

Proposed Surface Water Attenuation Overview

Unit 1, M50 Business Park

Client: Creighton Properties LLC

Date: 4th April 2023

Job Number: 22_112

Civil Engineering Structural

Transport

Environmental Project

Project Management Health and Safety



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Proposed Surface Water Attenuation Overview

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Project: Unit 1, M50 Business Park





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1 Introduction

1.1 Background

This Proposed Surface Water Attenuation Overview report has been prepared by Clifton Scannell Emerson Associates (CSEA) on behalf of Creighton Properties LLC in response to Further Information Request No. 3 (E) as issued by South Dublin County Council in response to application for planning permission submitted for development at Unit 1, M50 Business Park, Ballymount, Dublin 12 (Reg Ref SD22A/0460).

1.2 Overview

This Proposed Surface Water Attenuation Overview report is to be read in conjunction with the RPT-22_112-004 SuDS Management Plan report. In this report the areas and runoff coefficients of different surface types are defined. Surface water attenuation is calculated to ensure that the Greenfield runoff rate for the site is maintained at the outfall manhole during the 1 in 100 year critical storm event, inclusive of the climate change allowance.

1.3 Existing Site

The existing site is located in the Urban Fringe/Periurban area of the Green Infrastructure (GI) network of the County. Although the site is not partially or wholly within the Riparian Corridors, urbanisation disrupts the land-water linkages. Surface water runoff from existing hardstanding areas are collected in a sealed system of pipes and gullies and outfalls via a bypass petrol interceptor to the existing M50 Business Park drainage network. There is no existing provision for surface water attenuation thus increasing flood risk within the site and is likely to increase flood risk elsewhere during critical storm events.

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2 Determination of Greenfield Runoff Rate

The allowable discharge rate, Q_{BAR}, is given by the following equation in accordance with the Institute of Hydrology Report No. 124 (IH 124 method):

$$Q_{BAR} = 0.00108AREA^{0.89}SAAR^{1.17}SOIL^{2.17}$$

However, the total site area is less than 50 hectares. Therefore, Q_{BAR} is calculated for 50 hectares and linearly interpolated to 0.86 hectares. See calculations below.

IH 124 method for 50 hectare site area:

AREA = 0.5 km^2 (i.e. 50 ha)

SAAR = 700 mm (Met Eireann SAAR, see Appendix D)

SOIL = 0.3 (SOIL TYPE 2, see Table D1 of Appendix D of Volume 2 of GDSDS)

 $Q_{BAR} = 0.00108(0.5)^{0.89}(700)^{1.17}(0.3)^{2.17}$

= 0.09 m³/s for 50 ha site area

Interpolation for 0.86 hectares:

 $Q_{BAR} = (0.09 \text{ m}^3/\text{s} / 50 \text{ ha}) \times 0.86 \text{ ha}$

 $= 0.002 \text{ m}^3/\text{s}$

Therefore, QBAR = 1.57 l/s.

Check whichever is greater for the maximum discharge rate of Q_{bar} or 2 l/s/ha in accordance with Criterion 4.3 of Table 6.3 of Volume 2 the GDSDS.

 $Q_{BAR} = 1.57 \text{ l/s}$

 $2 \frac{1}{s}$ = 1.73 $\frac{1}{s}$ for 0.86 ha site

Therefore, the maximum allowable discharge for the site is **1.73 I/s** at a design head of **2.0m**. Discharge from the site will be controlled by means of an online hydrobrake vortex control (Unit Reference SHE-0053-1730-2000-1730). Details of the hydrobrake proposed are provided in **Appendix A**.

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3 Coefficients of Runoff for Contributing Impermeable Areas

The proposed development contains the following impermeable areas:

Roof Area (A_{RF}) = 0.236 ha Green Roof Area (A_{GRF}) = 0.004 ha Concrete Area (A_{CONC}) = 0.216 ha Gravel Area (A_{GRAV}) = 0.028 ha Grasscrete Area (A_{GCRETE}) = 0.147 ha

Section 8.4.4.1 of the 'SDCC SuDS explanatory design and evaluation guide' states that the runoff co-efficient of 0.95 for roofs and 0.9 for paved areas would be accepted by SDCC where no more detailed assessment is undertaken and notes that the designer must evaluate the runoff coefficient for the types of surfaces contributing to the storage location. As there are a number of other surfaces with varying co-efficient of runoff contributing to the design of the attenuation system CSEA have undertaken a review of best practice in relation to co-efficient of run-off for various surfaces and have located detailed guidance for same in Table 9 of the German standard DIN 1986-100:2016-12 (refer to **Appendix B**, note text is in German). The run-off co-efficients adopted are outlined below:

 $\begin{array}{ll} \mbox{Roof Coefficients of Runoff } (\mbox{$C_{\rm RF}$}) & = 0.95 \\ \mbox{Green Roof Coefficients of Runoff } (\mbox{$C_{\rm GRF}$}) & = 0.40 \\ \mbox{Concrete Coefficients of Runoff } (\mbox{$C_{\rm CONC}$}) & = 0.90 \\ \mbox{Gravel Coefficients of Runoff } (\mbox{$C_{\rm GRAV}$}) & = 0.70 \\ \mbox{Grasscrete Coefficients of Runoff } (\mbox{$C_{\rm GCRETE}$}) & = 0.30 \\ \end{array}$

Therefore, total impermeable are for the site is calculated as follows:

Total Impermeable Area =
$$A_{RF} \times C_{RF} + A_{GRF} \times C_{GRF} + A_{CONC} \times C_{CONC} + A_{GRAV} \times C_{GRAV} + A_{GCRETE} \times C_{GCRETE}$$

= $0.236 \times 0.95 + 0.004 \times 0.40 + 0.216 \times 0.90 + 0.028 \times 0.70 + 0.147 \times 0.30$
= 0.484 ha

Refer to **Appendix C** for the drawing showing the different surface types, area and respective runoff coefficients.

