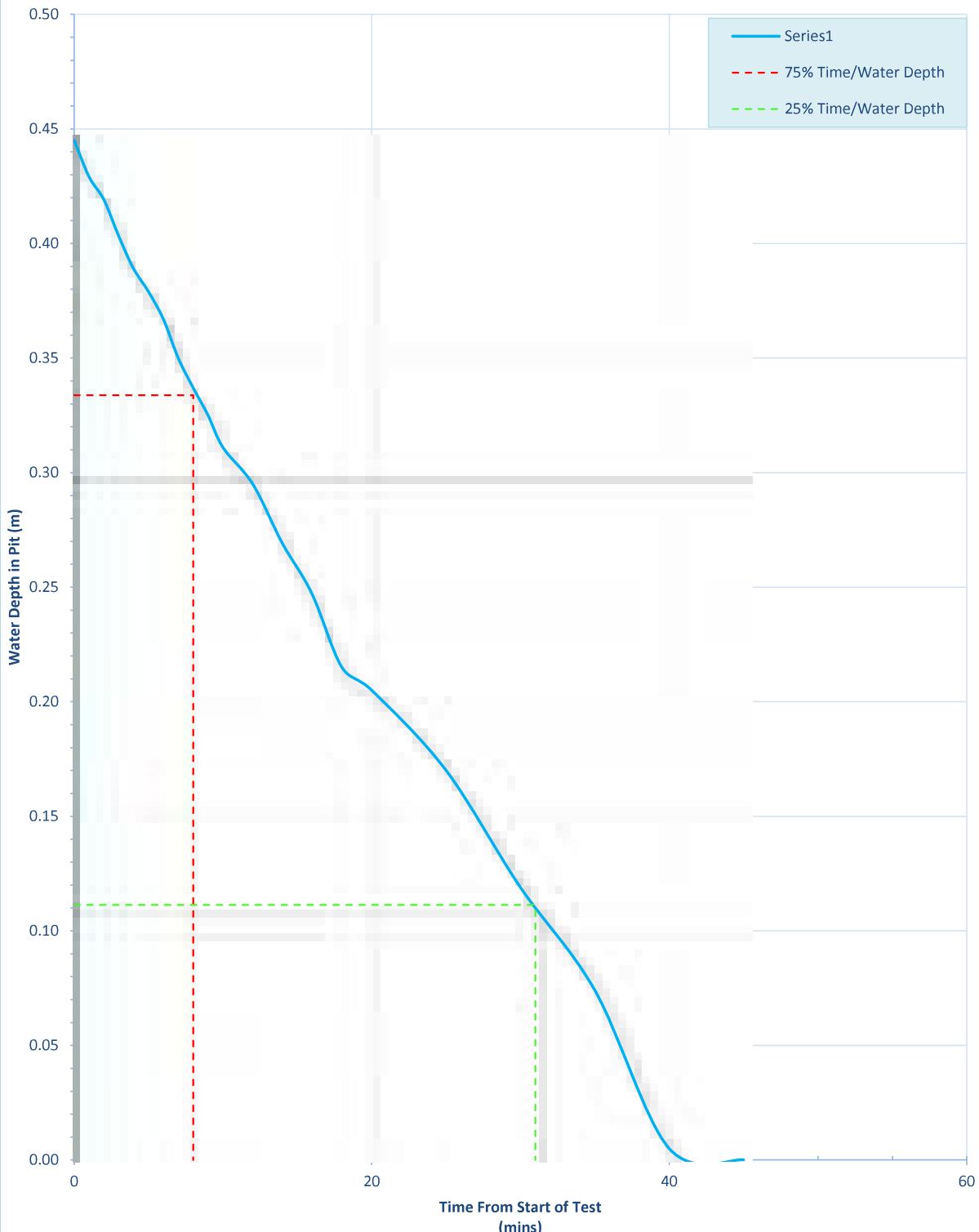


BRE 365 SOIL INFILTRATION TEST



BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.90	SOIL TYPE	Grey silty, sandy, gravelly CLAY	TP03

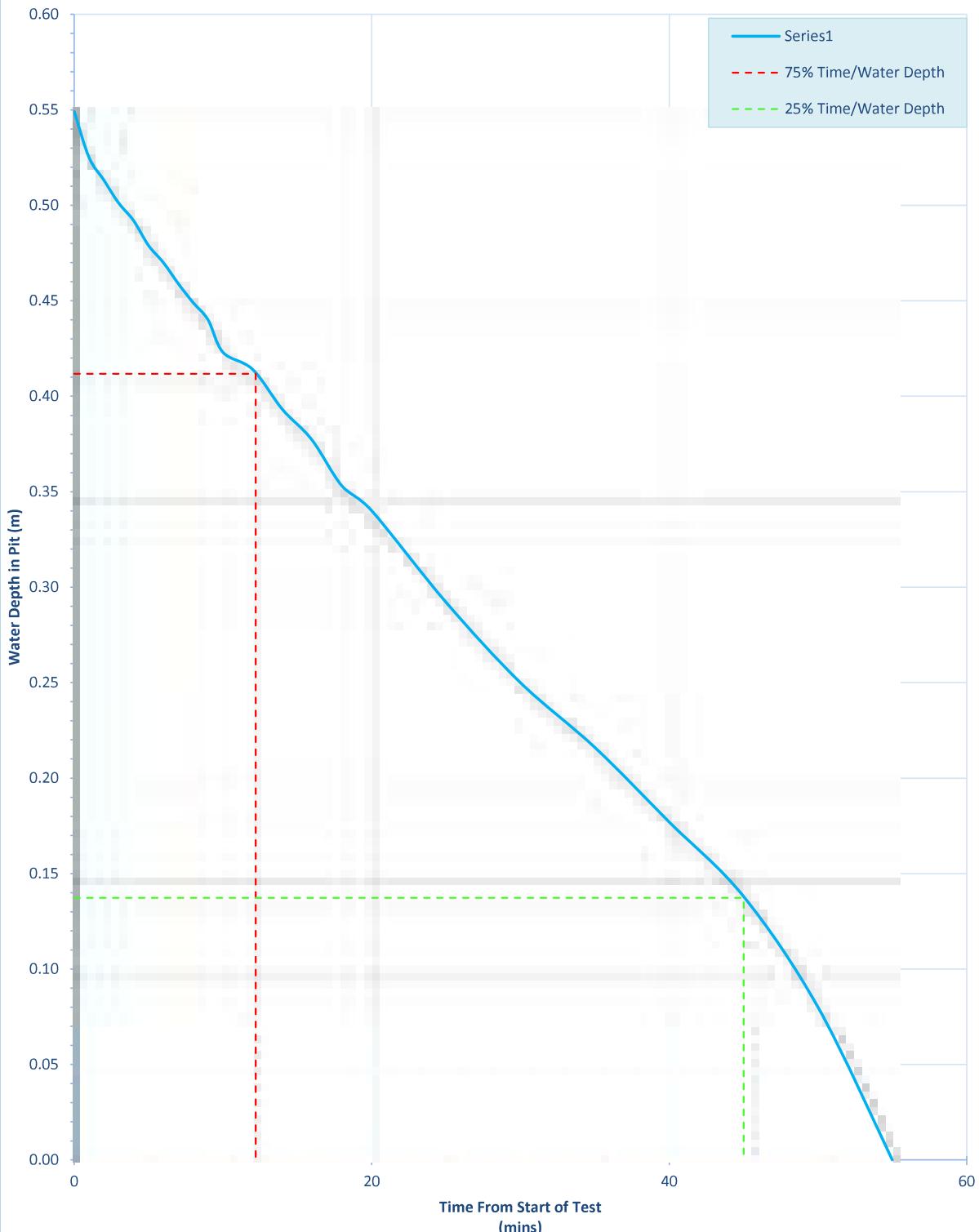


BRE 365 SOIL INFILTRATION TEST



BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.90	SOIL TYPE	Grey silty, sandy, gravelly CLAY	TP03

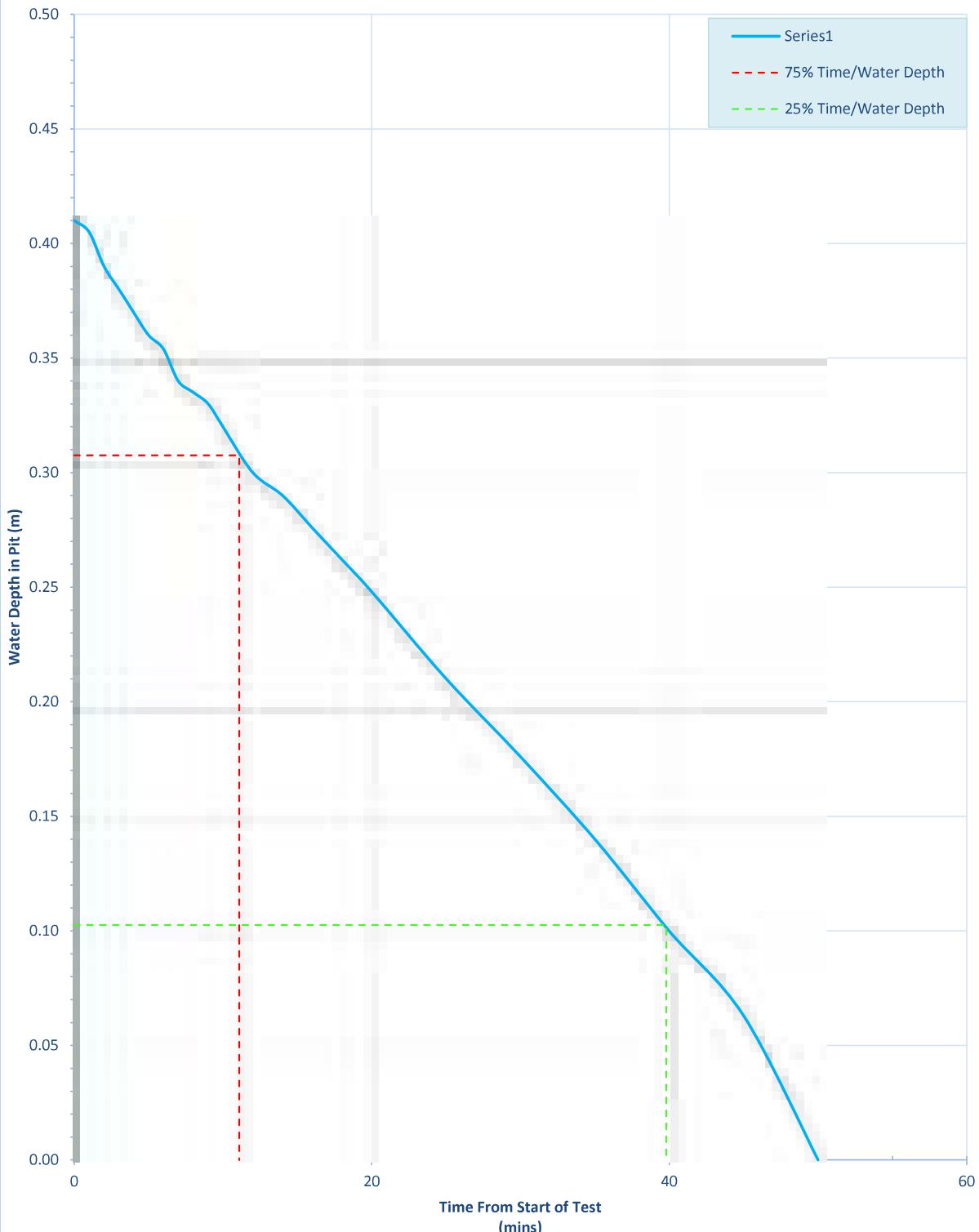


BRE 365 SOIL INFILTRATION TEST



BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.70	SOIL TYPE	Grey silty, sandy, gravelly CLAY	TP04

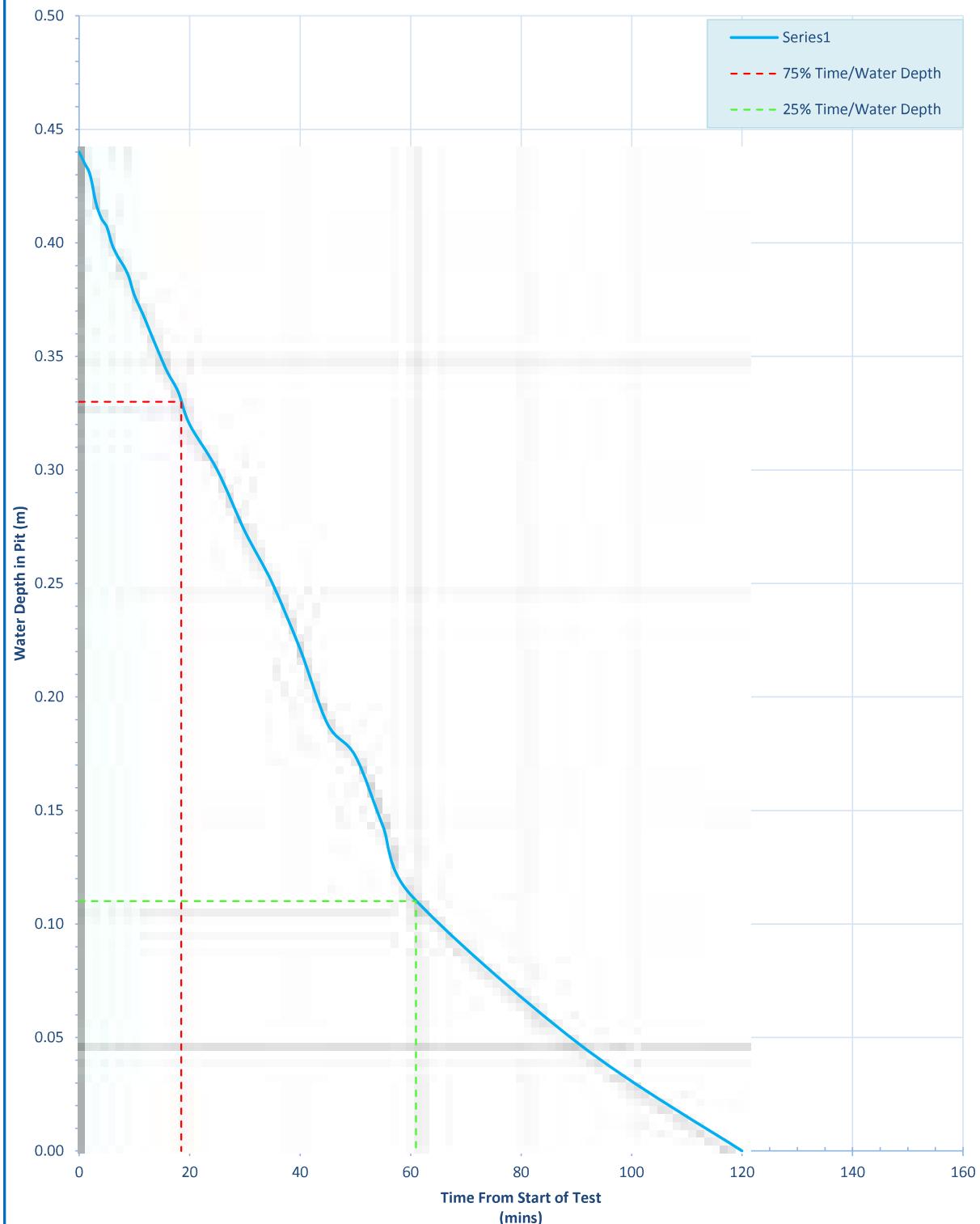


BRE 365 SOIL INFILTRATION TEST



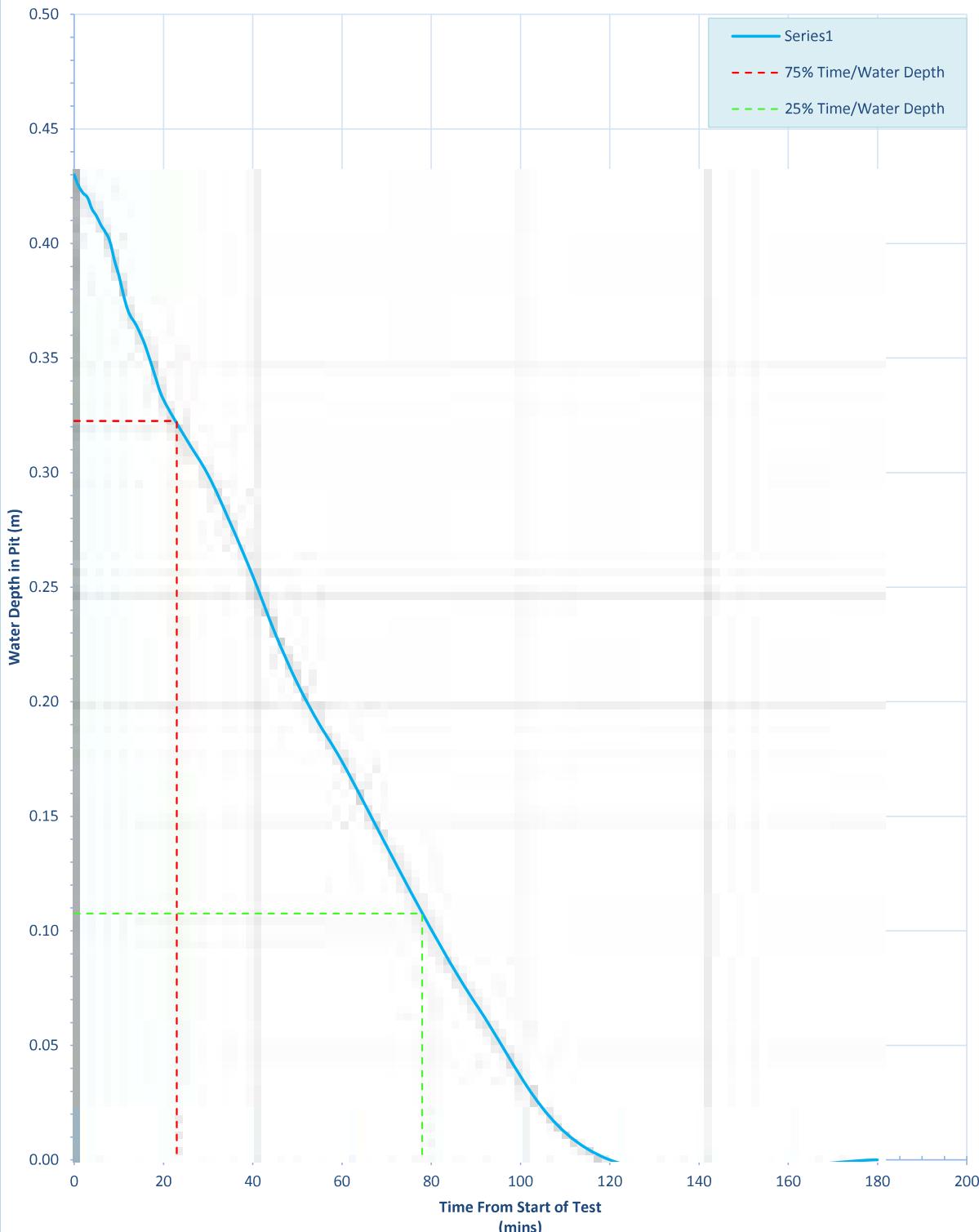
BRE 365 SOIL INFILTRATION TEST

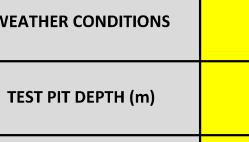
JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.70	SOIL TYPE	Grey silty, sandy, gravelly CLAY	TP04



BRE 365 SOIL INFILTRATION TEST

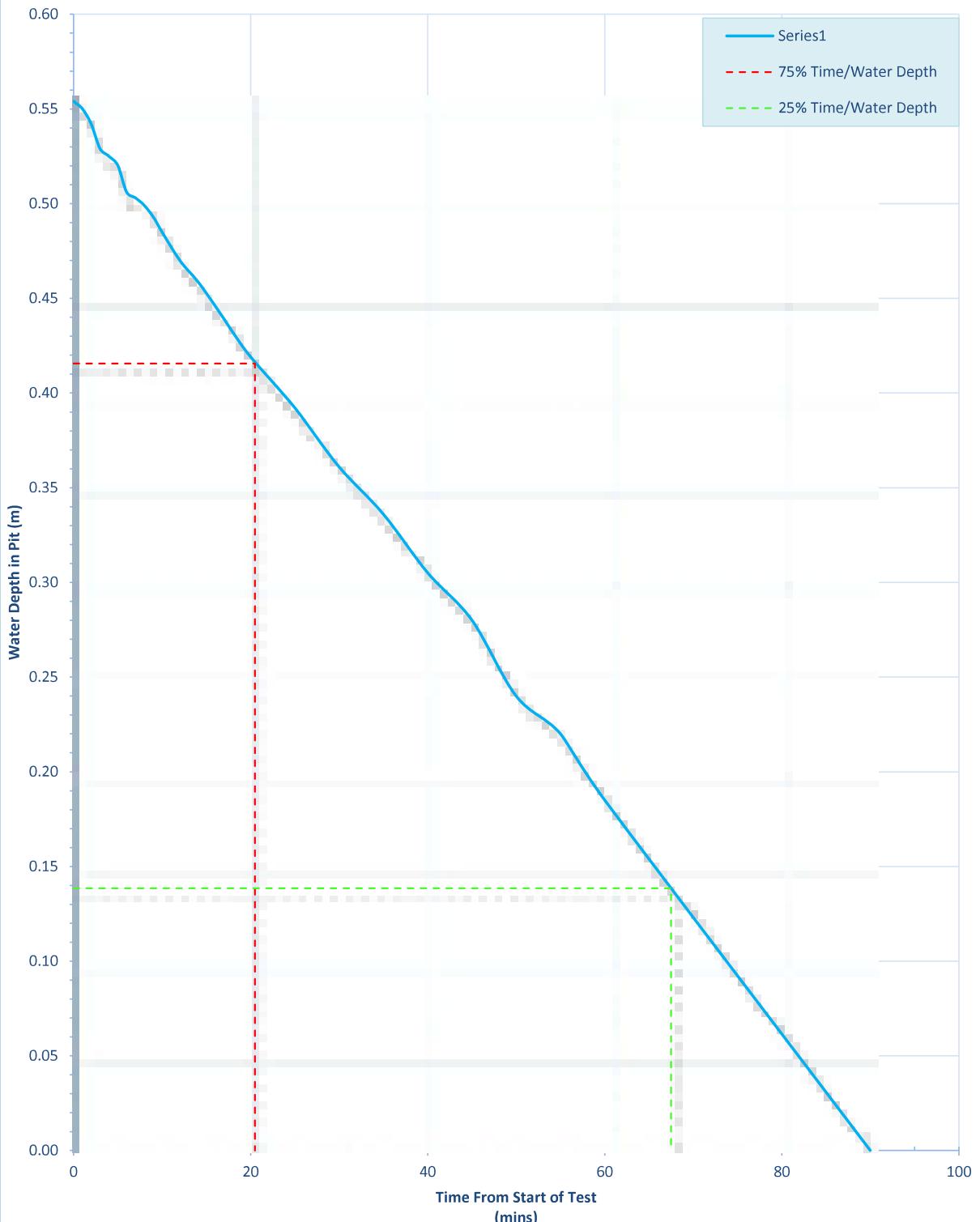
JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.70	SOIL TYPE	Grey silty, sandy, gravelly CLAY	TP04