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4 Required Surface Water Attenuation Storage

In order to account for climate change, an additional allowance of 20% in rainfall intensities have been allowed as per Section 8.4.6.4 of SDDCC Sustainable Drainage Explanatory Design & Evaluation Guide which exceeds the requirements of Table 6.1 of Volume 2 of the GDSDS (10%).

Analysis of the 1 in 30 year storm event yields a critical required storage volume of 357.607 m³ during the critical 1440 minute storm event. Similarly, analysis of the 1 in 100 year storm event yields a critical required storage volume of 532.583 m³ during the 1440 minute storm event. See **Appendix D** for analysis the 1 in 30 and 1 in 100 year storm event.

As a result, the required surface water storage is **532.583** m³ during the critical 1440 minute of the 1 in 100 year storm event.

Considering the site constraints and underground service congestion, 3 no. StormTech $^{\text{TM}}$ systems by Cubic M^3 or similar is being proposed. These systems have been modified to use storage volume within the gravel media rather than tanked storage where possible. See **Appendix E** for further details.



5 Surface Water Network Flooding Check for Critical Storm Event

The critical storm event occurs during the 1440 minute of the 1 in 100 year storm event for which $532.583 \, \text{m}^3$ of surface water attenuation storage is required. During this storm event the Top Water Level (TWL) = $66.60 \, \text{m}$ in the surface water network.

As a result, the surface water volume of 532.583 m³ is stored in the network as follows:

- Attenuation A1
- Cover Level (CL) = 67.47 m
 Invert Level (IL) = 64.88 m
 Plan Area = 96.55 m²
 Top of Attenuation System level = 66.56 m
 Top Water Level (TWL) during Critical Storm = 66.56 m
- Storage Volume Contribution during Critical Storm = 75 m³ (100 % of Capacity)
- Attenuation A2 (Inclusive of additional 127 m³ Porous Stone)
- Cover Level (CL) = 67.52 m
 Invert Level (IL) = 64.68 m
 Plan Area = 357.77 m²
 Top of Attenuation System level = 66.48 m
 Top Water Level (TWL) during Critical Storm = 66.48 m
- Storage Volume Contribution during Critical Storm = 300 m³ (103 % of Capacity)
- Attenuation A3
- Cover Level (CL) = 66.61 m
 Invert Level (IL) = 65.03 m
 Attenuation System Plan Area = 169.85 m²
 Top of Attenuation System level = 66.09 m
 Top Water Level (TWL) during Critical Storm = 66.09 m
- Storage Volume Contribution during Critical Storm = 105 m³ (100 % of Capacity)
- Manhole Storage
 - Top Water Level (TWL) during Critical Storm = 66.60 m
- Storage Volume Contribution during Critical Storm = 34.965 m³ (53 % of Capacity)
- Pipes Storage
 - Top Water Level (TWL) during Critical Storm = 66.19 m
- Storage Volume Contribution during Critical Storm = 17.618 m³ (92 % of Capacity)
- Total Provided Storage (during Critical Storm) = Attenuation A1 + Attenuation A2 + Attenuation A3 + Manhole Storage + Pipe Storage
 = 75 + 300 + 105 + 34.965 + 17.618
 = 532.583 m³

As the proposed drainage system, inclusive of the attenuation systems provided as outlined above, has greater capacity that the estimated storage volume required during the critical 1440 minute during the 1 in 100 year storm event it can be concluded that the site will not be subject to flooding during the critical storm period.

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Refer to **Appendix G** for the drawing showing surface water attenuation capacity during 1440 minute of 1 in 100 year critical storm event. Refer to **Appendix H** for the drawing demonstrating the SuDS treatment train and proposed source and site controls.

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6 Conclusion

This report provides a comprehensive response to Additional Information Request 3 in respect of the Planning Application for the above scheme (Reg Ref SD22A/0460). As described in the report surface water attenuation has been provided such that there is sufficient storage during the 1440 minute of the 1 in 100 year critical storm, inclusive of the provision for the 20% climate change allowance to ensure improved resilience against future shocks and disruptions. A hydrobrake has been provisioned to ensure that the site outfalls to the Greenfield runoff rate.

Attenuated surface water runoff means that flood risk within the proposed development is reduced and the likelihood of flood risk occurring downstream of the proposed development during critical storm events will be decreased due to the significant reduction in surface water discharge from the site.