BRE 365 SOIL INFILTRATION TEST					
JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.	TP05
INFILTRATION TEST No.	1	SOIL TYPE	Light brown silty, sandy, gravelly CLAY	WEATHER CONDITIONS	DRY
TEST PIT WIDTH (m)	0.50	TEST PIT LENGTH (m)	1.30	TEST PIT DEPTH (m)	0.80
WATER SURFACE LEVEL (m)	0.25	GROUNDWATER DEPTH (m)	Dry	HEAD OF WATER IN PIT (m)	0.55
BASE SURFACE AREA (m ²)	0.65	SIDEWALL SURFACE AREA (m ²)	2.88	a(p50) Internal Surface Area @ 50% Effective Depth (m ²)	2.09
75% Effective Water Depth (m)	0.4155	25% Effective Water Depth (m)	0.1385	V(p75-25) Volume of Hole Between 75 & 25% Effective Water Depth (m ³)	0.18005
t(p75) Time for Water Level to Drain to 75% Effective Depth (mins)	20.5	t(p25) Time for Water Level to Drain to 25% Effective Depth (mins)	67.5	t(p75-25) Time for Water Level to Drain from 75to 25% Effective Depth (mins)	47
SOIL INFILTRATION RATE		3.05E-05			m/sec
24 Hr Clock Time hh:mm	Time Elapsed (mins)	Depth of Water in Pit (m)			
09:00	0	0.554			
09:01	1	0.550			
09:02	2	0.542			
09:03	3	0.529			
09:04	4	0.525			
09:05	5	0.520			
09:06	6	0.506			
09:07	7	0.503			
09:08	8	0.499			
09:09	9	0.493			
09:10	10	0.485			
09:15	12	0.470			
09:30	14	0.459			
09:45	16	0.446			
10:00	18	0.432			
10:15	20	0.419			
10:30	25	0.392			
10:45	30	0.361			
11:00	35	0.336			
11:30	40	0.305			
12:00	45	0.280			
12:30	50	0.240			
13:00	55	0.220			
13:30	60	0.185			
14:00	90	0.000			
					

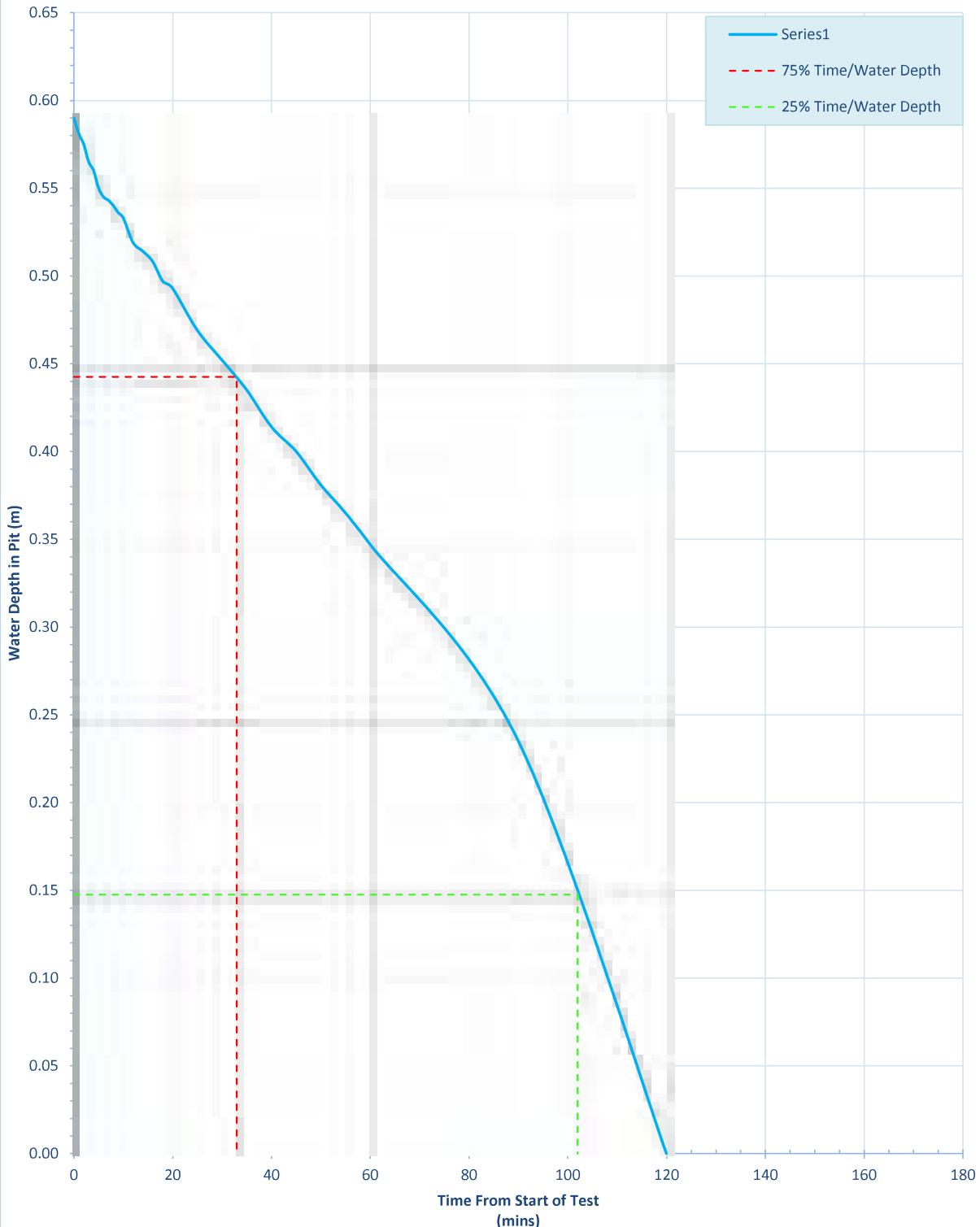
BRE 365 SOIL INFILTRATION TEST

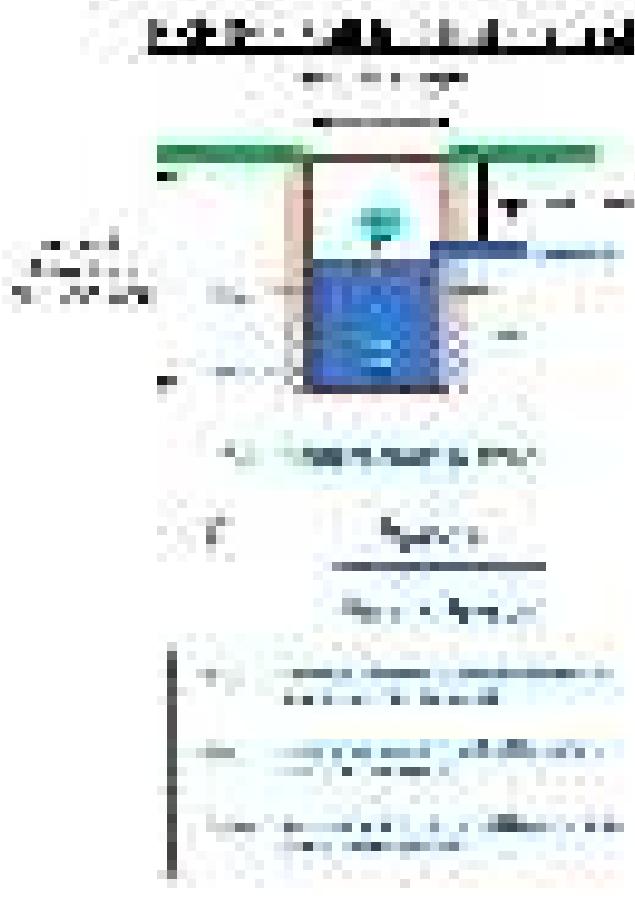
JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.80	SOIL TYPE	Light brown silty, sandy, gravelly CLAY	TP05

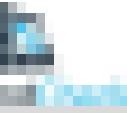


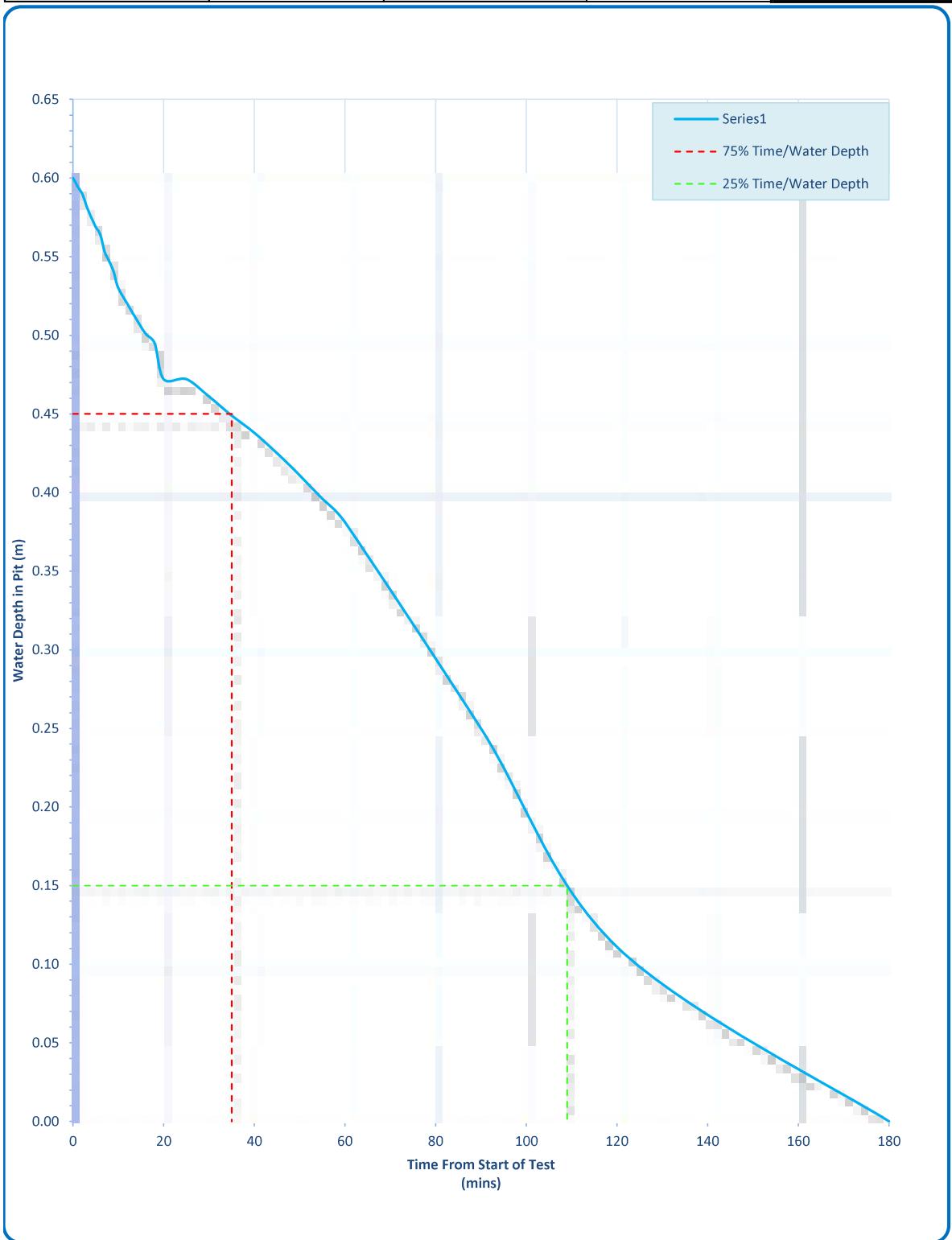
BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.80	SOIL TYPE	Light brown silty, sandy, gravelly CLAY	TP05



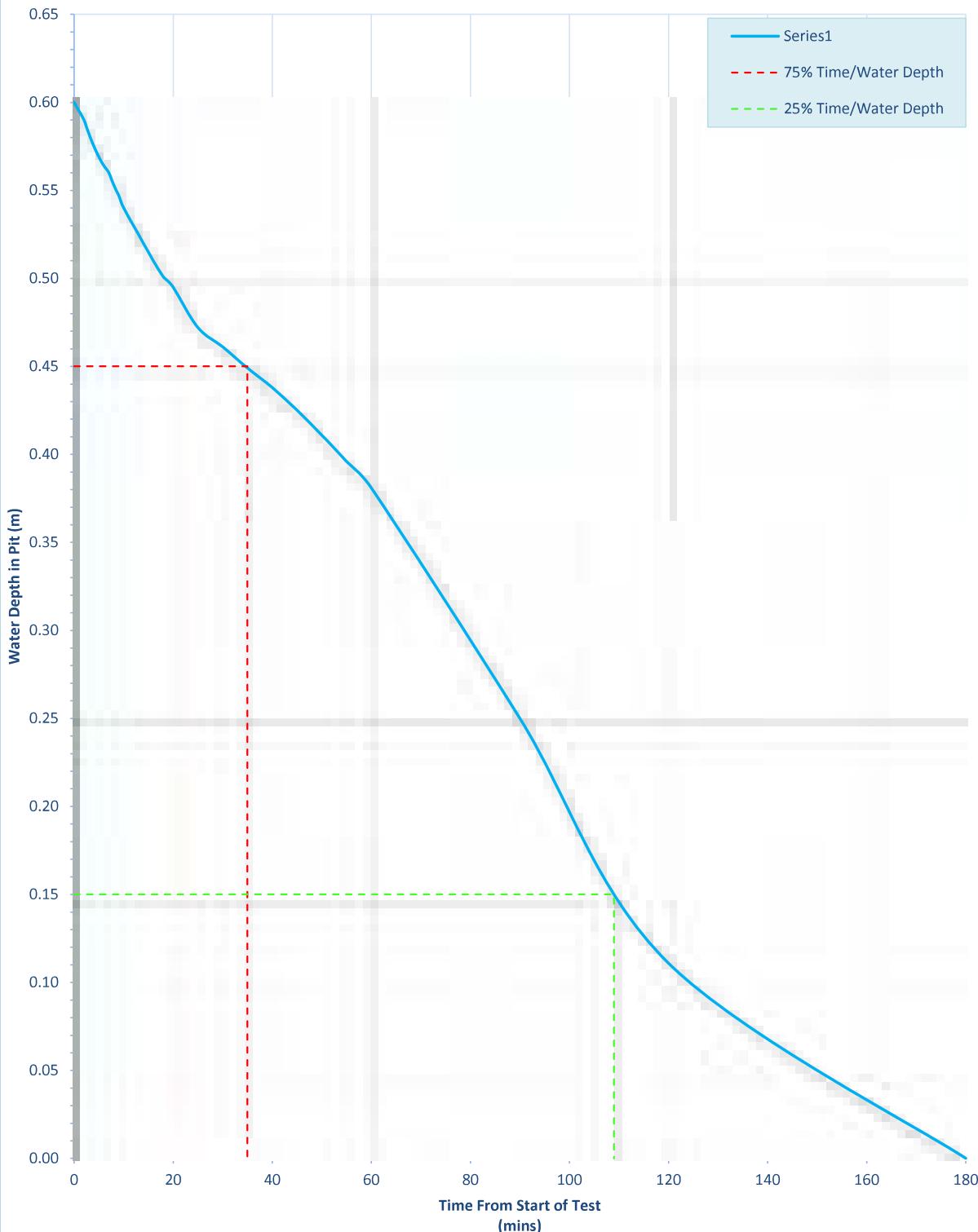
BRE 365 SOIL INFILTRATION TEST				TRIAL PIT No.	TP05
JOB No.	23-3170	SITE	Calmount Drive, Dublin		
INFILTRATION TEST No.	3	SOIL TYPE	Light brown silty, sandy, gravelly CLAY	WEATHER CONDITIONS	DRY
TEST PIT WIDTH (m)	0.50	TEST PIT LENGTH (m)	1.30	TEST PIT DEPTH (m)	0.80
WATER SURFACE LEVEL (m)	0.20	GROUNDWATER DEPTH (m)	Dry	HEAD OF WATER IN PIT (m)	0.60
BASE SURFACE AREA (m ²)	0.65	SIDEWALL SURFACE AREA (m ²)	2.88	a(p50) Internal Surface Area @ 50% Effective Depth (m ²)	2.09
75% Effective Water Depth (m)	0.45	25% Effective Water Depth (m)	0.15	V(p75-25) Volume of Hole Between 75 & 25% Effective Water Depth (m ³)	0.195
t(p75) Time for Water Level to Drain to 75% Effective Depth (mins)	35	t(p25) Time for Water Level to Drain to 25% Effective Depth (mins)	109	t(p75-25) Time for Water Level to Drain from 75 to 25% Effective Depth (mins)	74
SOIL INFILTRATION RATE		2.10E-05			m/sec
24 Hr Clock Time hh:mm	Time Elapsed (mins)	Depth of Water in Pit (m)			
09:00	0	0.600			
09:01	1	0.595			
09:02	2	0.590			
09:03	3	0.582			
09:04	4	0.575			
09:05	5	0.569			
09:06	6	0.564			
09:07	7	0.553			
09:08	8	0.547			
09:09	9	0.540			
09:10	10	0.530			
09:15	12	0.520			
09:30	14	0.510			
09:45	16	0.501			
10:00	18	0.495			
10:15	20	0.472			
10:30	25	0.472			
10:45	30	0.461			
11:00	35	0.449			
11:30	40	0.438			
12:00	45	0.425			
12:30	50	0.411			
13:00	55	0.396			
13:30	60	0.381			
14:00	90	0.250			
14:30	120	0.111			
15:00	180	0.000			
15:30	240				
16:00	300				
16:30	360				
17:00	3600				
17:30	720				
18:00	780				
	1200				
	2400				
	3600				
	4800				
Interpolated	6000				
	7200				
	8400				
	12000				
	14750				

BRE 365 SOIL INFILTRATION TEST				
JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.80	SOIL TYPE	Light brown silty, sandy, gravelly CLAY	TP05



BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.80	SOIL TYPE	Light brown silty, sandy, gravelly CLAY	TP05

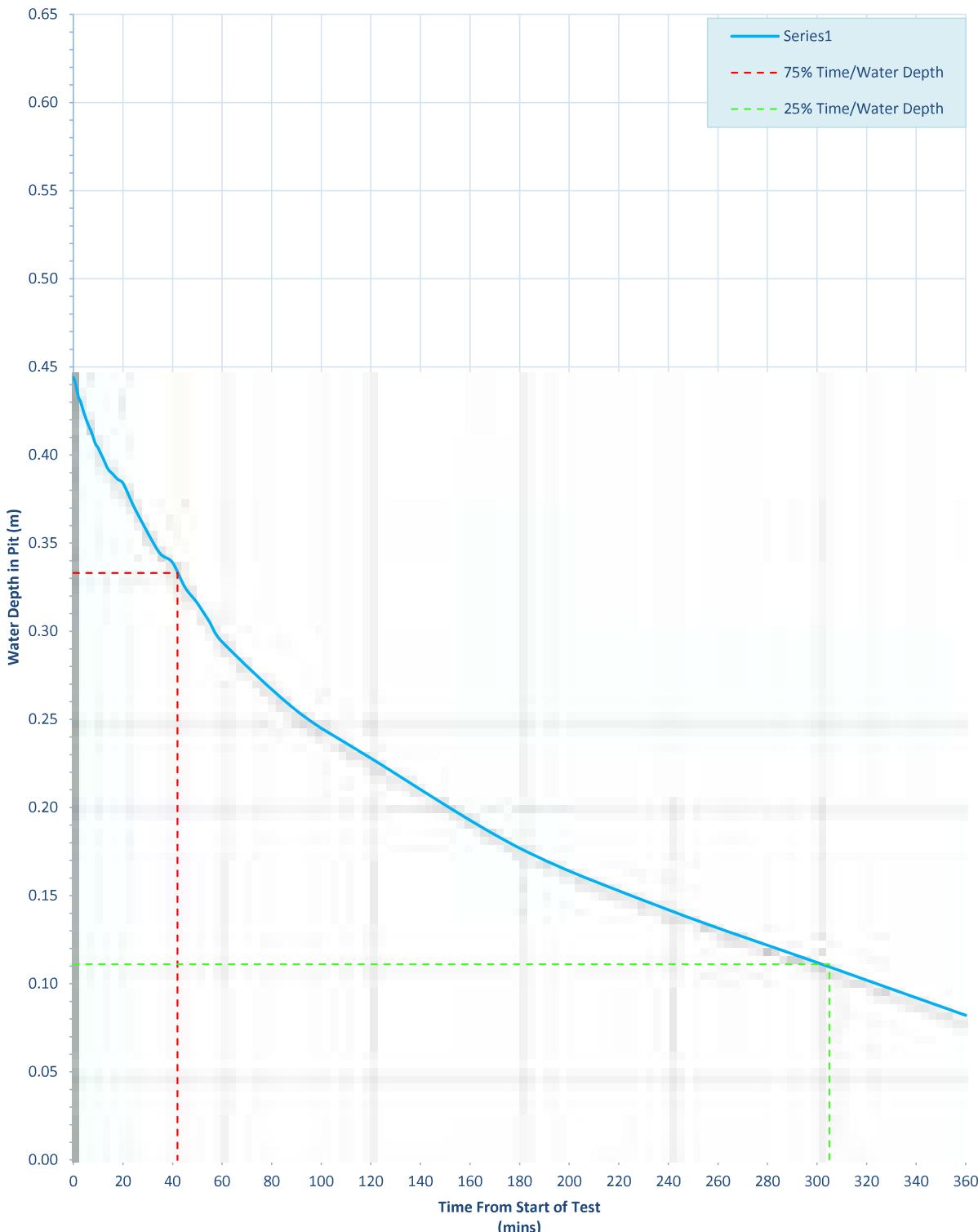


BRE 365 SOIL INFILTRATION TEST



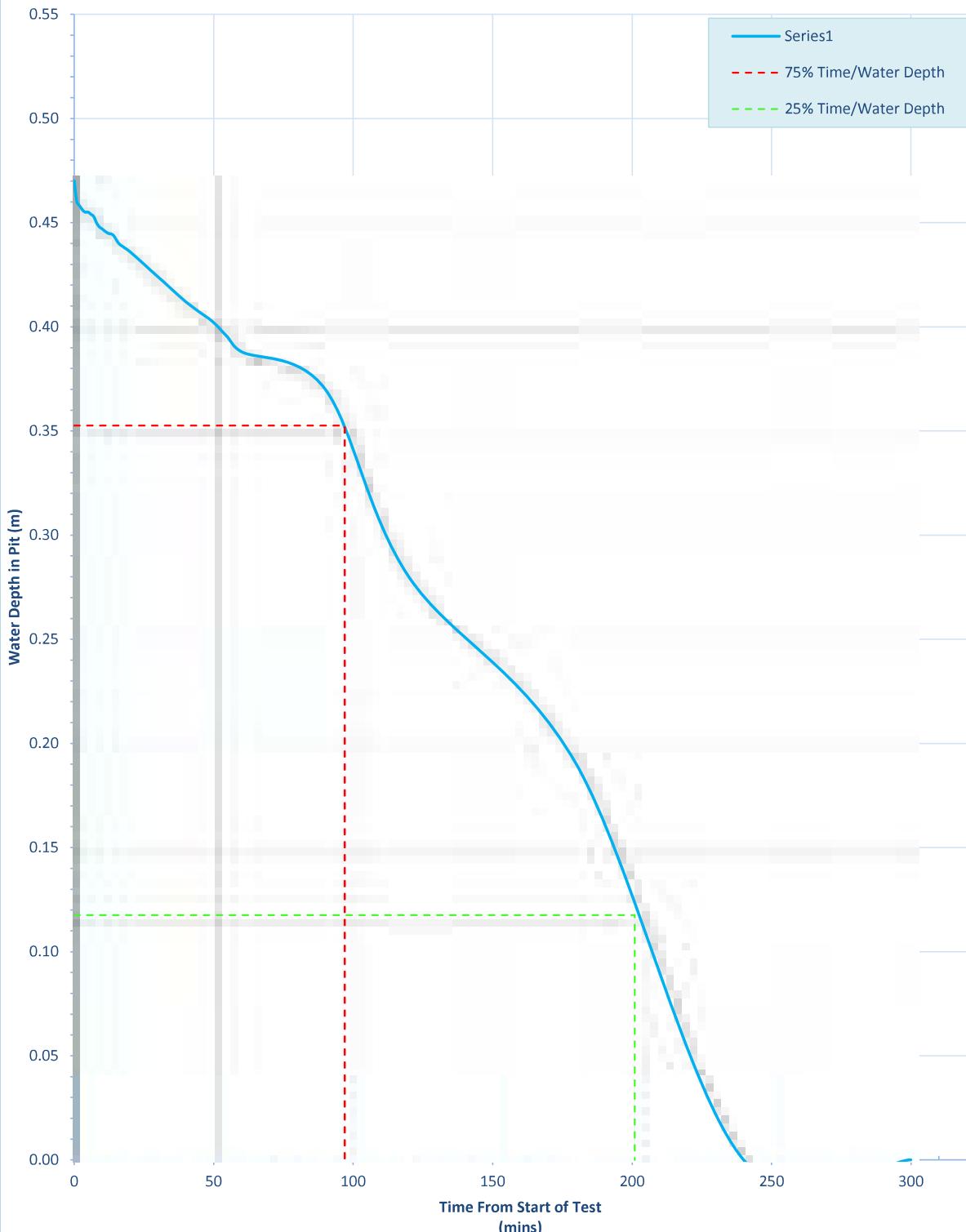
BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.80	SOIL TYPE	Light brown silty, sandy, gravelly CLAY	TP06



BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.80	SOIL TYPE	Light brown silty, sandy, gravelly CLAY	TP06

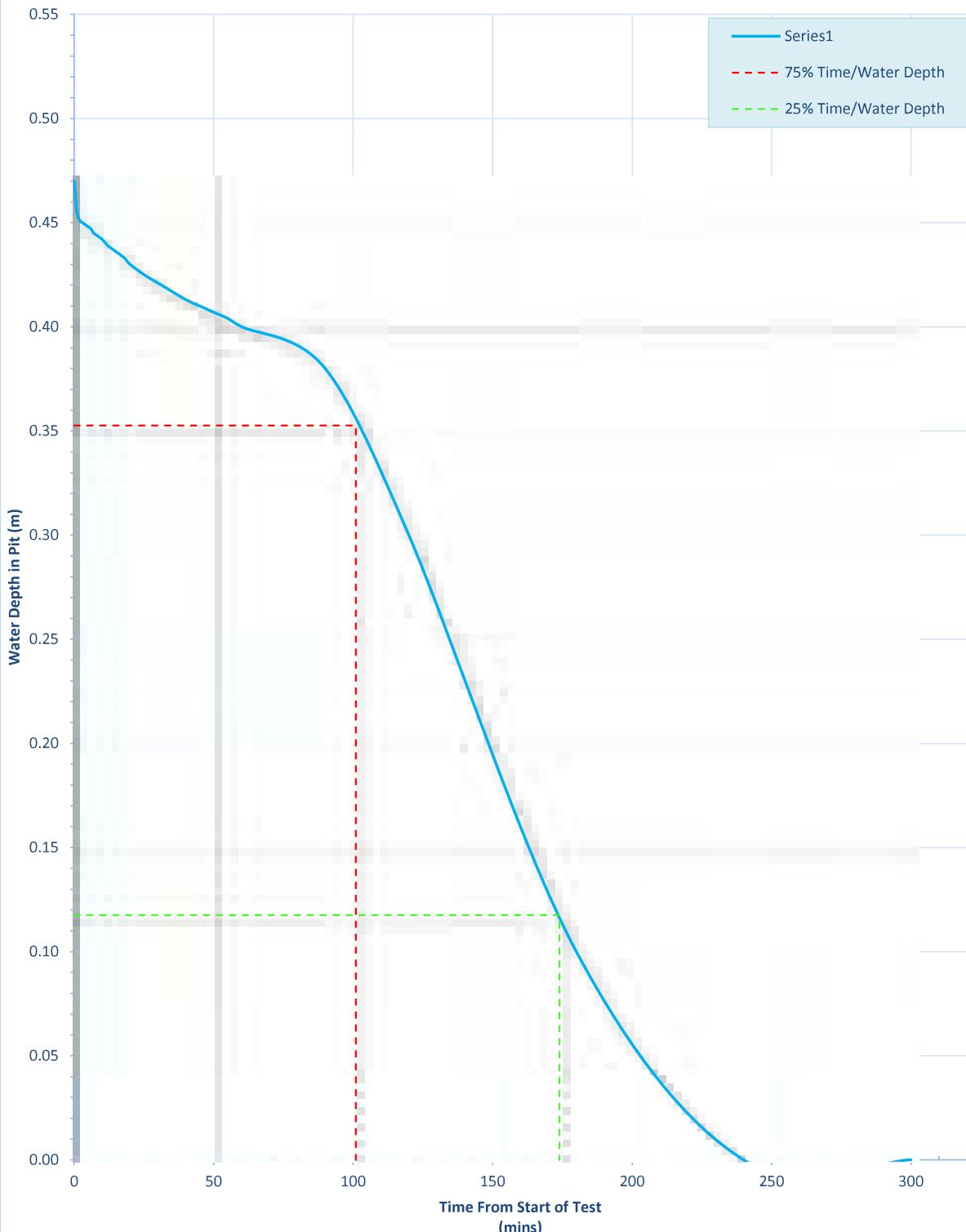


BRE 365 SOIL INFILTRATION TEST



BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.80	SOIL TYPE	Light brown silty, sandy, gravelly CLAY	TP06

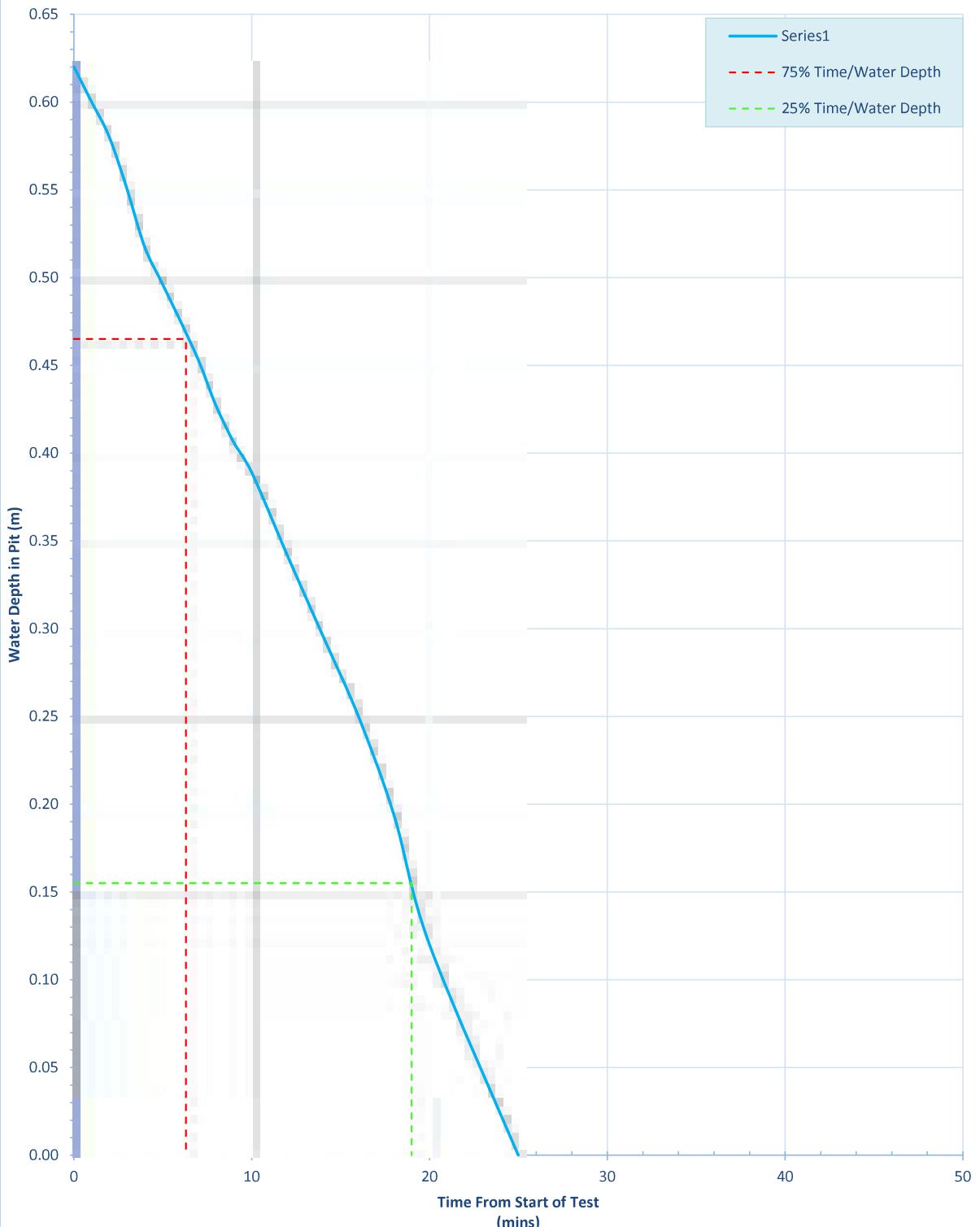


BRE 365 SOIL INFILTRATION TEST



BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.95	SOIL TYPE	Light brown silty, sandy, gravelly CLAY	TP07

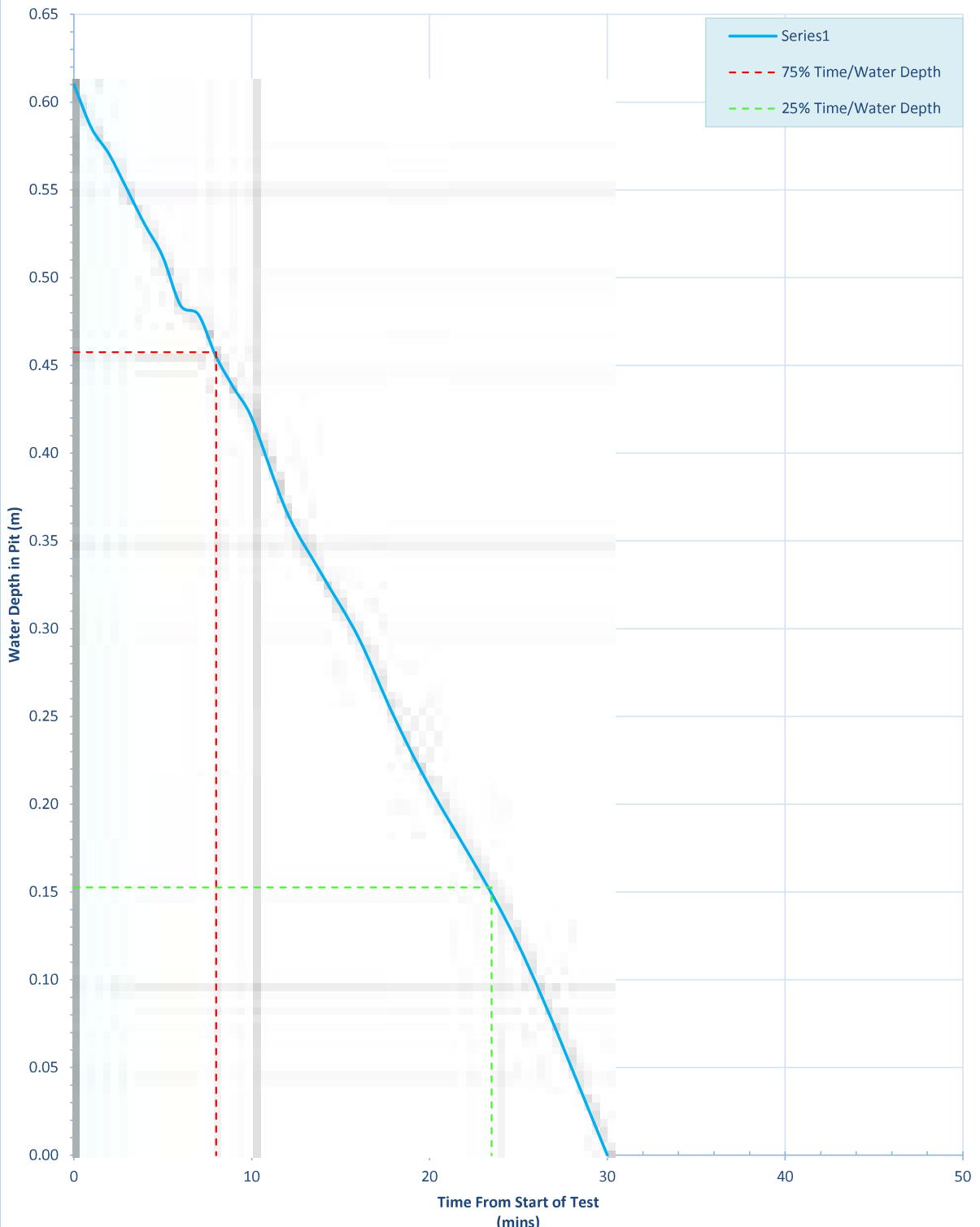


BRE 365 SOIL INFILTRATION TEST



BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.95	SOIL TYPE	Light brown silty, sandy, gravelly CLAY	TP07

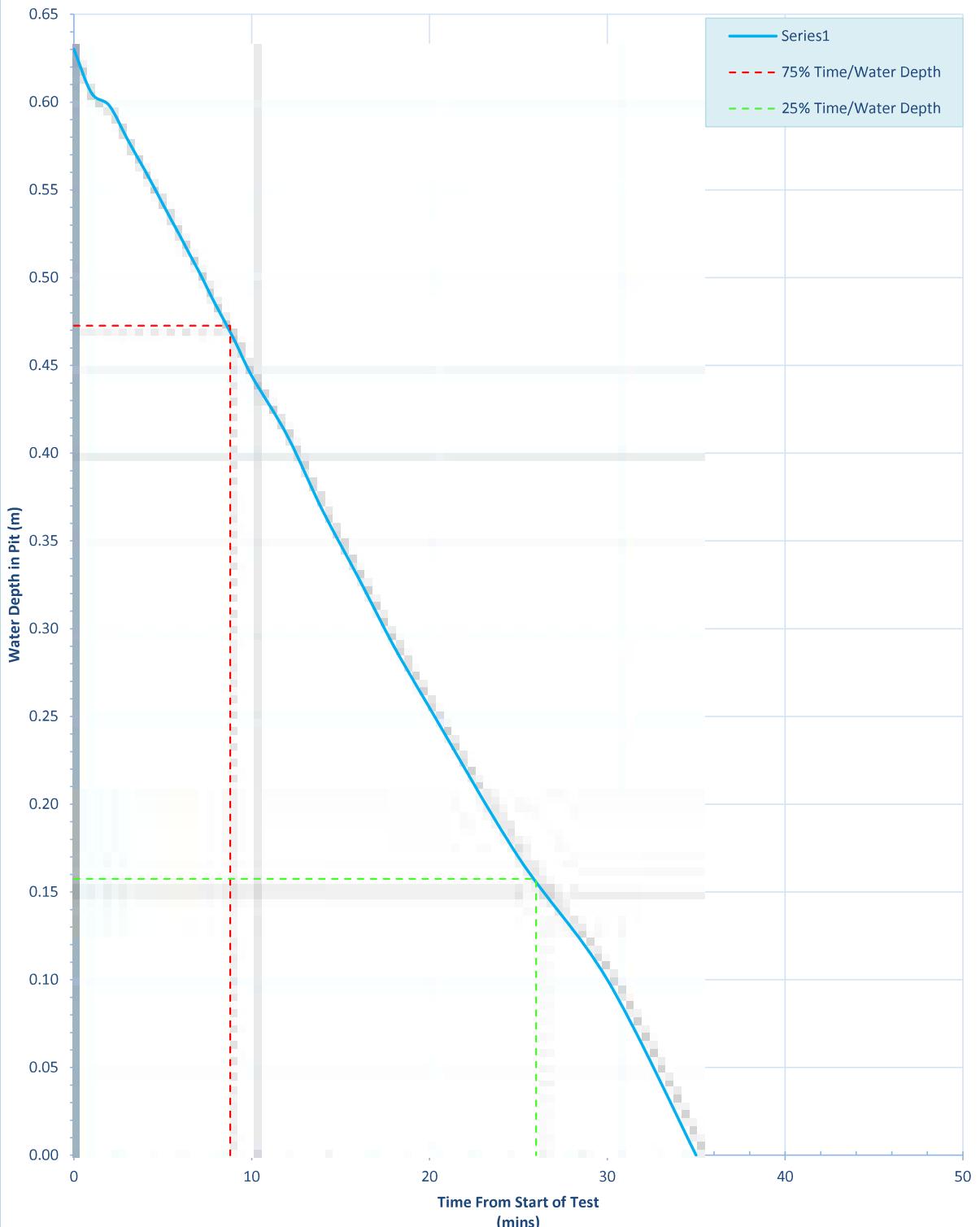


BRE 365 SOIL INFILTRATION TEST



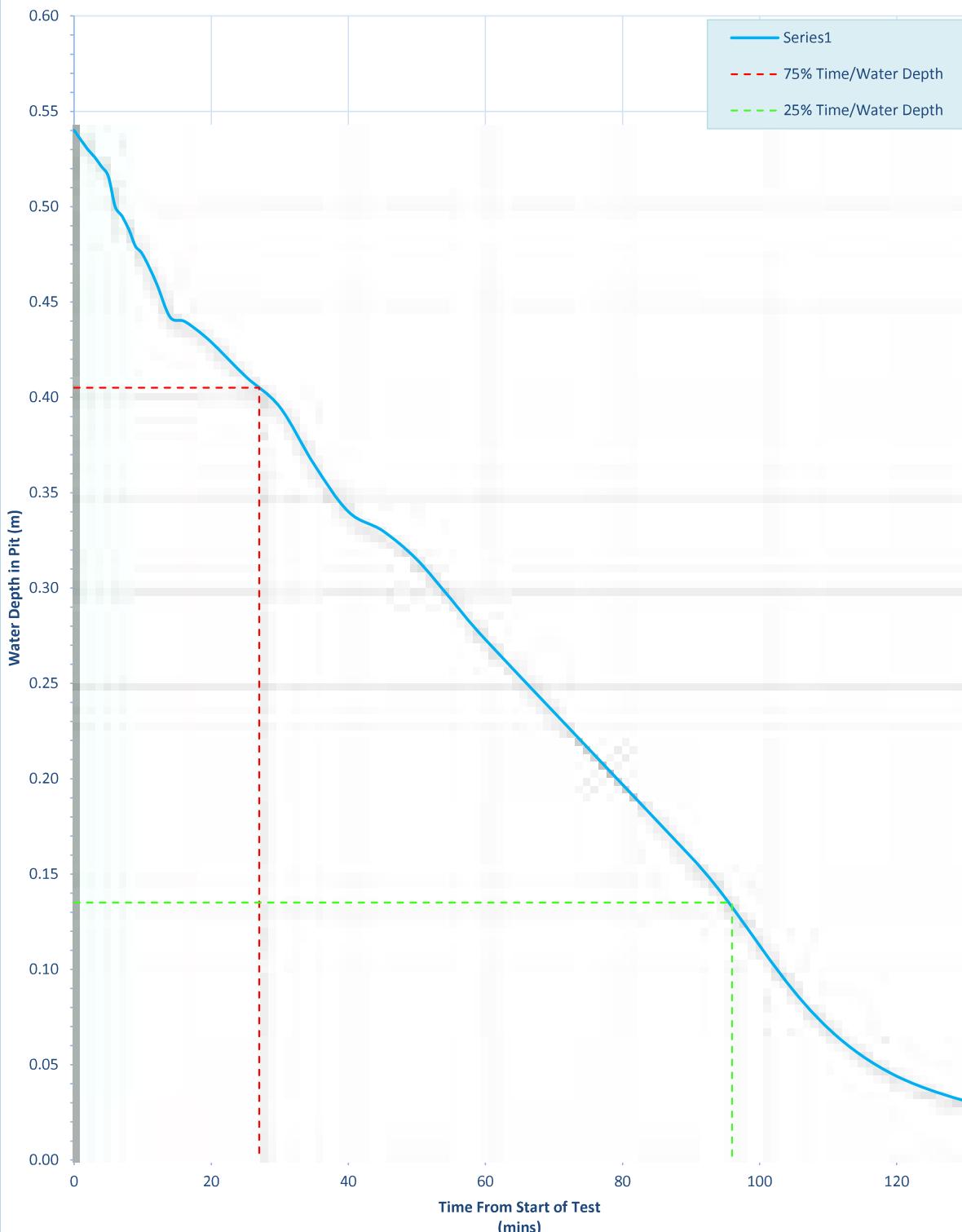
BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.95	SOIL TYPE	Light brown silty, sandy, gravelly CLAY	TP07