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Appendix A - Flow Control Device Details

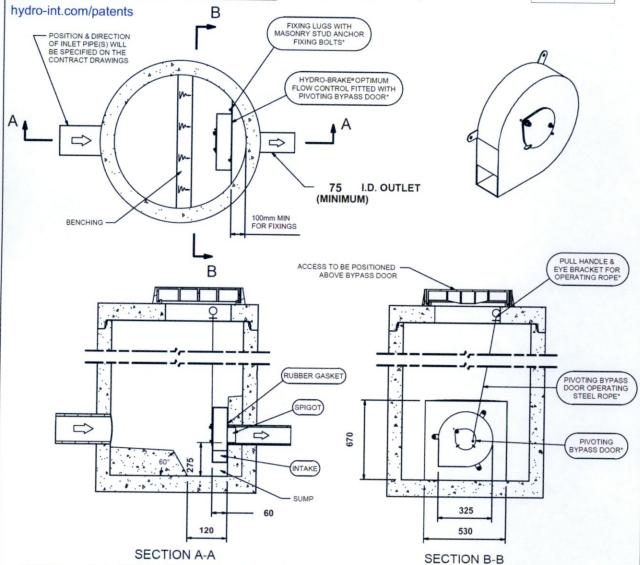
Technical Specification Control Point Head (m) Flow (I/s) Primary Design 2.000 1.730 Flush-Flo™ 0.233 1.105 Kick-Flo® 0.473 0.907 Mean Flow 1.271

Hydro-Brake* Optimum Flow Control including:

- grade 304L stainless steel Integral stainless steel pivoting by-pass door allowing clear line of sight through to outlet, c/w stainless steel operating rope
- Beed blasted finish to maximise corrosion resistance
- Stainless steel fixings
- Rubber gasket to seal outlet
- Indicative Weight: 49 kg







IMPORTANT:

> LIMIT OF HYDRO INTERNATIONAL SUPPLY

LIMIT OF HYDRO INTERNATIONAL SUPPLY
THE DEVICE WILL BE HANDED TO SUIT SITE CONDITIONS
FOR SITE SPECIFIC DETAILS AND MINIMUM CHAMBER SIZE REFER TO HYDRO INTERNATIONAL
ALL CIVIL AND INSTALLATION WORK BY OTHERS

*WHERE SUPPLIED

*WHERE SUPPLIED

HYDRO-BRAKE* FLOW CONTROL & HYDRO-BRAKE* OPTIMUM FLOW CONTROL ARE REGISTERED TRADEMARKS FOR FLOW

CONTROLS DESIGNED AND MANUFACTURED EXCLUSIVELY BY HYDRO INTERNATIONAL

THIS DESIGN LAYOUT IS FOR ILLUSTRATIVE PURPOSES ONLY. NOT TO SCALE.

Hydro-Brake®Optimum Flow Control are unique. Dynamic hydraulic modelling **ADVICE** evaluates the full head/flow characteristic curve. The use of any other flow control will invalidate any design based on this data and could constitute a flood risk. DATE 30/08/2022 09:26 SITE

The head/flow characteristics of this SHE-0053-1730-2000-1730

Unit 1, M50 Business Park Kyle Brill 22 112

International 4

SHE-0053-1730-2000-1730 Hydro-Brake® Optimum

© 2022 Hydro International Ltd, Shearwater House, Clevedon Hall Estate, Victoria Road, Clevedon, BS21 7RD. Tel; 01275 878371 Fax; 01275 874979 Web; www.hydro-int.com Email; enquiries@hydro-int.com

DESIGNER

REF

DESIGN

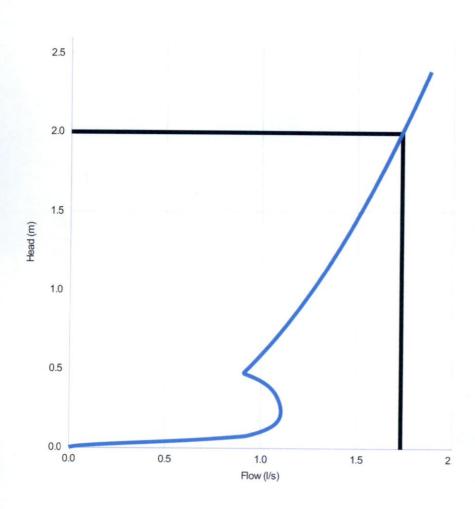
Technical Specification				
Control Point	Head (m)	Flow (l/s)		
Primary Design	2.000	1.730		
Flush-Flo	0.233	1.105		
Kick-Flo®	0.473	0.907		
Mean Flow		1.271		





PT/329/0412

hydro-int.com/patents



Head (m)	Flow (I/s)
0.000	0.000
0.069	0.839
0.138	1.057
0.207	1.103
0.276	1.100
0.345	1.075
0.414	1.016
0.483	0.915
0.552	0.970
0.621	1.022
0.690	1.071
0.759	1.117
0.828	1.161
0.897	1.204
0.966	1.244
1.034	1.283
1.103	1.321
1.172	1.358
1.241	1.393
1.310	1.427
1.379	1.461
1.448	1.493
1.517	1.525
1.586	1.556
1.655	1.586
1.724	1.616
1.793	1.645
1.862	1.674
1.931	1.702
2.000	1.729

	DESIGN ADVICE The head/flow characteristics of this SHE-0053-1730-2000-1730 Hydro-Brake Optimum® Flow Control are unique. Dynamic hydraulic modelling evaluates the full head/flow characteristic curve. The use of any other flow control will invalidate any design based on this data		Hydro S			
	DATE	and could constitute a flood risk. 30/08/2022 09:26				
1	Site	Unit 1, M50 Business Park	SHE-0053-1730-2000-1730			
Γ	DESIGNER	Kyle Brill	Under Brake Ontino			
	Ref	22_112	Hydro-Brake Optimum®			
L	© 2018 Hydro International, Shearwater House, Clevedon Hall Estate, Victoria Road, Clevedon, BS21 7RD. Tel 01275 878371 Fax 01275 874979 Web www.hydro-int.com Email designtcols@hydro-int.com					