BRE 365 SOIL INFILTRATION TEST

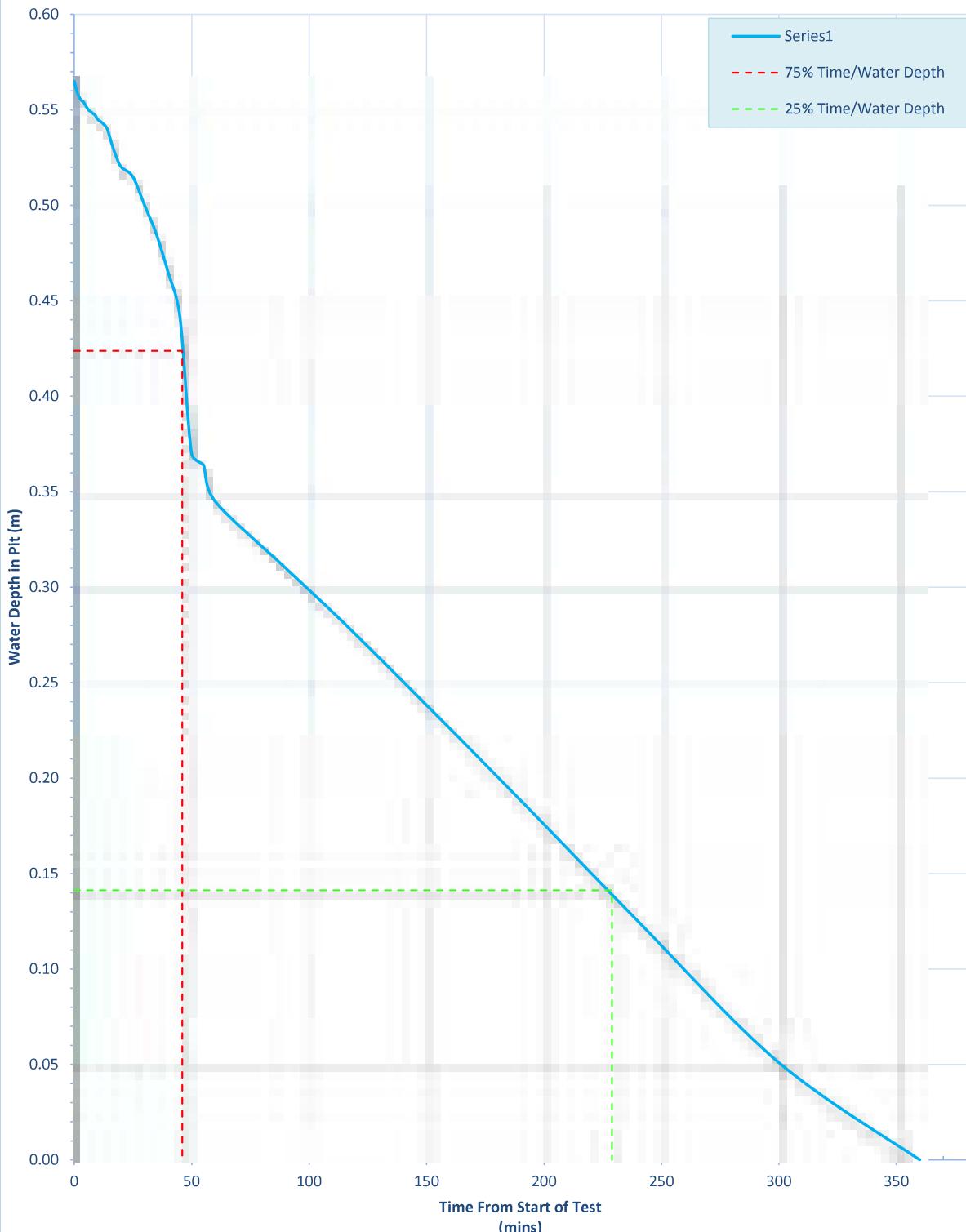
JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	1	SOIL TYPE	Grey, sandy, organic, clayey SILT	TP08



BRE 365 SOIL INFILTRATION TEST					
JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT NO.	TP08
INFILTRATION TEST NO.	2	SOIL TYPE	Grey, sandy, organic, clayey SILT	WEATHER CONDITIONS	DRY
TEST PIT WIDTH (m)	0.50	TEST PIT LENGTH (m)	1.40	TEST PIT DEPTH (m)	0.80
WATER SURFACE LEVEL (m)	0.24	GROUNDWATER DEPTH (m)	Dry	HEAD OF WATER IN PIT (m)	0.57
BASE SURFACE AREA (m ²)	0.70	SIDEWALL SURFACE AREA (m ²)	3.04	a(p50) Internal Surface Area @ 50% Effective Depth (m ²)	2.22
75% Effective Water Depth (m)	0.42375	25% Effective Water Depth (m)	0.14125	V(p75-25) Volume of Hole Between 75 & 25% Effective Water Depth (m ³)	0.19775
t(p75) Time for Water Level to Drain to 75% Effective Depth (mins)	46	t(p25) Time for Water Level to Drain to 25% Effective Depth (mins)	229	t(p75-25) Time for Water Level to Drain from 75 to 25% Effective Depth (mins)	183
SOIL INFILTRATION RATE		8.11E-06			m/sec
24 Hr Clock Time hh:mm	Time Elapsed (mins)	Depth of Water in Pit (m)			
09:00	0	0.565			
09:01	1	0.560			
09:02	2	0.557			
09:03	3	0.555			
09:04	4	0.554			
09:05	5	0.552			
09:06	6	0.550			
09:07	7	0.549			
09:08	8	0.548			
09:09	9	0.547			
09:10	10	0.545			
09:15	12	0.543			
09:30	14	0.540			
09:45	16	0.532			
10:00	18	0.525			
10:15	20	0.520			
10:30	25	0.515			
10:45	30	0.500			
11:00	35	0.485			
11:30	40	0.465			
12:00	45	0.442			
12:30	50	0.370			
13:00	55	0.364			
13:30	60	0.345			
14:00	90	0.310			
14:30	120	0.275			
15:00	180	0.201			
15:30	240	0.125			
16:00	300	0.051			
16:30	360	0.000			

BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	2	SOIL TYPE	Grey, sandy, organic, clayey SILT	TP08

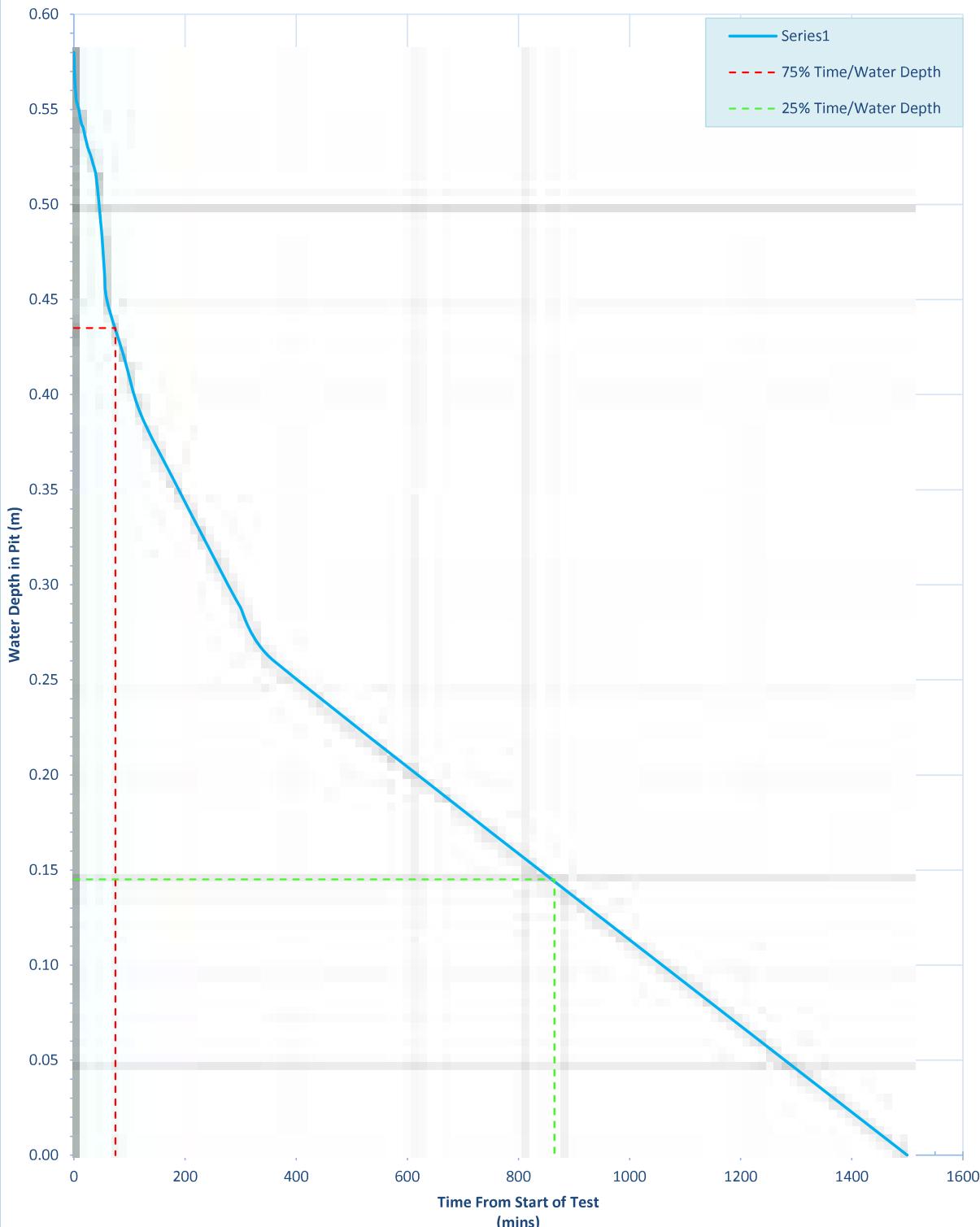


BRE 365 SOIL INFILTRATION TEST



BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	3	SOIL TYPE	Grey, sandy, organic, clayey SILT	TP08

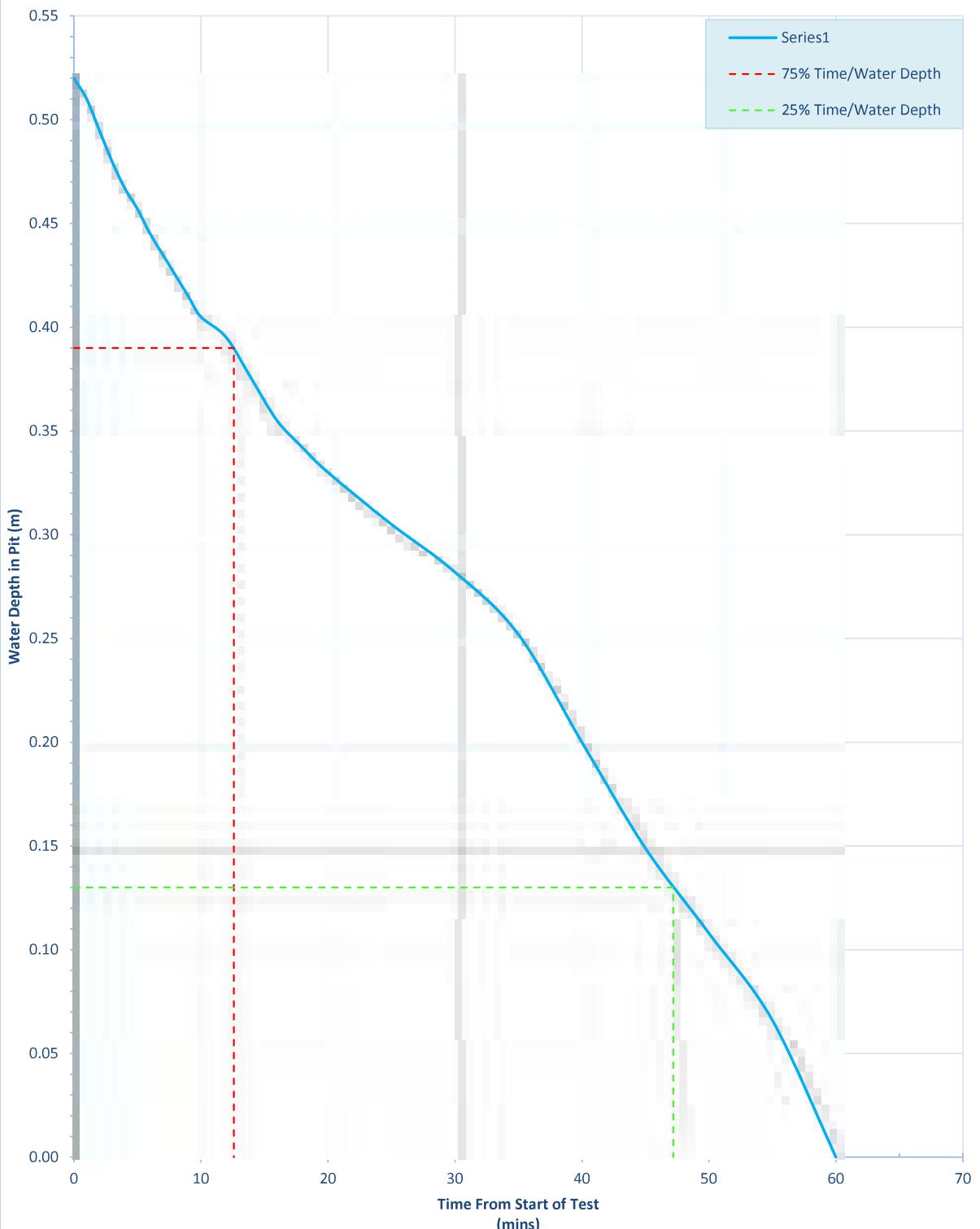


BRE 365 SOIL INFILTRATION TEST



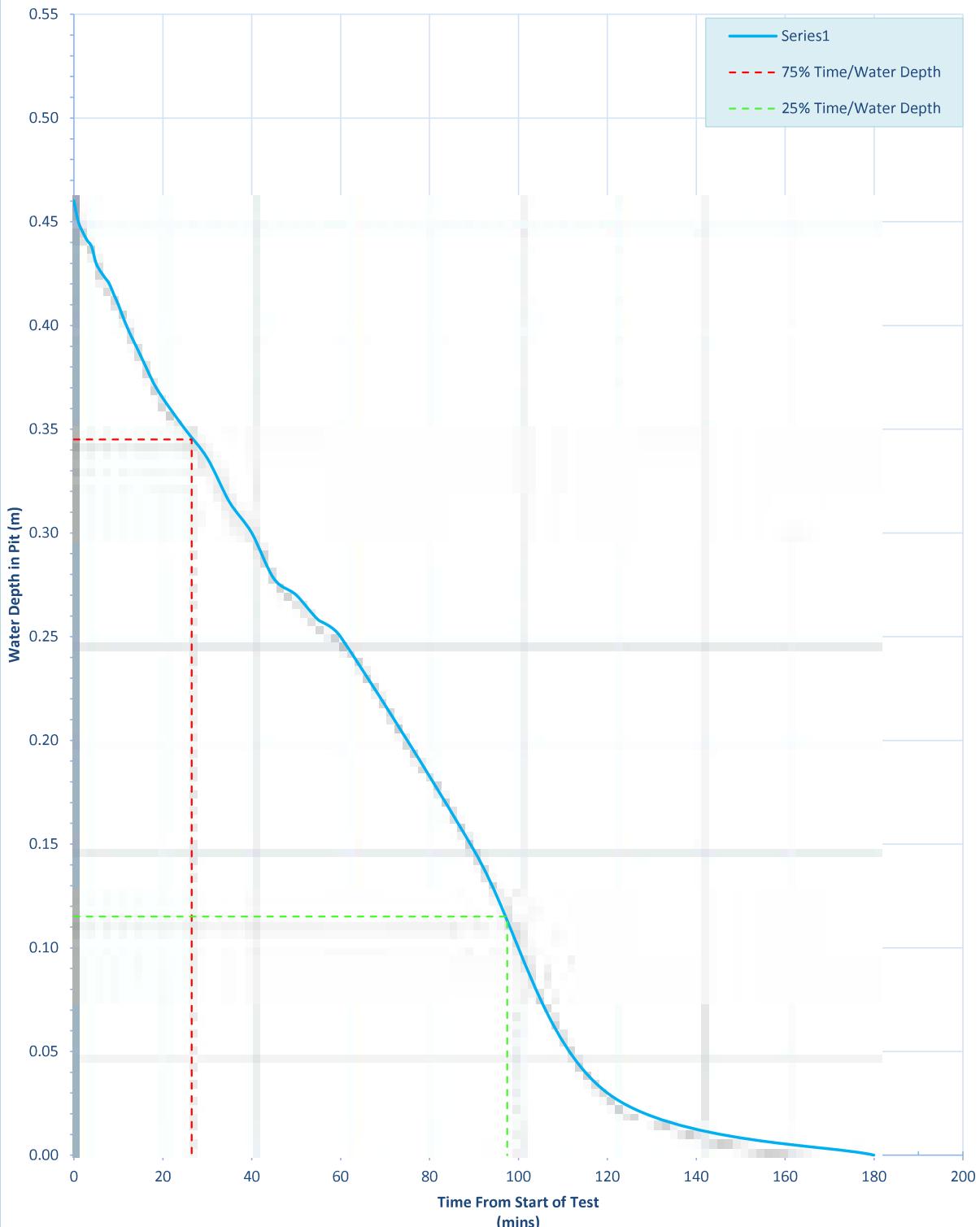
BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.70	SOIL TYPE	Light brown silty, sandy, gravelly CLAY	TP09



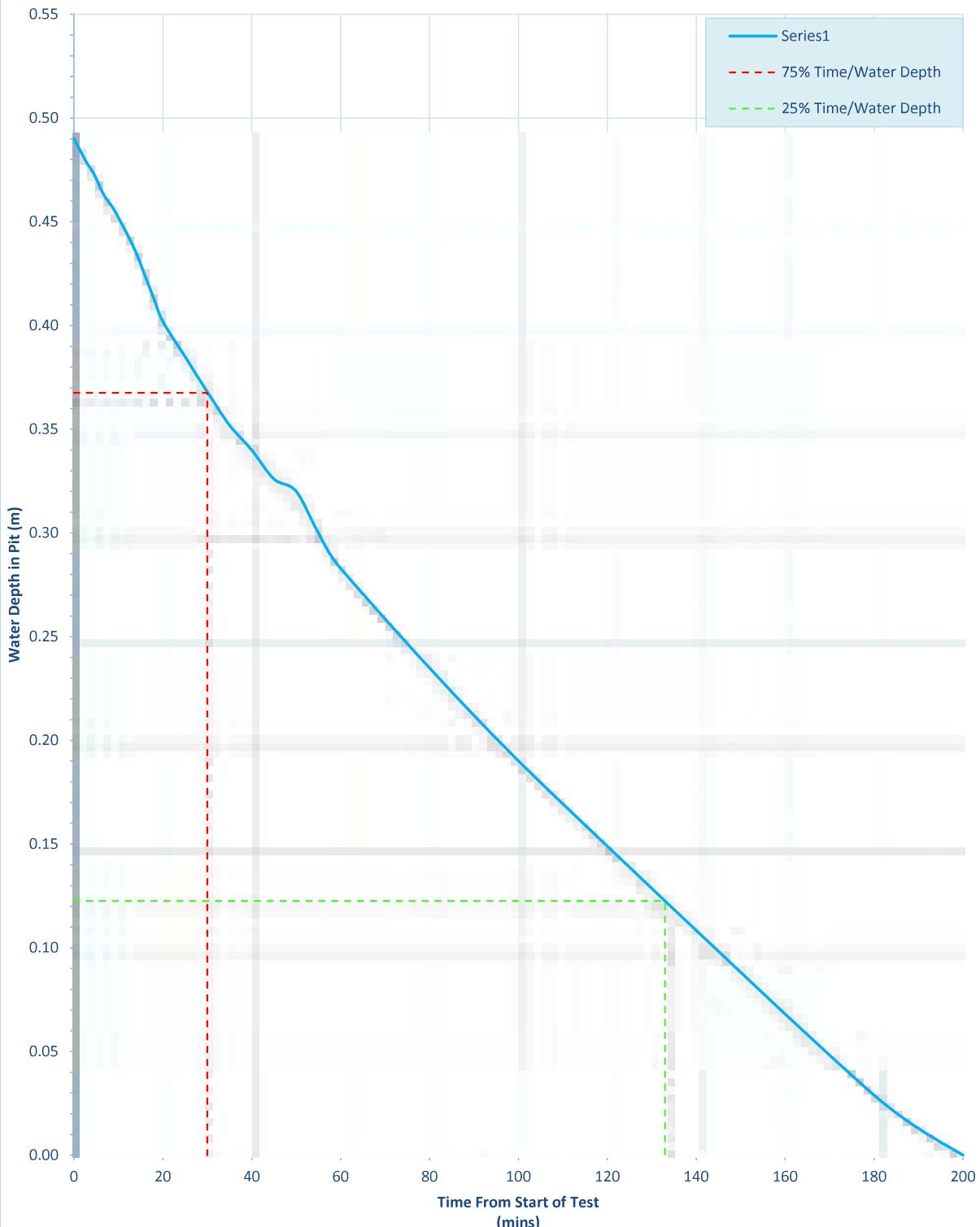
BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.70	SOIL TYPE	Light brown silty, sandy, gravelly CLAY	TP09



BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.70	SOIL TYPE	Light brown silty, sandy, gravelly CLAY	TP09

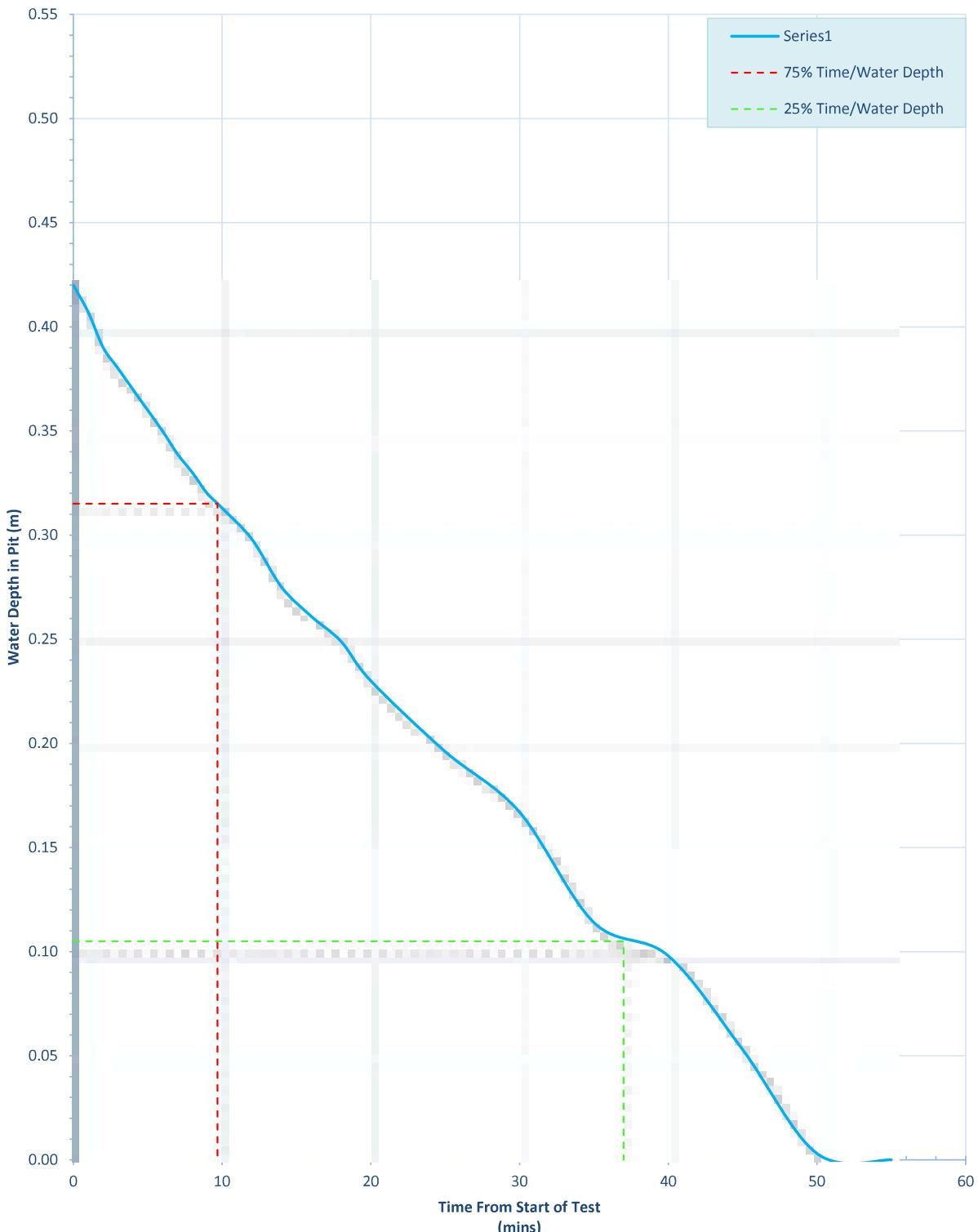


BRE 365 SOIL INFILTRATION TEST



BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.70	SOIL TYPE	Light brown silty, sandy, gravelly CLAY	TP10

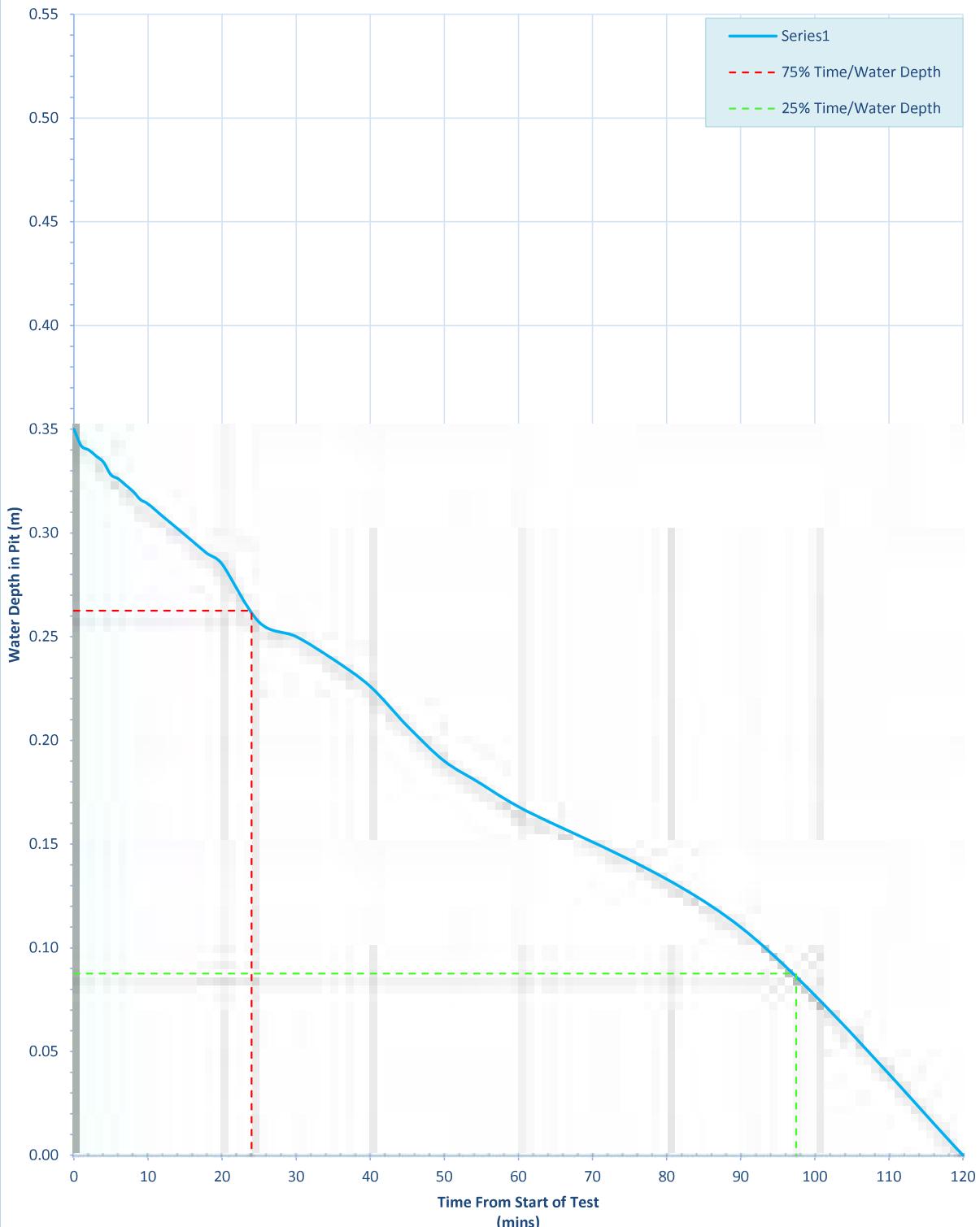


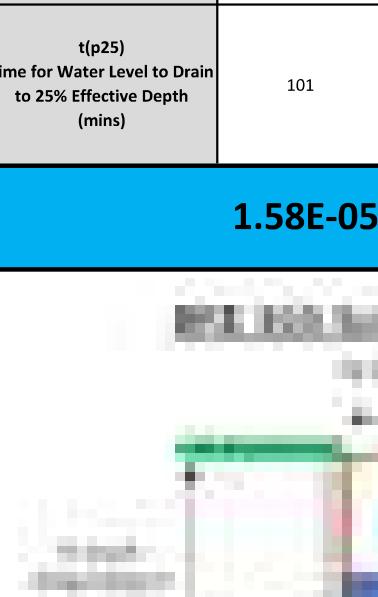
BRE 365 SOIL INFILTRATION TEST



BRE 365 SOIL INFILTRATION TEST

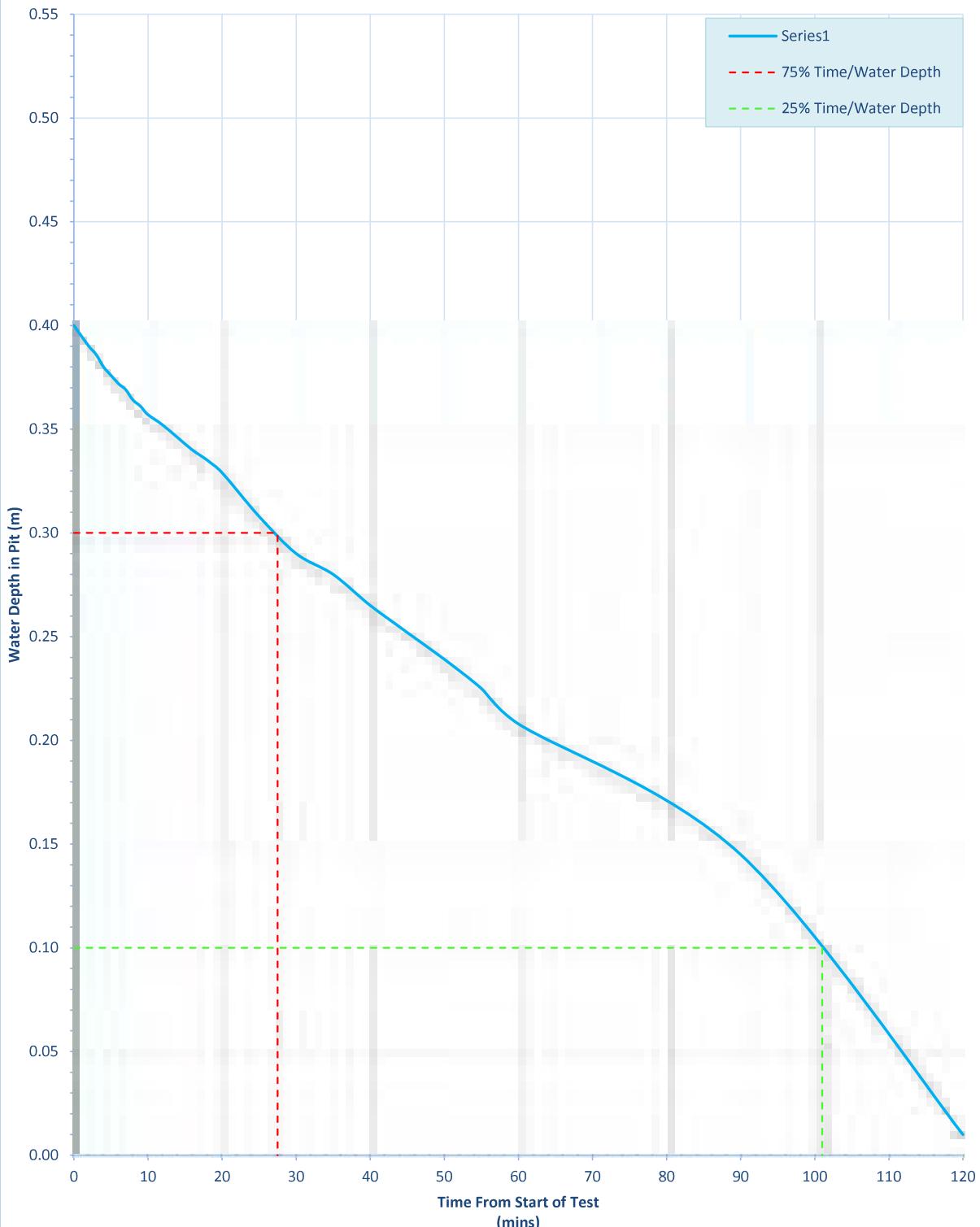
JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.70	SOIL TYPE	Light brown silty, sandy, gravelly CLAY	TP10

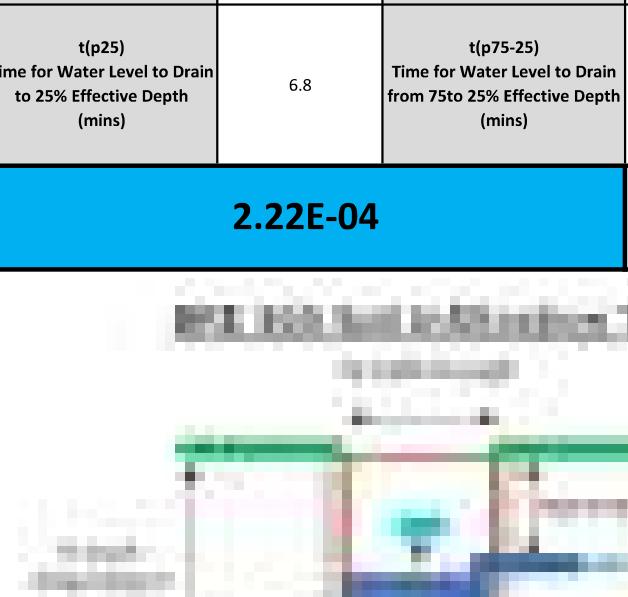
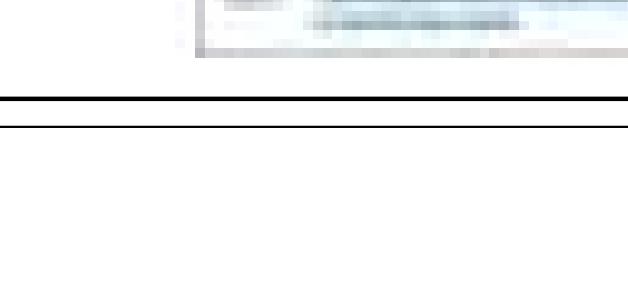


BRE 365 SOIL INFILTRATION TEST					
JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.	TP10
INFILTRATION TEST No.	3	SOIL TYPE	Light brown silty, sandy, gravelly CLAY	WEATHER CONDITIONS	DRY
TEST PIT WIDTH (m)	0.50	TEST PIT LENGTH (m)	1.50	TEST PIT DEPTH (m)	0.70
WATER SURFACE LEVEL (m)	0.30	GROUNDWATER DEPTH (m)	Dry	HEAD OF WATER IN PIT (m)	0.40
BASE SURFACE AREA (m ²)	0.75	SIDEWALL SURFACE AREA (m ²)	2.80	a(p50) Internal Surface Area @ 50% Effective Depth (m ²)	2.15
75% Effective Water Depth (m)	0.3	25% Effective Water Depth (m)	0.1	V(p75-25) Volume of Hole Between 75 & 25% Effective Water Depth (m ³)	0.15
t(p75) Time for Water Level to Drain to 75% Effective Depth (mins)	27.5	t(p25) Time for Water Level to Drain to 25% Effective Depth (mins)	101	t(p75-25) Time for Water Level to Drain from 75 to 25% Effective Depth (mins)	73.5
SOIL INFILTRATION RATE		1.58E-05			m/sec
24 Hr Clock Time hh:mm	Time Elapsed (mins)	Depth of Water in Pit (m)			
09:00	0	0.400			
09:01	1	0.395			
09:02	2	0.390			
09:03	3	0.386			
09:04	4	0.380			
09:05	5	0.376			
09:06	6	0.372			
09:07	7	0.369			
09:08	8	0.364			
09:09	9	0.361			
09:10	10	0.357			
09:15	12	0.352			
09:30	14	0.346			
09:45	16	0.340			
10:00	18	0.335			
10:15	20	0.329			
10:30	25	0.308			
10:45	30	0.290			
11:00	35	0.280			
11:30	40	0.265			
12:00	45	0.252			
12:30	50	0.239			
13:00	55	0.225			
13:30	60	0.208			
14:00	90	0.145			
14:30	120	0.010			
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
					
			<img alt="A		

BRE 365 SOIL INFILTRATION TEST

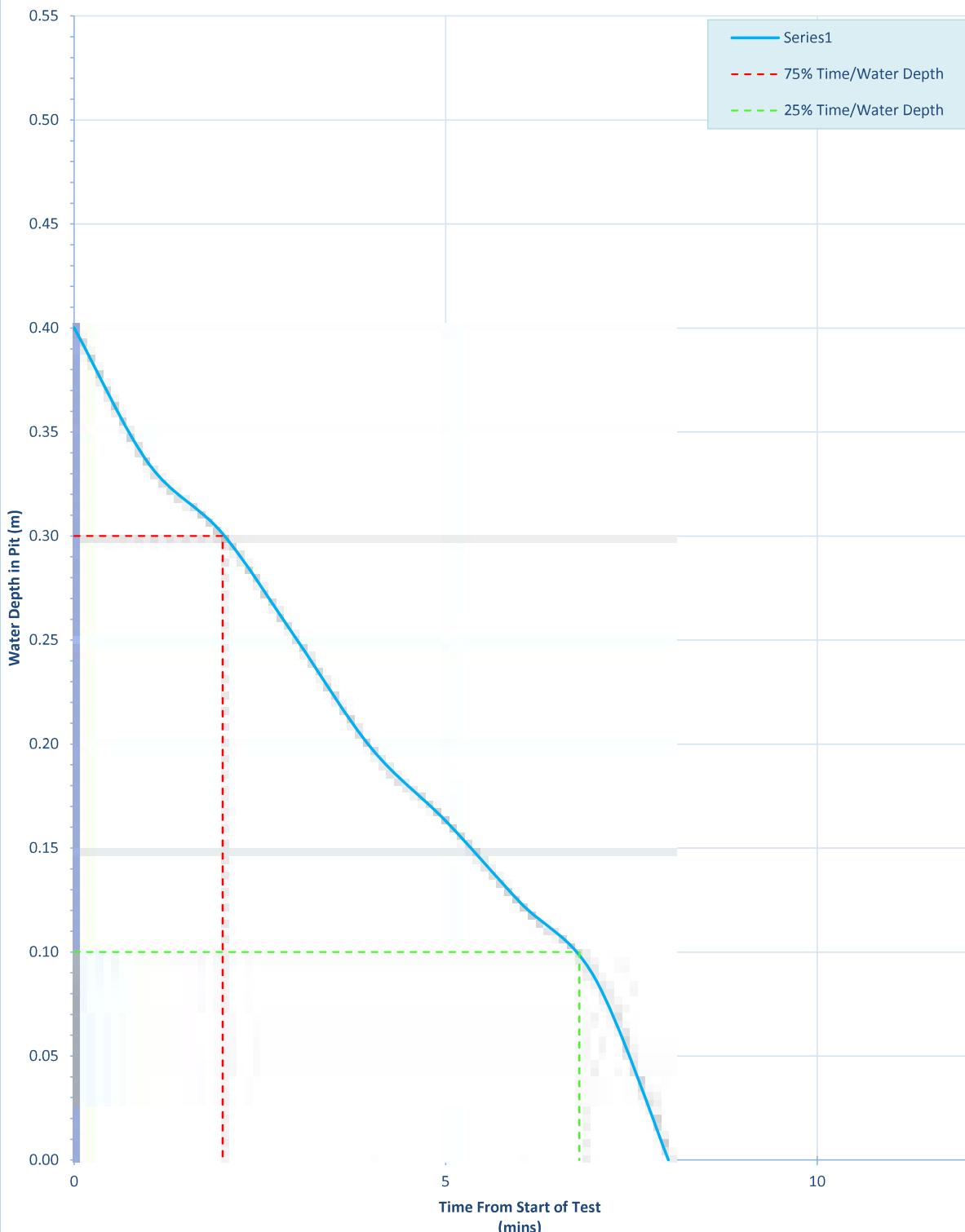
JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.70	SOIL TYPE	Light brown silty, sandy, gravelly CLAY	TP10



BRE 365 SOIL INFILTRATION TEST					
JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.	TP11
INFILTRATION TEST No.	1	SOIL TYPE	Light brown silty, sandy, gravelly CLAY	WEATHER CONDITIONS	DRY
TEST PIT WIDTH (m)	0.50	TEST PIT LENGTH (m)	1.50	TEST PIT DEPTH (m)	0.80
WATER SURFACE LEVEL (m)	0.40	GROUNDWATER DEPTH (m)	Dry	HEAD OF WATER IN PIT (m)	0.40
BASE SURFACE AREA (m ²)	0.75	SIDEWALL SURFACE AREA (m ²)	3.20	a(p50) Internal Surface Area @ 50% Effective Depth (m ²)	2.35
75% Effective Water Depth (m)	0.3	25% Effective Water Depth (m)	0.1	V(p75-25) Volume of Hole Between 75 & 25% Effective Water Depth (m ³)	0.15
t(p75) Time for Water Level to Drain to 75% Effective Depth (mins)	2	t(p25) Time for Water Level to Drain to 25% Effective Depth (mins)	6.8	t(p75-25) Time for Water Level to Drain from 75 to 25% Effective Depth (mins)	4.8
SOIL INFILTRATION RATE		2.22E-04			m/sec
24 Hr Clock Time hh:mm	Time Elapsed (mins)	Depth of Water in Pit (m)			
09:00	0	0.400			
09:01	1	0.335			
09:02	2	0.301			
09:03	3	0.250			
09:04	4	0.198			
09:05	5	0.163			
09:06	6	0.124			
09:07	7	0.088			
09:08	8	0.000			

BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.80	SOIL TYPE	Light brown silty, sandy, gravelly CLAY	TP11