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Appendix B Table 9 of DIN 1986-100:2016-12 (German Standard)

14.2.3 Abflussbeiwerte

Tabelle 9 — Abflussbeiwerte $\mathcal C$ zur Ermittlung des Regenwasserabflusses

Nr.	Art der Flächen	Spitzen- abflussbei- wert	Mittlerer Abflussbeiwert ^c	
	Die Abflussbeiwerte beziehen sich ausschließlich auf Flächen, die	Cs	$C_{ m m}$	
	potentiell einen Abfluss zum Entwässerungssystem haben.	O _S	Berechnung von	
			$V_{ m RRR}$	
1	Wasserundurchlässige Flächen, z. B.			
	Dachflächen			
	— Schrägdach			
	— Metall, Glas, Schiefer, Faserzement	1,0	0,9	
	— Ziegel, Abdichtungsbahnen	1,0	0,8	
	— Flachdach (Neigung bis 3° oder etwa 5 %			
	— Metall, Glas, Faserzement	1,0	0,9	
	— Abdichtungsbahnen	1,0	0,9	
	— Kiesschüttung	0,8	0,8	
	— Begrünte Dachflächen ^a			
	— Extensivbegrünung (> 5°)	0,7	0,4	
	 — Intensivbegrünung, ab 30 cm Aufbaudicke (≤ 5°) 	0,2	0,1	
	 Extensivbegrünung, ab 10 cm Aufbaudicke (≤ 5°) 	0,4	0,2	
	— Extensivbegrünung, unter 10 cm Aufbaudicke (≤ 5°)	0,5	0,3	
	Verkehrsflächen (Straßen, Plätze, Zufahrten, Wege)			
	— Betonflächen	1,0	0,9	
	— Schwarzdecken (Asphalt)	1,0	0,9	
	— befestigte Flächen mit Fugendichtung, z.B. Pflaster mit Fugenverguss	1,0	0,8	
	Rampen			
	— Neigung zum Gebäude, unabhängig von der Neigung und der	1,0	1,0	
	Befestigungsart			
2	Teildurchlässige und schwach ableitende Flächen,			
	z. B. Verkehrsflächen (Straßen, Plätze, Zufahrten, Wege)			
	— Betonsteinpflaster, in Sand oder Schlacke verlegt, Flächen mit Platten	0,9	0,7	
	— Pflasterflächen, mit Fugenanteil > 15 %, z. B. 10 cm × 10 cm und	0,7	0,6	
	kleiner oder fester Kiesbelag			
	— wassergebundene Flächen	0,9	0,7	
	— lockerer Kiesbelag, Schotterrasen, z. B. Kinderspielplätze	0,3	0,2	
	Verbundsteine mit Sickerfugen, Sicker-/Drainsteine	0,4	0,25	
	— Rasengittersteine (mit häufigen Verkehrsbelastungen,	0,4	0,2	
	z. B. Parkplatz)			
	Rasengittersteine (ohne häufige Verkehrsbelastungen,	0,2	0,1	
	z. B. Feuerwehrzufahrt)			
	Sportflächen mit Dränung			
	— Kunststoff-Flächen, Kunststoffrasen	0,6	0,5	
	— Tennenflächen	0,3	0,2	
	— Rasenflächen	0,2	0,1	
3	Parkanlagen, Rasenflächen, Gärten	The state of the s		
	— flaches Gelände	0,2 ^b	0,1	
	— steiles Gelände	0,3 ^b	0,2	

Siehe auch [7] für die Planung, Ausführung und Pflege von Dachbegrünungen, die dort genannten Werte sind $C_{\rm s}$ -Werte

b Bei diesen Flächen ist für den Überflutungsnachweis ein möglicher höherer Abflussbeitrag je nach örtlichen Gegebenheiten (z. B. Gefälle, Boden, Vegetation) zu prüfen.