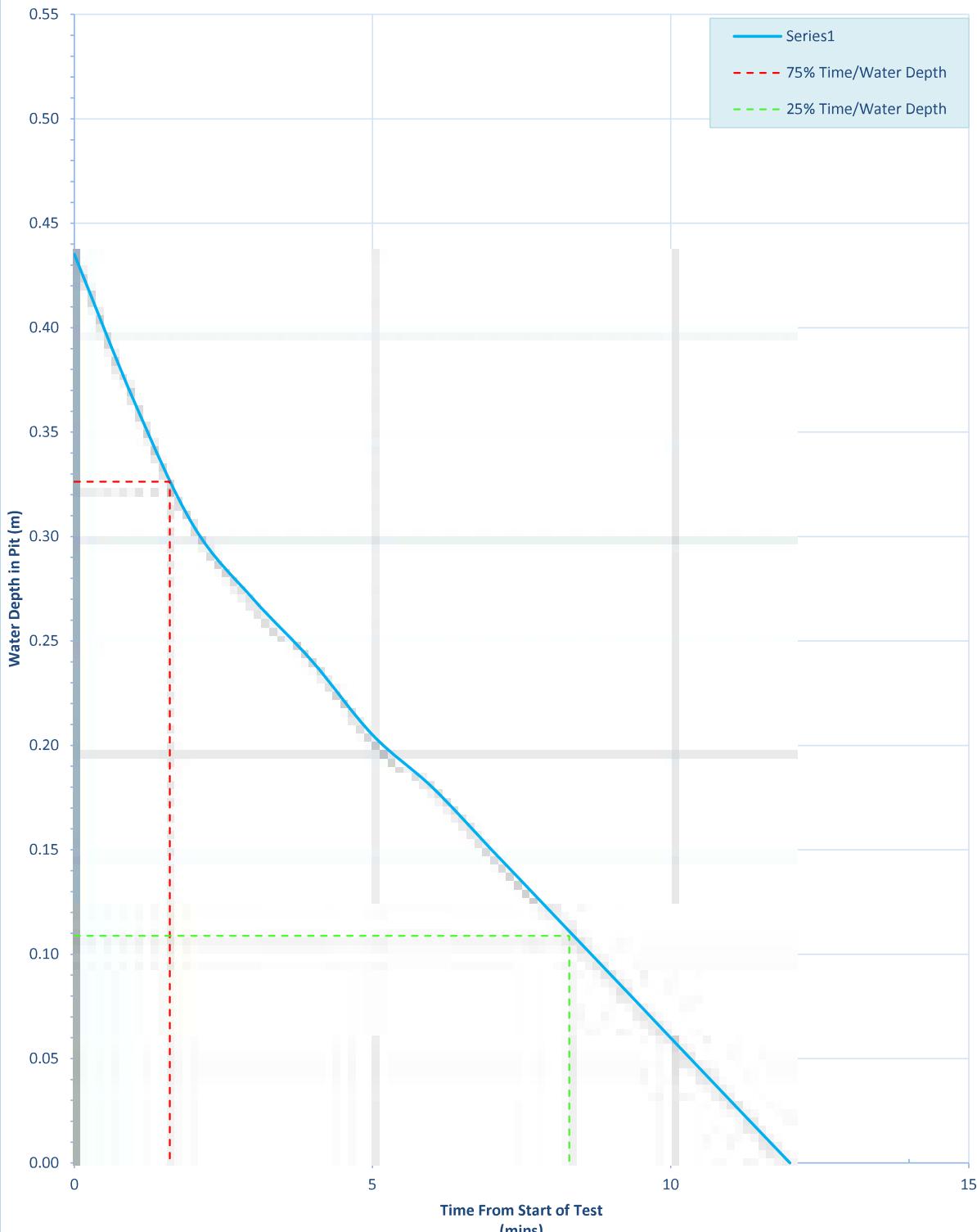


BRE 365 SOIL INFILTRATION TEST



BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.80	SOIL TYPE	Light brown silty, sandy, gravelly CLAY	TP11

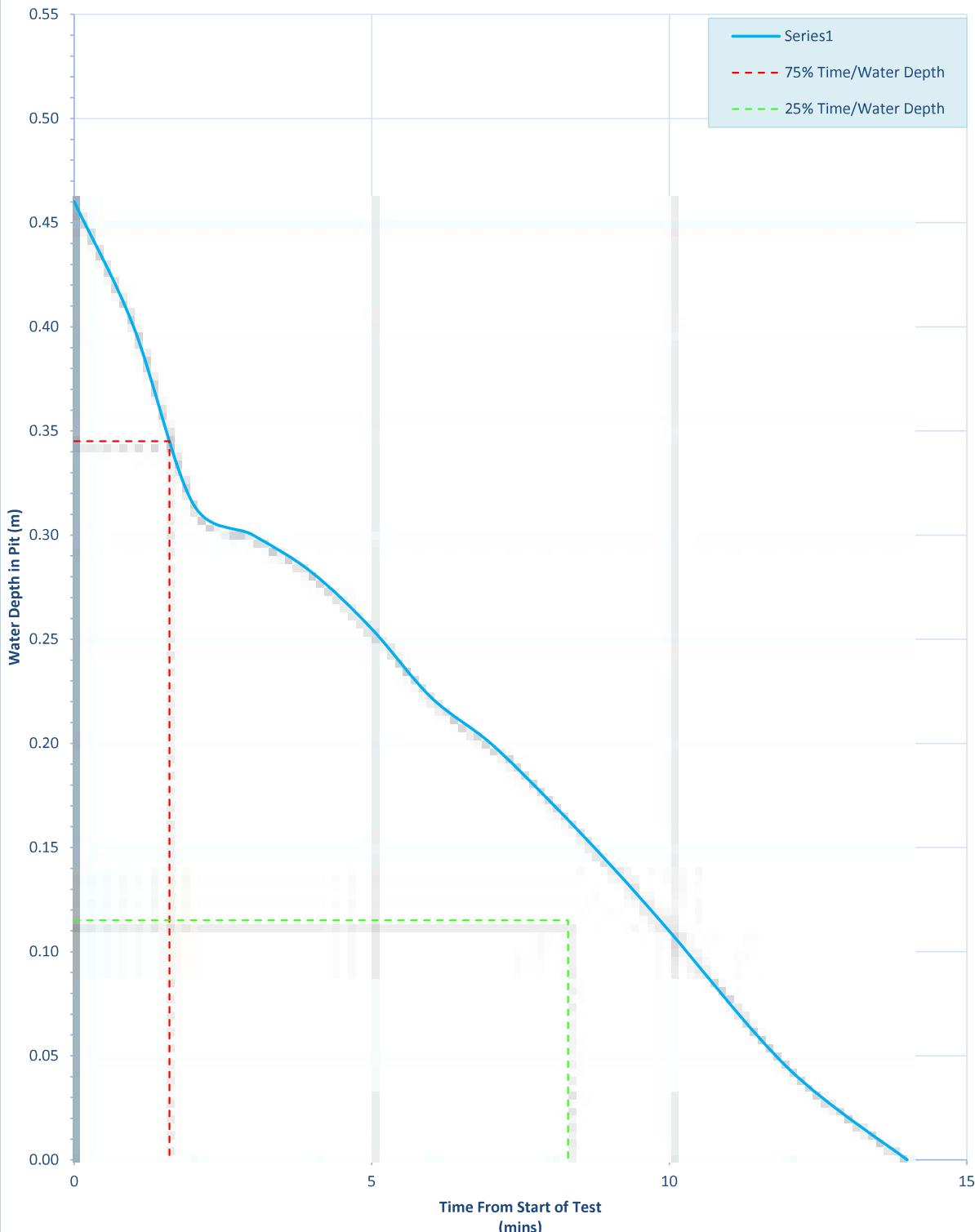


BRE 365 SOIL INFILTRATION TEST



BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.80	SOIL TYPE	Light brown silty, sandy, gravelly CLAY	TP11

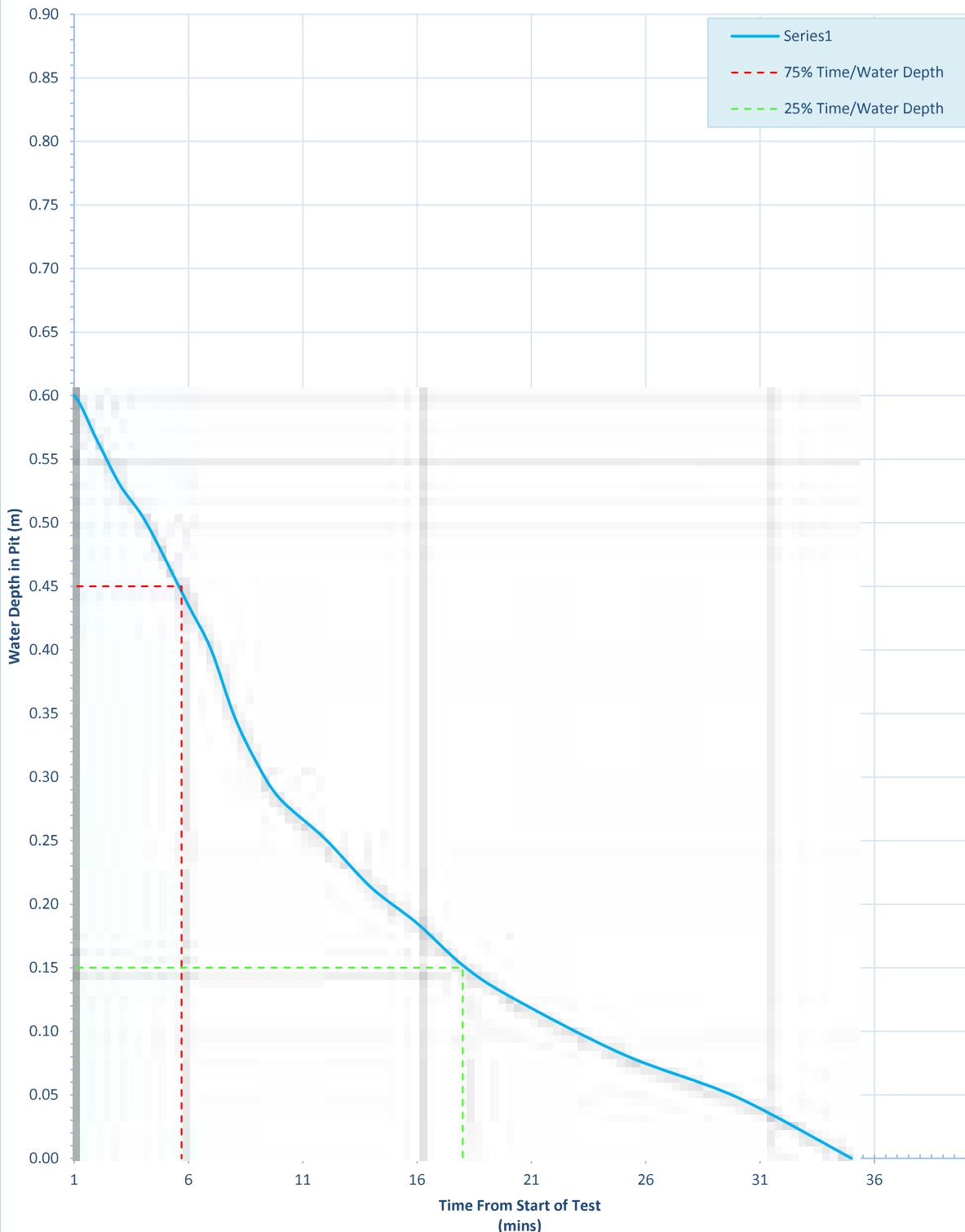


BRE 365 SOIL INFILTRATION TEST



BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.90	SOIL TYPE	See TP Log	TP12



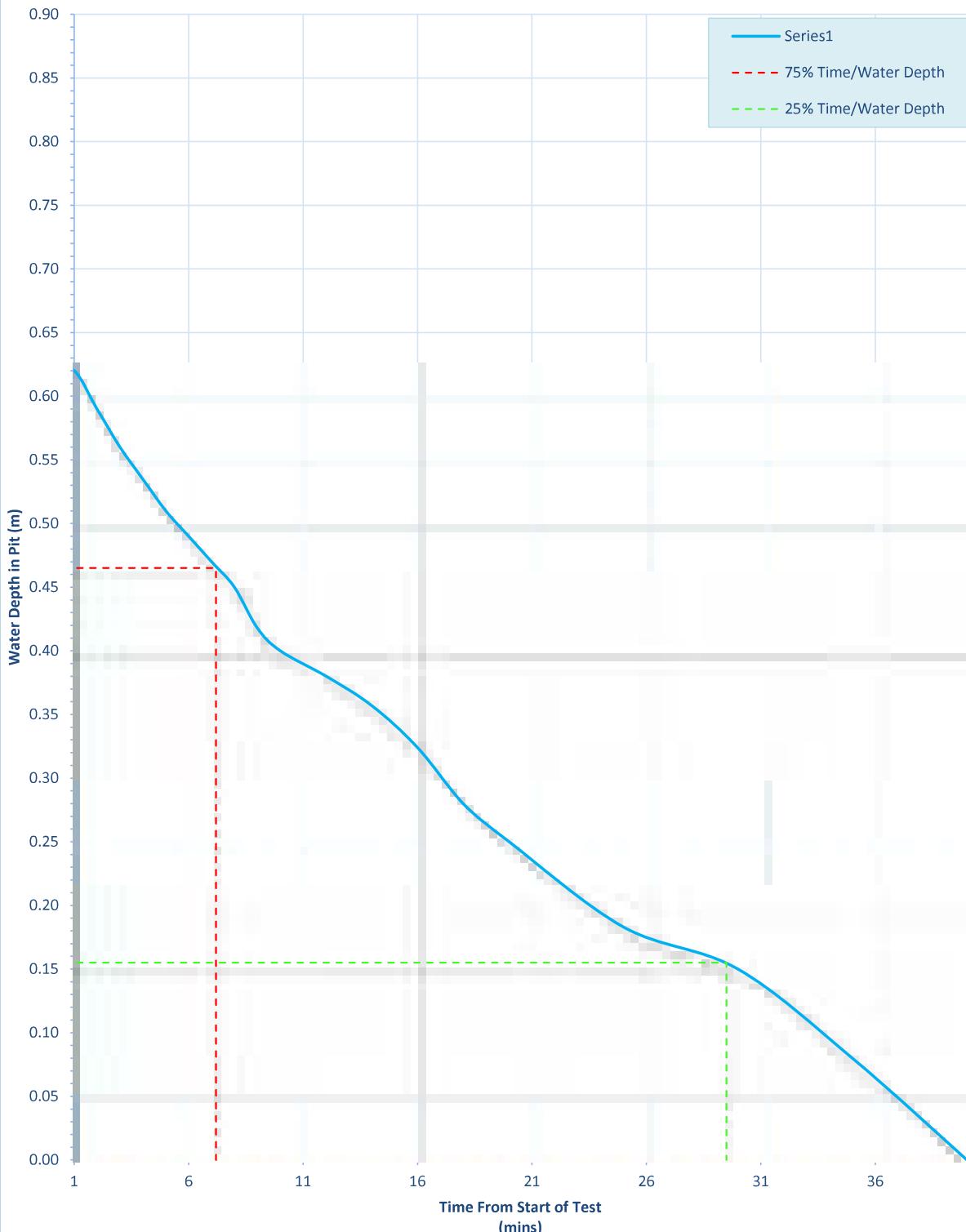
BRE 365 SOIL INFILTRATION TEST



JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.	TP12		
INFILTRATION TEST No.	2	SOIL TYPE	See TP Log	WEATHER CONDITIONS	DRY		
TEST PIT WIDTH (m)	0.50	TEST PIT LENGTH (m)	1.40	TEST PIT DEPTH (m)	0.90		
WATER SURFACE LEVEL (m)	0.28	GROUNDWATER DEPTH (m)	Dry	HEAD OF WATER IN PIT (m)	0.62		
BASE SURFACE AREA (m ²)	0.70	SIDEWALL SURFACE AREA (m ²)	3.42	a(p50) Internal Surface Area @ 50% Effective Depth (m ²)	2.41		
75% Effective Water Depth (m)	0.465	25% Effective Water Depth (m)	0.155	V(p75-25) Volume of Hole Between 75 & 25% Effective Water Depth (m ³)	0.217		
t(p75) Time for Water Level to Drain to 75% Effective Depth (mins)	7.2	t(p25) Time for Water Level to Drain to 25% Effective Depth (mins)	29.5	t(p75-25) Time for Water Level to Drain from 75to 25% Effective Depth (mins)	22.3		
SOIL INFILTRATION RATE	6.73E-05			m/sec			
24 Hr Clock Time hh:mm	Time Elapsed (mins)	Depth of Water in Pit (m)					
10:30	0	0.620					
11:22	1	0.620					
11:23	2	0.590					
11:24	3	0.560					
11:25	4	0.535					
11:26	5	0.510					
11:27	6	0.490					
11:28	7	0.470					
11:29	8	0.450					
11:30	9	0.418					
11:31	10	0.400					
11:33	12	0.380					
11:35	14	0.357					
11:37	16	0.324					
11:39	18	0.280					
11:41	20	0.250					
11:46	25	0.183					
11:51	30	0.150					
11:56	35	0.080					
12:01	40	0.000					

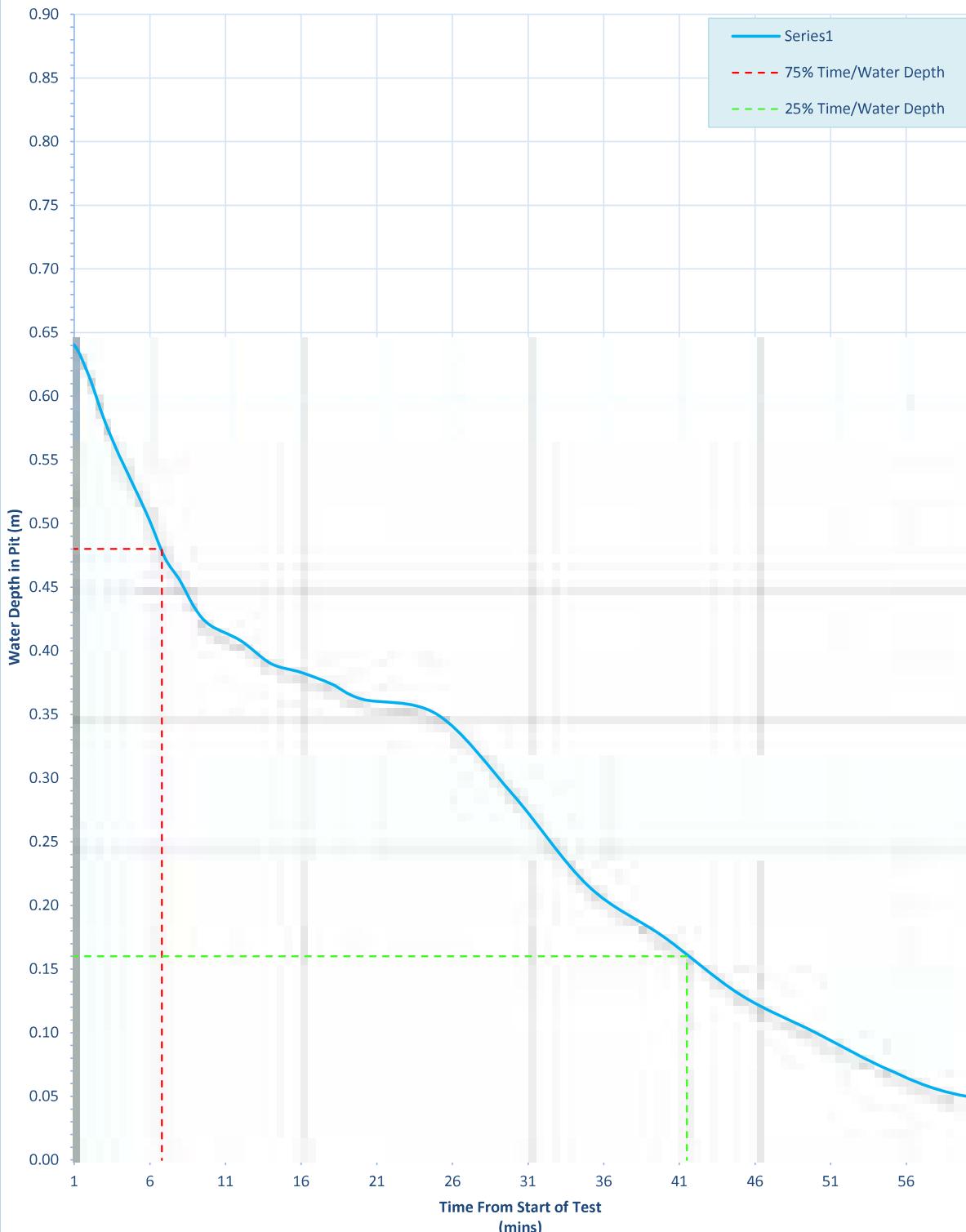
BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.90	SOIL TYPE	See TP Log	TP12



BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.90	SOIL TYPE	See TP Log	TP12

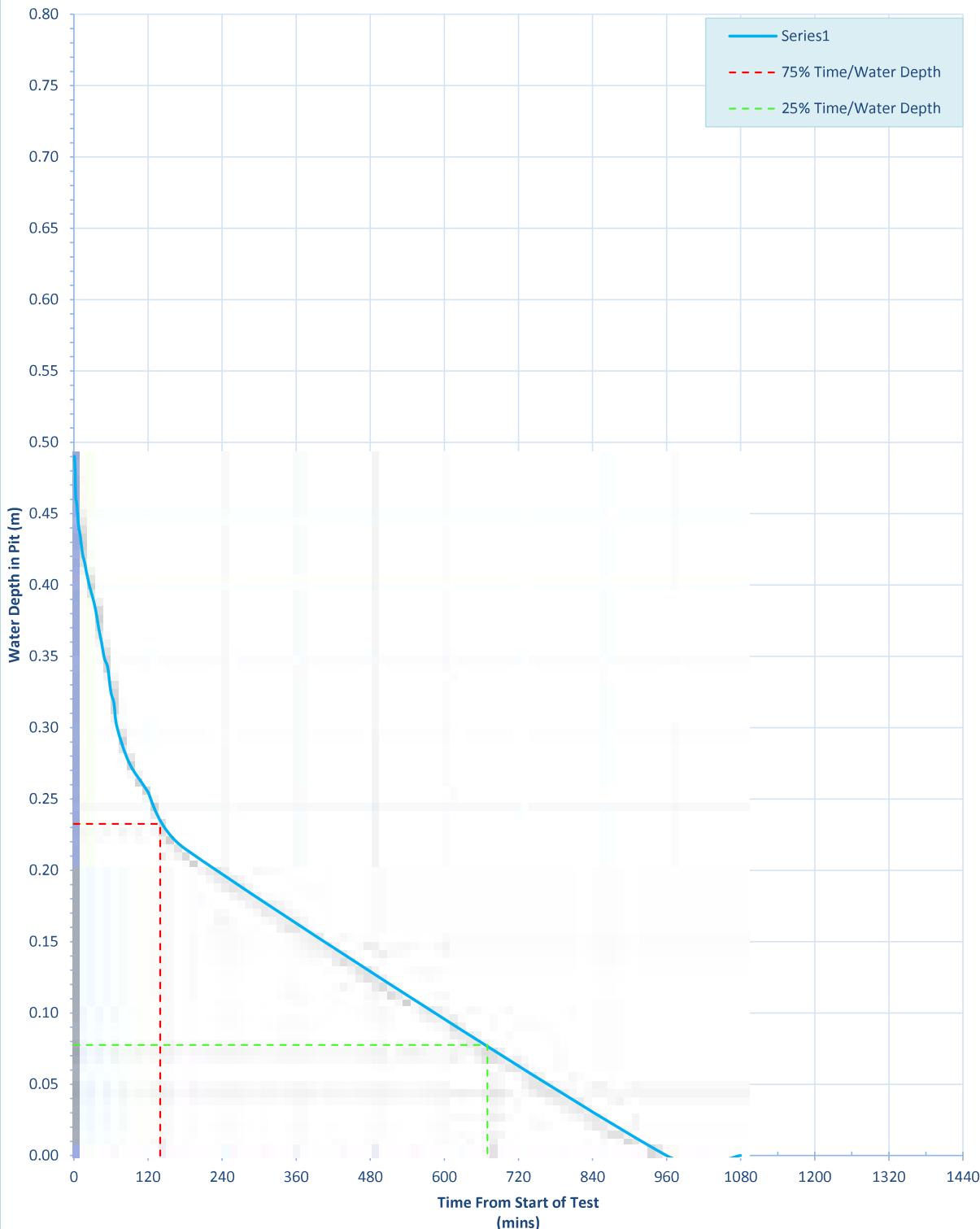


BRE 365 SOIL INFILTRATION TEST



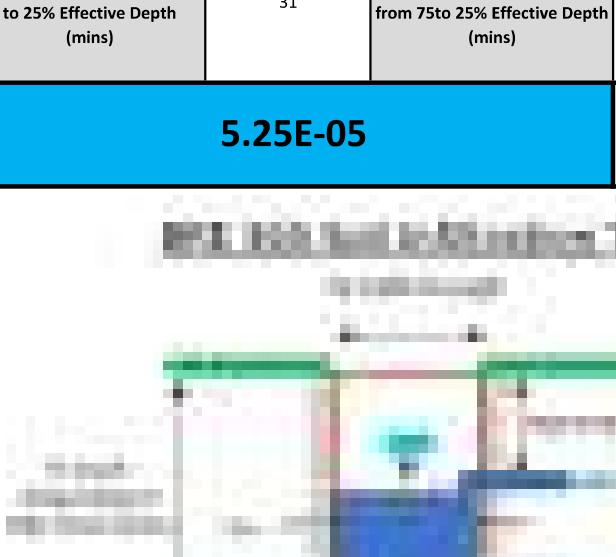
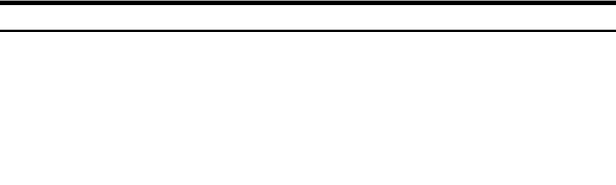
BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.80	SOIL TYPE	See TP Log	TP13



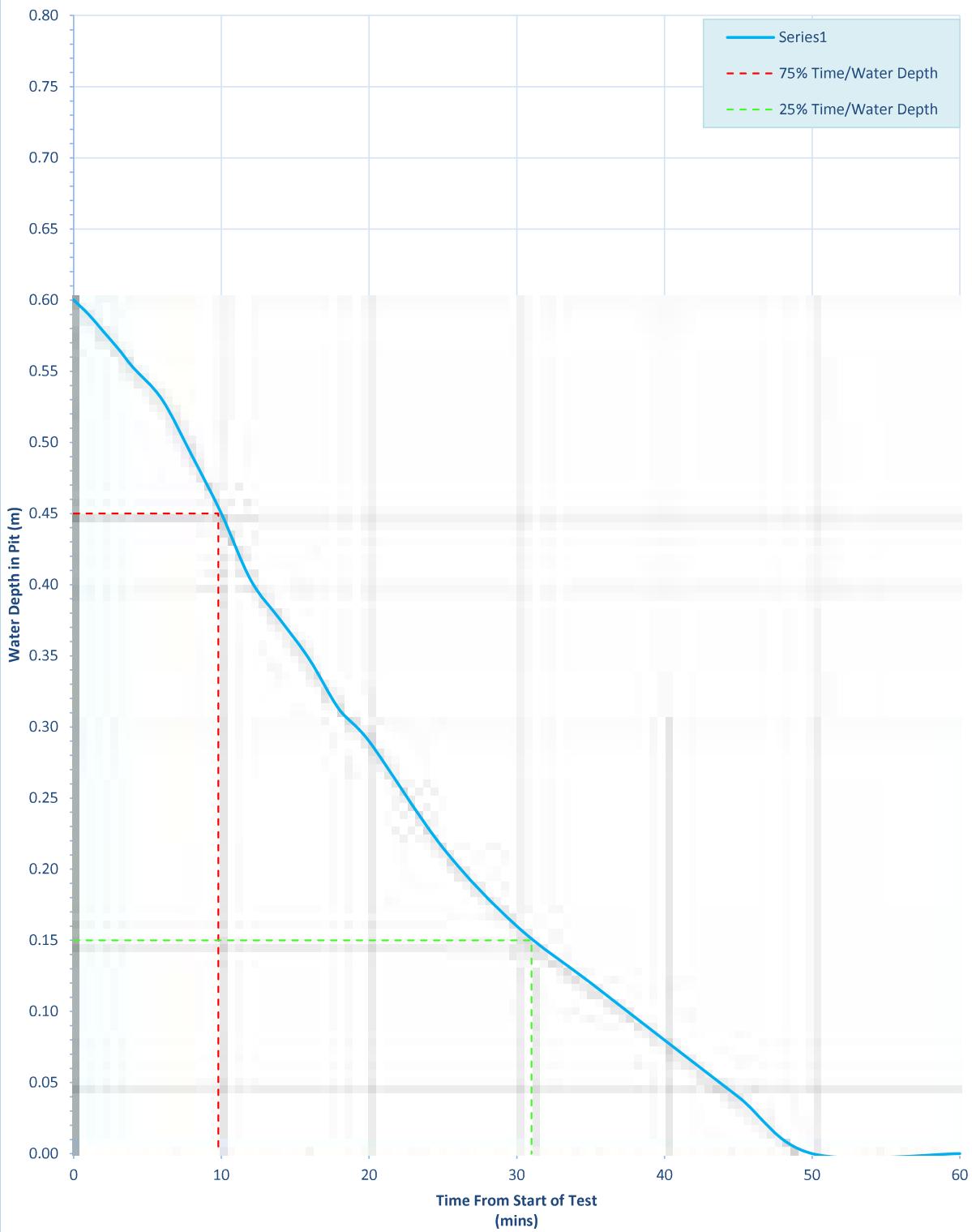
BRE 365 SOIL INFILTRATION TEST



JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.	TP14
INFILTRATION TEST No.	1	SOIL TYPE	See TP Log	WEATHER CONDITIONS	DRY
TEST PIT WIDTH (m)	0.50	TEST PIT LENGTH (m)	1.10	TEST PIT DEPTH (m)	1.20
WATER SURFACE LEVEL (m)	0.60	GROUNDWATER DEPTH (m)	Dry	HEAD OF WATER IN PIT (m)	0.60
BASE SURFACE AREA (m ²)	0.55	SIDEWALL SURFACE AREA (m ²)	3.84	a(p50) Internal Surface Area @ 50% Effective Depth (m ²)	2.47
75% Effective Water Depth (m)	0.45	25% Effective Water Depth (m)	0.15	V(p75-25) Volume of Hole Between 75 & 25% Effective Water Depth (m ³)	0.165
t(p75) Time for Water Level to Drain to 75% Effective Depth (mins)	9.8	t(p25) Time for Water Level to Drain to 25% Effective Depth (mins)	31	t(p75-25) Time for Water Level to Drain from 75to 25% Effective Depth (mins)	21.2
SOIL INFILTRATION RATE		5.25E-05			m/sec
24 Hr Clock Time hh:mm	Time Elapsed (mins)	Depth of Water in Pit (m)			
15:22	0	0.600			
15:23	1	0.590			
15:24	2	0.578			
15:25	3	0.566			
15:26	4	0.553			
15:28	6	0.530			
15:30	8	0.491			
15:32	10	0.450			
15:34	12	0.403			
15:36	14	0.375			
15:38	16	0.347			
15:40	18	0.312			
15:42	20	0.290			
15:47	25	0.215			
15:52	30	0.160			
15:57	35	0.120			
16:02	40	0.080			
16:07	45	0.040			
16:12	50	0.000			

BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	1.20	SOIL TYPE	See TP Log	TP14

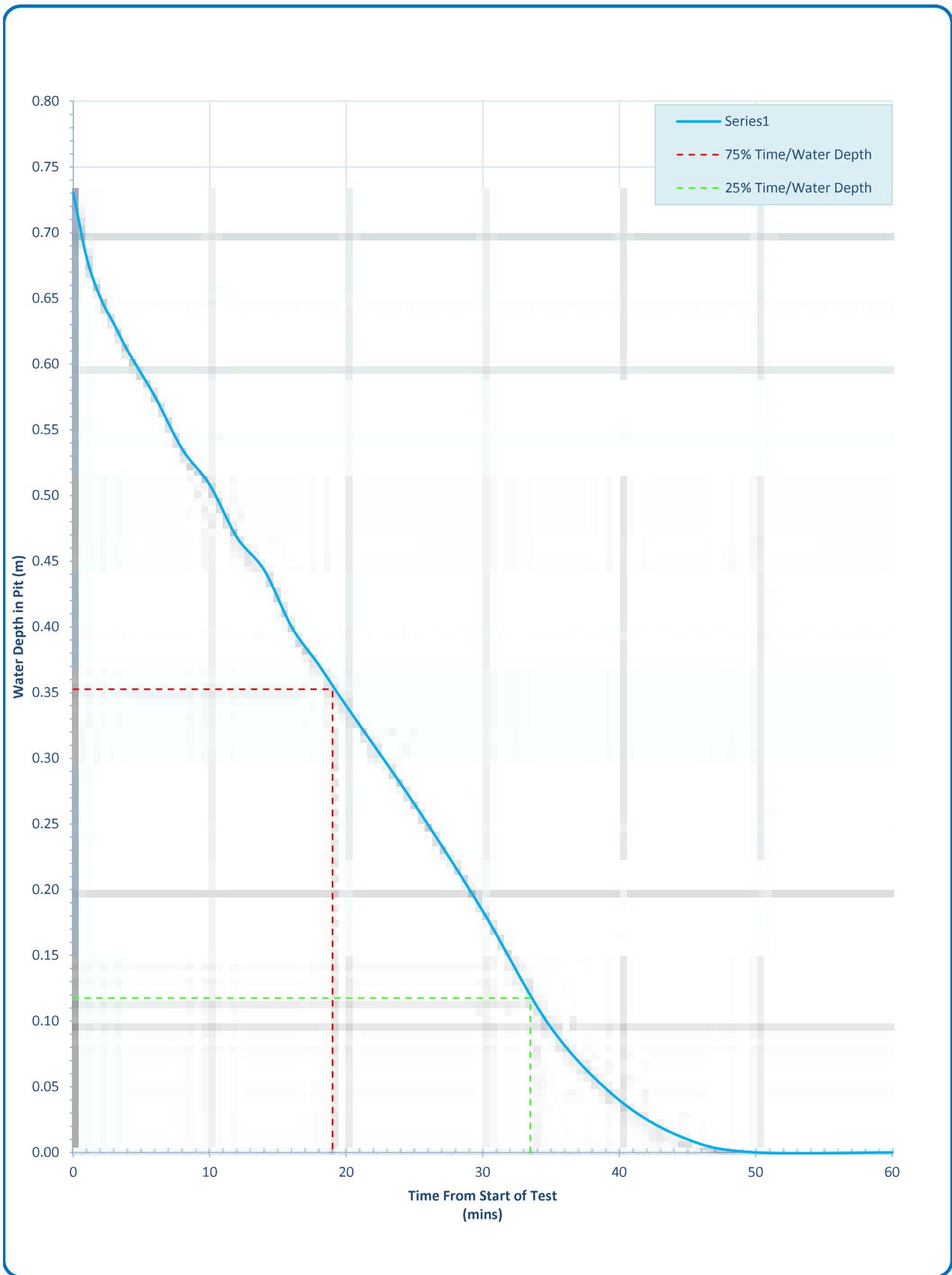


BRE 365 SOIL INFILTRATION TEST



BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	1.20	SOIL TYPE	See TP Log	TP14

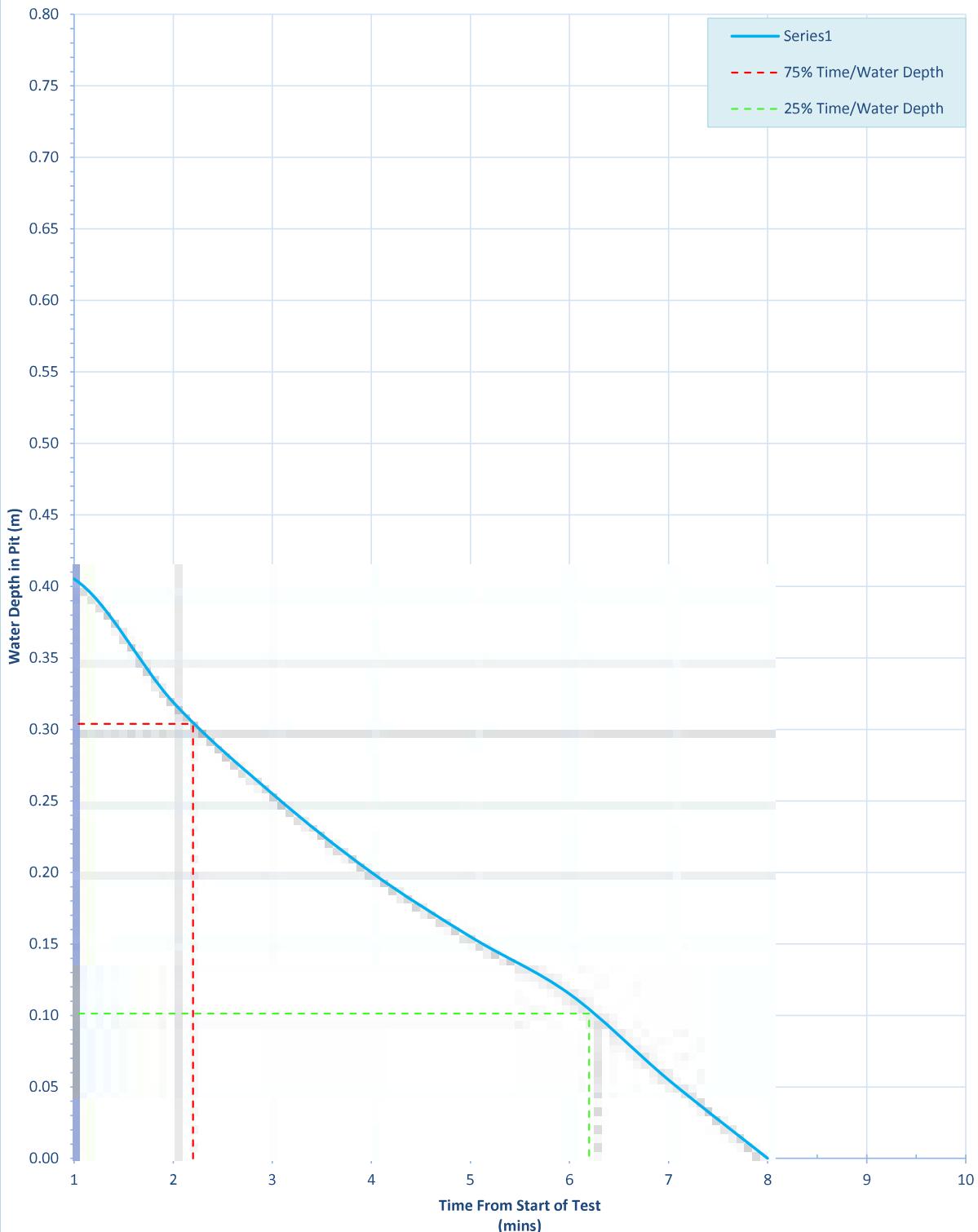


BRE 365 SOIL INFILTRATION TEST



BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.80	SOIL TYPE	See TP Log	TP15

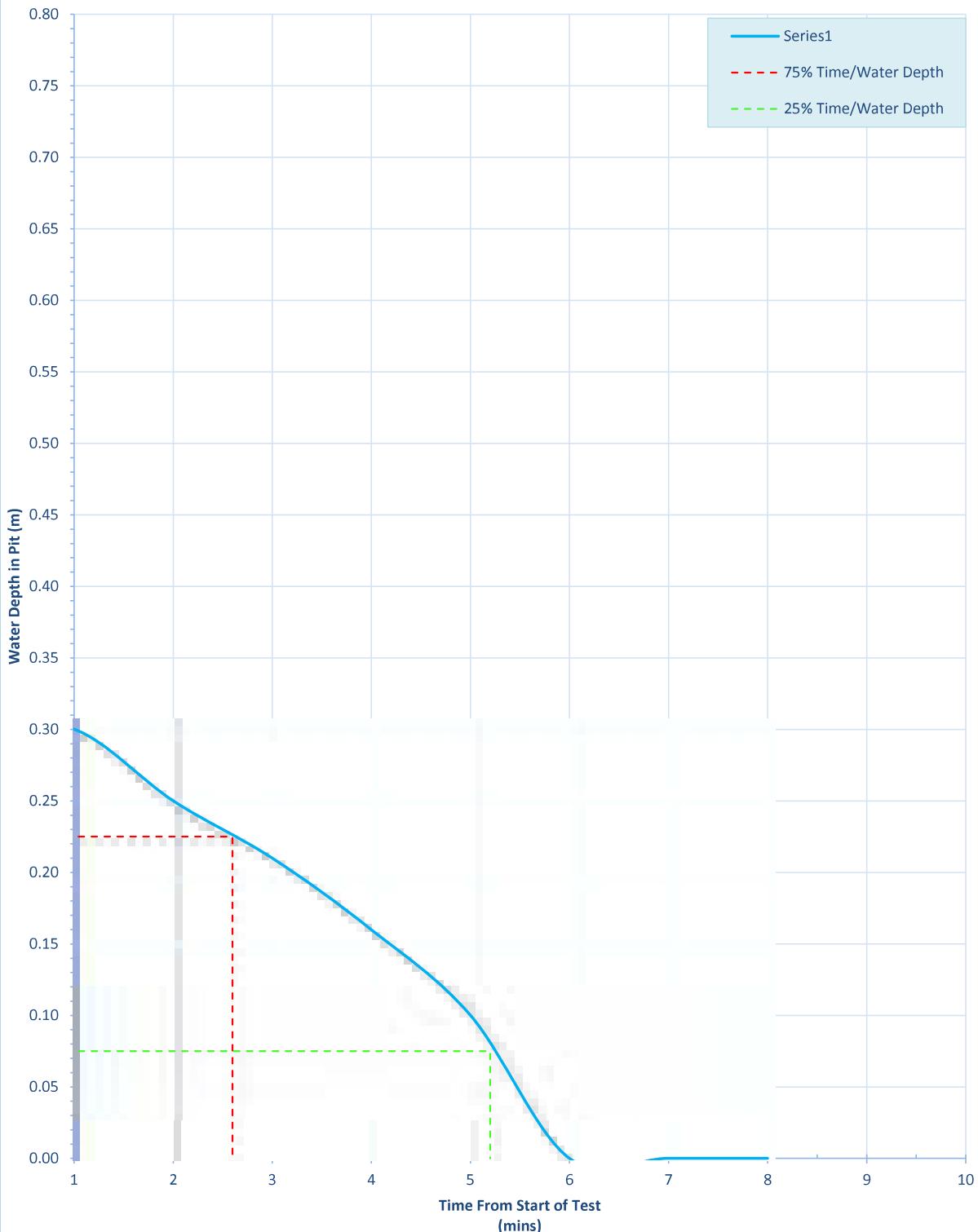


BRE 365 SOIL INFILTRATION TEST



BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.80	SOIL TYPE	See TP Log	TP15