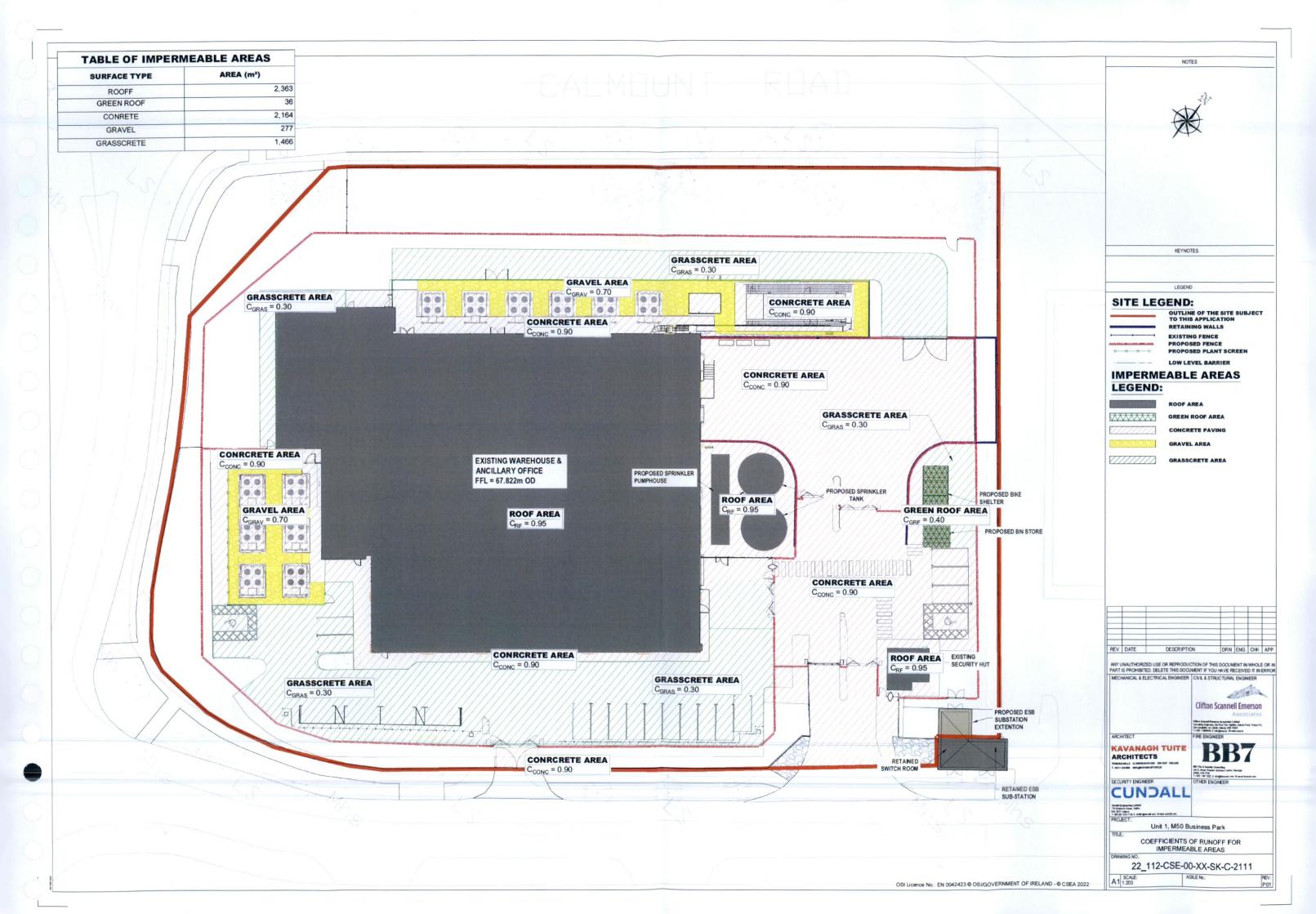
Aufgrund der Anwendung einer einheitlichen Wiederkehrzeit (T = 2 a) und des begrenzten Anwendungsspektrums für die Bemessung von V_{RRR} wird hier jeweils nur ein Wert für C_m genannt. Die in den DWA-Regelwerken genannten Wertespektren beziehen sich auf unterschiedliche Wiederkehrzeiten und Planungssituationen.

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Appendix C Surface Types, Areas and Runoff Coefficients



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Appendix D Surface Water Attenuation Storage Critical Storm Events

Surface Water Attenuation Requirement for 1 in 30 Year Storm Event

Total Site Area =

Total Impermeable Area =

PIMP =

0.86 hectares (ha) 0.484 hectares (ha)

56.02 %

(See Section 3)

Duration		Rainfall		1-1	Total	Inflow Rate	Inflow	Inflow Rate	Ouflow	Required	
	30 Year Event (mm)	+20% CC Allowance	Rainfall (mm)	Intensity (mm/hr)	Impermeable Area (ha)	$Q = 2.78*C*I*A^{1}$ (I/s)	Volume, I (m³)	Q _{BAR} (I/s)	Volume, O (m³)	Storage, S (m ³)	Comments
5	12.1	1.2	14.52	174.24	0.484	234.46	70.339	1.728	0.518		
10	16.9	1.2	20.28	121.68	0.484	163.74	98.242	1.728	1.037	97.205	
15	19.8	1.2	23.76	95.04	0.484	127.89	115.100	1.728	1.555	113.545	
30	24.8	1.2	29.76	59.52	0.484	80.09	144.166	1.728	3.110	141.056	
60	31.1	1.2	37.32	37.32	0.484	50.22	180.789	1.728	6.221	174.568	
120	38.9	1.2	46.68	23.34	0.484	31.41	226.131	1.728	12.442	213.690	
180	44.4	1.2	53.28	17.76	0.484	23.90	258.104	1.728	18.662	239.441	
240	48.8	1.2	58.56	14.64	0.484	19.70	283.681	1.728	24.883	258.798	
360	55.6	1.2	66.72	11.12	0.484	14.96	323.211	1.728	37.325	285.886	
540	63.5	1.2	76.2	8.47	0.484	11.39	369.135	1.728	55.987	313.147	
720	69.7	1.2	83.64	6.97	0.484	9.38	405.176	1.728	74.650	330.527	
1080	79.5	1.2	95.4	5.30	0.484	7.13	462.145	1.728	111.974	350.171	
1440	87.2	1.2	104.64	4.36	0.484	5.87	506.906	1.728	149.299	357.607	Critical Volume
2880	98.9	1.2	118.68	2.47	0.484	3.33	574.920	1.728	298.598	276.322	