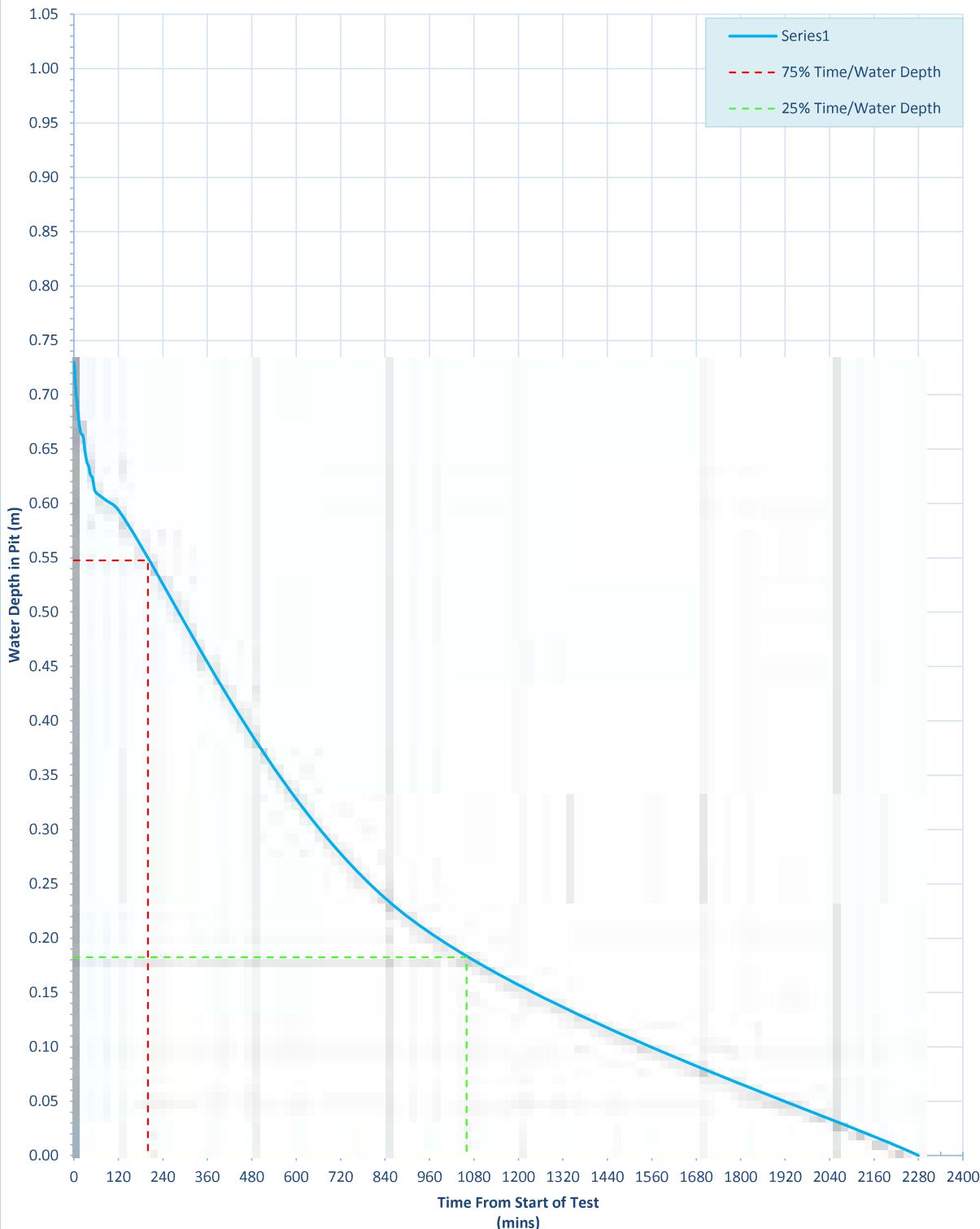
BRE 365 SOIL INFILTRATION TEST



JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.	TP16
INFILTRATION TEST No.	1	SOIL TYPE	See TP Log	WEATHER CONDITIONS	DRY
TEST PIT WIDTH (m)	0.50	TEST PIT LENGTH (m)	1.50	TEST PIT DEPTH (m)	1.05
WATER SURFACE LEVEL (m)	0.32	GROUNDWATER DEPTH (m)	Dry	HEAD OF WATER IN PIT (m)	0.73
BASE SURFACE AREA (m ²)	0.75	SIDEWALL SURFACE AREA (m ²)	4.20	a(p50) Internal Surface Area @ 50% Effective Depth (m ²)	2.85
75% Effective Water Depth (m)	0.5475	25% Effective Water Depth (m)	0.1825	V(p75-25) Volume of Hole Between 75 & 25% Effective Water Depth (m ³)	0.27375
t(p75) Time for Water Level to Drain to 75% Effective Depth (mins)	200	t(p25) Time for Water Level to Drain to 25% Effective Depth (mins)	1060	t(p75-25) Time for Water Level to Drain from 75to 25% Effective Depth (mins)	860
SOIL INFILTRATION RATE	1.86E-06				m/sec
24 Hr Clock Time hh:mm	Time Elapsed (mins)	Depth of Water in Pit (m)			
15:22	0	0.730			
15:23	1	0.728			
15:24	2	0.724			
15:25	3	0.715			
15:26	4	0.710			
15:27	5	0.706			
15:28	6	0.700			
15:29	7	0.697			
15:30	8	0.695			
15:31	9	0.692			
15:32	10	0.686			
15:34	12	0.682			
15:36	14	0.673			
15:38	16	0.669			
15:40	18	0.666			
15:42	20	0.664			
15:47	25	0.662			
15:52	30	0.649			
15:57	35	0.638			
16:02	40	0.634			
16:07	45	0.626			
16:12	50	0.624			
16:17	55	0.614			
16:22	60	0.610			
16:52	90	0.602			
17:22	120	0.594			
09:00	878	0.226			
Interpolated	2280	0.000			

BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	1.05	SOIL TYPE	See TP Log	TP16

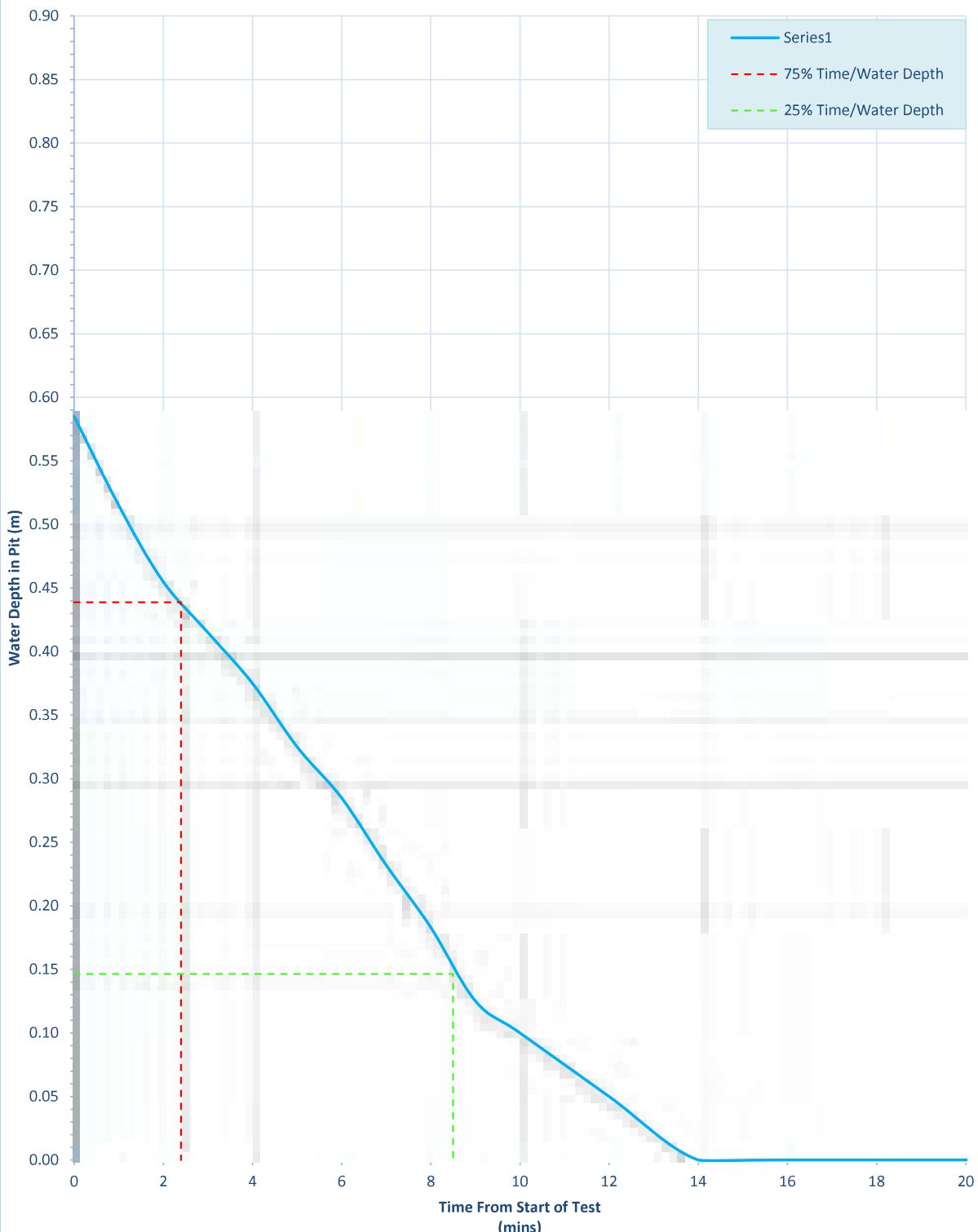


BRE 365 SOIL INFILTRATION TEST



BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.90	SOIL TYPE	See TP Log	TP17



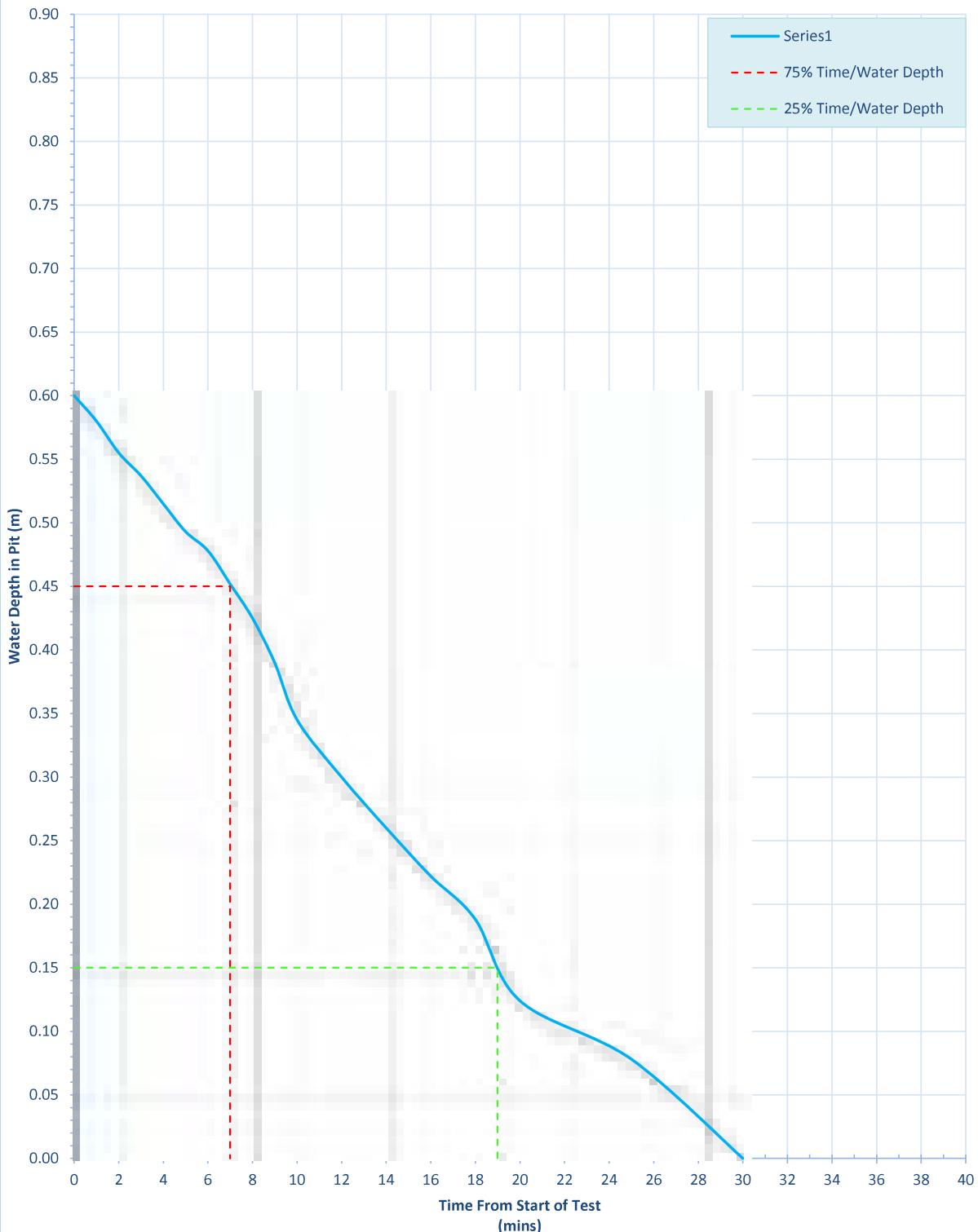
BRE 365 SOIL INFILTRATION TEST



JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.	TP17		
INFILTRATION TEST No.	2	SOIL TYPE	See TP Log	WEATHER CONDITIONS	DRY		
TEST PIT WIDTH (m)	0.50	TEST PIT LENGTH (m)	1.40	TEST PIT DEPTH (m)	0.90		
WATER SURFACE LEVEL (m)	0.30	GROUNDWATER DEPTH (m)	Dry	HEAD OF WATER IN PIT (m)	0.60		
BASE SURFACE AREA (m ²)	0.70	SIDEWALL SURFACE AREA (m ²)	3.42	a(p50) Internal Surface Area @ 50% Effective Depth (m ²)	2.41		
75% Effective Water Depth (m)	0.45	25% Effective Water Depth (m)	0.15	V(p75-25) Volume of Hole Between 75 & 25% Effective Water Depth (m ³)	0.21		
t(p75) Time for Water Level to Drain to 75% Effective Depth (mins)	7	t(p25) Time for Water Level to Drain to 25% Effective Depth (mins)	19	t(p75-25) Time for Water Level to Drain from 75to 25% Effective Depth (mins)	12		
SOIL INFILTRATION RATE	1.21E-04			m/sec			
24 Hr Clock Time hh:mm	Time Elapsed (mins)	Depth of Water in Pit (m)					
10:30	0	0.600					
10:31	1	0.580					
10:32	2	0.555					
10:33	3	0.537					
10:34	4	0.515					
10:35	5	0.493					
10:36	6	0.478					
10:37	7	0.452					
10:38	8	0.425					
10:39	9	0.390					
10:40	10	0.345					
10:42	12	0.300					
10:44	14	0.260					
10:46	16	0.222					
10:48	18	0.188					
10:50	20	0.124					
10:55	25	0.078					
11:00	30	0.000					
			<img alt="A photograph of a soil infiltration test setup. A blue cylindrical container sits in a hole in the ground, surrounded by soil. A				

BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.90	SOIL TYPE	See TP Log	TP17

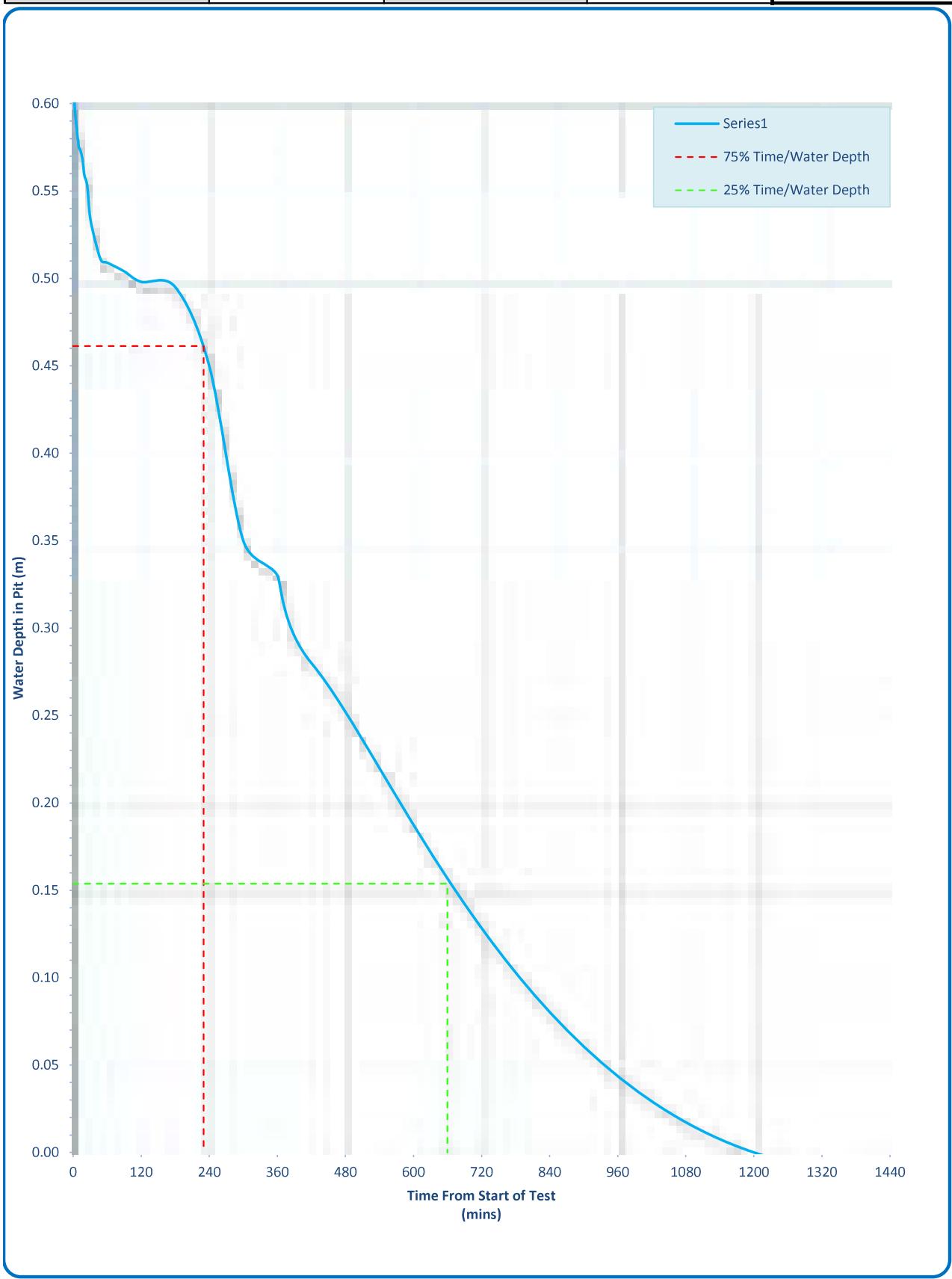


BRE 365 SOIL INFILTRATION TEST



BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.90	SOIL TYPE	See TP Log	TP18



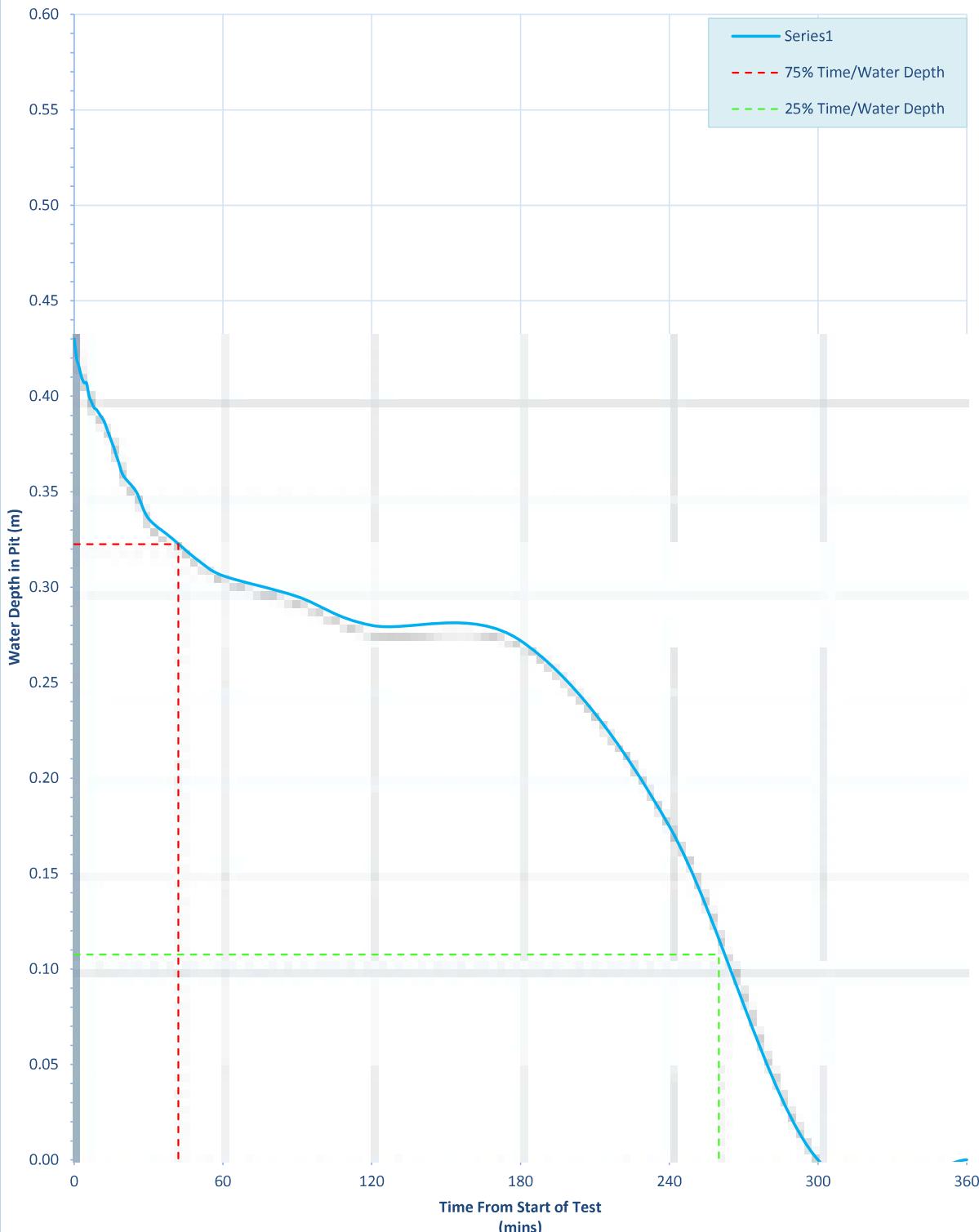
BRE 365 SOIL INFILTRATION TEST



JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.	TP19
INFILTRATION TEST No.	1	SOIL TYPE	See TP Log	WEATHER CONDITIONS	DRY
TEST PIT WIDTH (m)	0.50	TEST PIT LENGTH (m)	1.10	TEST PIT DEPTH (m)	0.60
WATER SURFACE LEVEL (m)	0.17	GROUNDWATER DEPTH (m)	Dry	HEAD OF WATER IN PIT (m)	0.43
BASE SURFACE AREA (m ²)	0.55	SIDEWALL SURFACE AREA (m ²)	1.92	a(p50) Internal Surface Area @ 50% Effective Depth (m ²)	1.51
75% Effective Water Depth (m)	0.3225	25% Effective Water Depth (m)	0.1075	V(p75-25) Volume of Hole Between 75 & 25% Effective Water Depth (m ³)	0.11825
t(p75) Time for Water Level to Drain to 75% Effective Depth (mins)	42	t(p25) Time for Water Level to Drain to 25% Effective Depth (mins)	260	t(p75-25) Time for Water Level to Drain from 75to 25% Effective Depth (mins)	218
SOIL INFILTRATION RATE	5.99E-06				m/sec
24 Hr Clock Time hh:mm	Time Elapsed (mins)	Depth of Water in Pit (m)			
10:30	0	0.430			
10:31	1	0.420			
10:32	2	0.415			
10:33	3	0.410			
10:34	4	0.407			
10:35	5	0.407			
10:36	6	0.400			
10:37	7	0.397			
10:38	8	0.394			
10:39	9	0.393			
10:40	10	0.391			
10:42	12	0.387			
10:44	14	0.380			
10:46	16	0.373			
10:48	18	0.365			
10:50	20	0.358			
10:55	25	0.350			
11:00	30	0.336			
11:10	40	0.325			
11:20	50	0.314			
11:30	60	0.306			
12:00	90	0.295			
12:30	120	0.280			
13:30	180	0.272			
14:30	240	0.175			
15:30	300	0.000			
16:30	360	0.000			
	</td				

BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	0.60	SOIL TYPE	See TP Log	TP19



BRE 365 SOIL INFILTRATION TEST



BRE 365 SOIL INFILTRATION TEST

JOB No.	23-3170	SITE	Calmount Drive, Dublin	TRIAL PIT No.
TEST PIT DEPTH (m)	1.00	SOIL TYPE	See TP Log	TP20