Notes:

- 1. See Appendix F for Met Eireaan rainfall data during 1 in 30 year storm event
- **2.** $Q = 2.78 * C*I*A = 2.78 * I*(C_{RF}*A_{RF}+C_{GRF}*A_{GRF}+C_{CONC}*A_{CONC}+C_{GRAV}*A_{GRAV}+C_{GRAS}*A_{GRAS})$

Surface Water Attenuation Requirement for 1 in 100 Year Storm Event

Total Site Area =

Total Impermeable Area =

PIMP =

0.86 hectares (ha) 0.484 hectares (ha)

(See Section 3)

56.02 %

Duration		Rainfall			Total	Inflow Rate	Inflow	Inflow Rate	Ouflow	Required	
	100 Year Event (mm)	+20% CC Allowance	Rainfall (mm)	Intensity (mm/hr)	Impermeable Area (ha)	Q = 2.78*C*I*A ¹ (I/s)	Volume, I (m³)	Q _{BAR} (I/s)	Volume, O (m³)		Comments
5	17.7	1.2	21.24	254.88	0.484						
10	24.6	1.2	29.52	177.12	0.484						
15	29.0	1.2	34.8	139.20	0.484	187.31	168.581	1.728			
30	35.8	1.2	42.96	85.92	0.484	115.62	208.111	1.728			
60	44.3	1.2	53.16	53.16	0.484	71.53	257.522	1.728		251.301	
120	54.8	1.2	65.76	32.88	0.484	44.24	318.560	1.728	12.442	306.119	
180	62.0	1.2	74.4	24.80	0.484	33.37	360.415	1.728	18.662	341.753	
240	67.8	1.2	81.36	20.34	0.484	27.37	394.131	1.728	24.883	369.248	
360	76.7	1.2	92.04	15.34	0.484	20.64	445.868	1.728	37.325	408.543	
540	86.9	1.2	104.28	11.59	0.484	15.59	505.162	1.728	55.987	449.175	
720	94.9	1.2	113.88	9.49	0.484	12.77	551.667	1.728	74.650	477.018	
1080	107.4	1.2	128.88	7.16	0.484	9.63	624.332	1.728	111.974	512.357	
1440	117.3	1.2	140.76	5.87	0.484	7.89	681.882	1.728	149.299	532.583	Critical Volum
2880	129.9	1.2	155.88	3.25	0.484	4.37	755.127	1.728	298.598	456.529	

Notes:

- 1. See Appendix F for Met Eireaan rainfall data during 1 in 100 year storm event
- 2. $Q = 2.78 * C*I*A = 2.78*I*(C_{RF}*A_{RF}+C_{GRF}*A_{GRF}+C_{CONC}*A_{CONC}+C_{GRAV}*A_{GRAV}+C_{GRAS}*A_{GRAS})$

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Appendix E Attenuation Sizing Calculations

PROJECT REF: 22_112 LOCATION: Calmount Road - A1 DATE: 22/08/2022 CREATED BY: Kyle Brill

SYSTEM PARAMETERS

Required Total Storage	75 m ³
Stormtech chamber model	MC3500
Number of Isolator Rows for TSS Removal	1

SITE PARAMETERS

Maximum Width at Excavation Base	5 m
Stone Porosity	43%
Excavation Batter Angle (degrees)	60°
Stone Below Chambers	0.23 m
Stone Above Chambers	0.305 m
Additional Storage. E.g manholes, pipe	0 m ³

CALCULATED CHAMBER SYSTEM DIMENSIONS Calculated Adopted Number of Rows Number of units per Row ea Number of MC3500 Chambers ea Number of MC3500 Endcaps ea System Installed Storage Depth (effective storage depth) 1.680 Tank overall installed Width at base 4.74 Tank overall installed Length at Base 12.64 Total Effective System Storage 75.6 75.4

Minimum Requirement

0.23 0.30 Instructions: Fill in blue highlighted cells

Set width to maximum allowance

Adjust site parameters and system dimension until volume achieved For Rectangular systems only, for irregular shape dig contact Microstrain

STORMTECH SYSTEM DETAIL

StormTech Chamber Model	MC3500
Unit Width	1.955 m
Unit Length	2.18 m
Unit Height	1.145 m
Min Cover Over System	0.3 m
Max Cover Over Chamber	2.4 m
Internal Storage Vol. (Chamber only)	3.11 m

STONE AND EXCAVATION DETAIL

Volume of Dig for System	132
Area of Dig at Base of System	60 m ²
Area of Dig at Top of System	97 m ²
Void Ratio	57%
Stone Requirement - tonne	159 tonne



PROJECT REF: 22_112 LOCATION: Calmount Road - A2 DATE: 22/08/2022 CREATED BY: Kyle Brill

SYSTEM PARAMETERS

Required Total Storage	276 m ³
Stormtech chamber model	MC3500
Number of Isolator Rows for TSS Removal	1

SITE PARAMETERS

Maximum Width at Excavation Base	3.2 m	
Stone Porosity	43%	
Excavation Batter Angle (degrees)	60 °	Minimum Requirement
Stone Below Chambers	0.23 m	0.23
Stone Above Chambers	0.425 m	0.30
Additional Storage. E.g manholes, pipe	126.7812 m ³	

CALCULATED CHAMBER SYSTEM DIMENSIONS	Calculated	Adopted
Number of Rows	1	ea
Number of units per Row	18	ea
Number of MC3500 Chambers	18	ea
Number of MC3500 Endcaps	2	ea
System Installed Storage Depth (effective storage depth)	1.800	m
Tank overall installed Width at base	2.56	3.2 m
Tank overall installed Length at Base	40.98	42 m
Total Effective System Storage	276.5	300.8 m ³

Instructions: Fill in blue highlighted cells

Set width to maximum allowance

Adjust site parameters and system dimension until volume achieved

For Rectangular systems only, for irregular shape dig contact Microstrain

STORMTECH SYSTEM DETAIL

StormTech Chamber Model	MC3500
Unit Width	1.955 m
Unit Length	2.18 m
Unit Height	1.145 m
Min Cover Over System	0.3 m
Max Cover Over Chamber	2.4 m
Internal Storage Vol. (Chamber only)	3.11 m

STONE AND EXCAVATION DETAIL

Volume of Dig for System	330
Area of Dig at Base of System	134 m ²
Area of Dig at Top of System	233 m ²
Void Ratio	91%
Stone Requirement - tonne	445 tonne



PROJECT REF: 22_112 LOCATION: Calmount Road - A3 DATE: 22/08/2022 CREATED BY: Kyle Brill

SYSTEM PARAMETERS

Required Total Storage	105 m
Stormtech chamber model	SC740
Number of Isolator Rows for TSS Removal	1

SITE PARAMETERS

Maximum Width at Excavation Base	9.5 m	
Stone Porosity	43%	
Excavation Batter Angle (degrees)	60 °	Minimum Requirement
Stone Below Chambers	0.15 m	0.15
Stone Above Chambers	0.15 m	0.15
Additional Storage. E.g manholes, pipe	0 m ³	

CALCULATED CHAMBER SYSTEM DIMENSIONS	Calculated	Adopted
Number of Rows	6	ea
Number of units per Row	7	ea
Number of SC740 Chambers	42	ea
Number of SC740 Endcaps	12	ea
System Installed Storage Depth (effective storage depth)	1.060	m
Tank overall installed Width at base	9.12	9.5 m
Tank overall installed Length at Base	15.89	15.4 m
Total Effective System Storage	105.2	105.8 m ³

Instructions: Fill in blue highlighted cells

Set width to maximum allowance

Adjust site parameters and system dimension until volume achieved For Rectangular systems only, for irregular shape dig contact Microstrain

STORMTECH SYSTEM DETAIL

StormTech Chamber Model	SC740
Unit Width	1.295 n
Unit Length	2.17 n
Unit Height	0.76 n
Min Cover Over System	0.3 m
Max Cover Over Chamber	2.4 m
Internal Storage Vol. (Chamber only)	1.3 m

STONE AND EXCAVATION DETAIL

Volume of Dig for System	172
Area of Dig at Base of System	146 m ²
Area of Dig at Top of System	178 m ²
Void Ratio	61%
Stone Requirement - tonne	191 tonn



Project: Unit 1, M50 Business Park

Title: Proposed Surface Water Attenuation Overview Report



Appendix F Met Éireann

MET ÉIREANN RAINFALL DATA

1981-2010 Annual Average Rainfall Grid:

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Eastin and Northing Irish Grid Co-ordinates east north Annual Average Rainfall(mm) 310000 227000 824 310000 228000 763 310000 229000 721 310000 230000 700 310000 231000 702 310000 232000 718 310000 233000 733 310000 234000 746
```

Return Period Rainfall depths for Sliding Durations:

Met Eireann Return Period Rainfall Depths for sliding Durations Irish Grid: Easting: 309895, Northing: 230126,

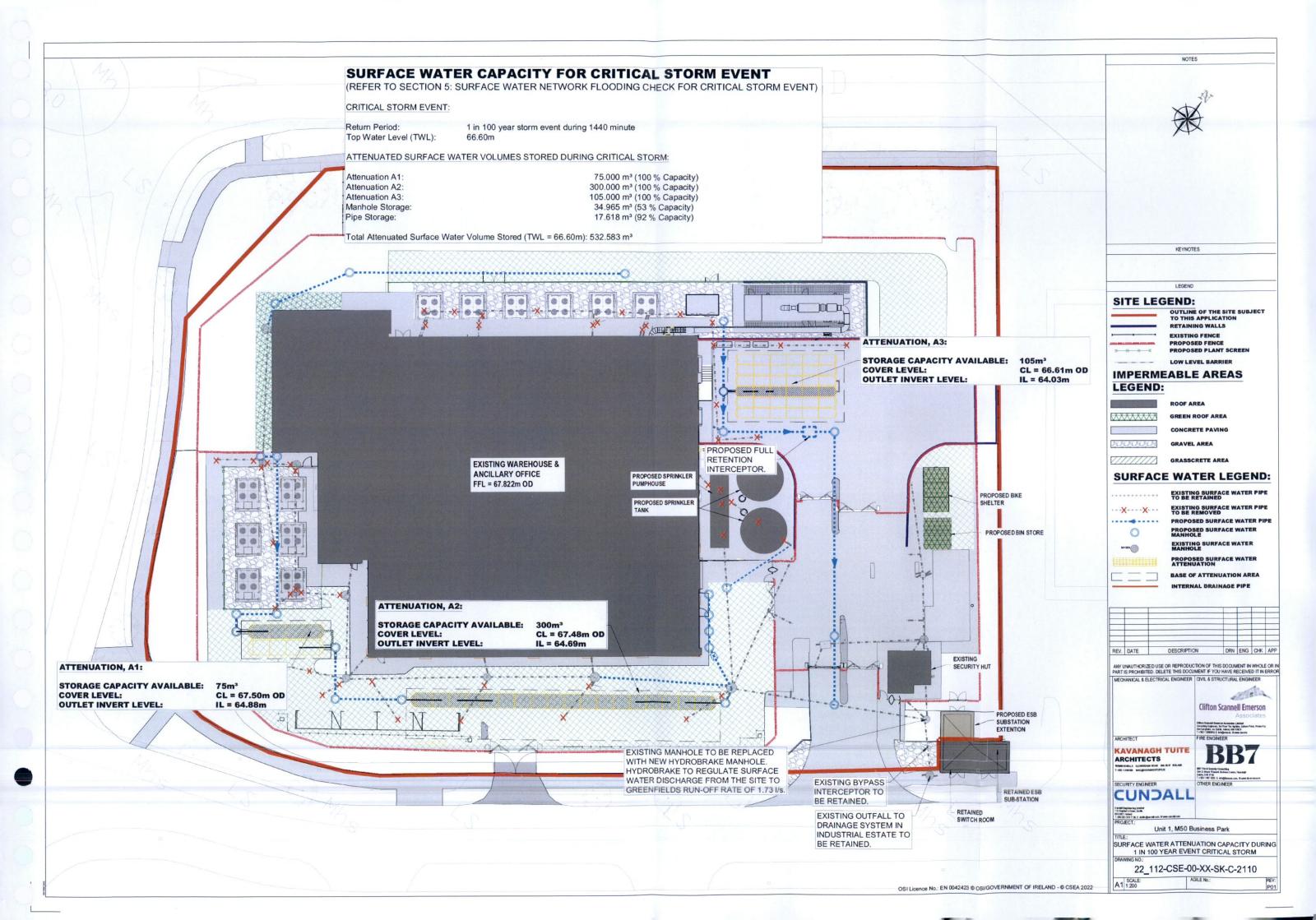
	Inte	rval	1					Years								
DURATION	6months,	lyear,	2,	3,	4,	5,	10,	20,	30,	50,	75,	100,	150,	200,	250,	500,
5 mins	2.4,	3.6,	4.3,	5.3,	6.0,	6.6,	8.4,	10.6,	12.1,	14.2,			20.1.	21.9.	23.5.	N/A
10 mins	3.4,	5.0,	5.9,	7.4,	8.4,	9.1,	11.7,	14.8,	16.9,	19.8,	22.5,	24.6,	28.0,	30.6,	32.8,	N/A
15 mins	4.0,	5.9,	7.0,	8.7,	9.8,	10.7,	13.8,	17.4,	19.8,	23.3,	26.5,	29.0,	32.9,	36.0,	38.6,	N/A .
30 mins	5.2,	7.7,	9.1,	11.2,	12.6,	13.7,	17.5,	21.9,	24.8,	29.0,	32.9,	35.8,	40.5,	44.2.	47.2.	N/A
1 hours	6.9,	10.1,	11.8,	14.4,	16.2,	17.6,	22.2,	27.5,	31.1,	36.2,	40.7,	44.3,	49.9,	54.2,	57.8,	N/A,
2 hours	9.2,	13.1,	15.3,	18.5,	20.7,	22.4,	28.1,	34.6,	38.9,	45.1,	50.5,	54.8,	61.4,	66.5,	70.8,	N/A ,
3 hours	10.8,	15.3,	17.8,	21.5,	24.0,	25.9,	32.3,	39.6,	44.4,	51.2,	57.3,	62.0,	69.3,	75.0,	79.7,	N/A
4 hours		17.1,	19.8,	23.8,	26.6,	28.7,	35.6,	43.5,	48.8,	56.1,	62.7,	67.8,	75.6,	81.7,	86.7,	N/A
6 hours		20.0,	23.0,	27.6,	30.7,	33.1,	41.0,	49.8,	55.6,	63.8,	71.1,	76.7,	85.4,	92.1,	97.7,	N/A ,
9 hours	16.8,	23.3,	26.8,	32.0,	35.5,	38.2,	47.0,	57.0,	63.5,	72.6,	80.6,	86.9,	96.4,	103.8,	110.0,	N/A,
12 hours	18.8,		29.9,	35.6,	39.4,	42.3,	51.9,	62.6,	69.7,	79.5,	88.2,	94.9,	105.1,	113.1,	119.6,	N/A,
18 hours		30.4,	34.8,	41.2,	45.5,	48.9,	59.6,	71.6,	79.5,	90.4,	100.0,	107.4,	118.7,	127.5,	134.7,	N/A,
24 hours	24.9,	34.0,	38.7,	45.8,	50.5,	54.1,	65.8,	78.8,	87.2,	99.0,	109.3,	117.3,	129.4,	138.8,	146.5,	173.2,
2 days		41.4,	46.8,	54.6,	59.7,	63.7,	76.2,	90.0,	98.9,	111.1,	121.8,	129.9,	142.3,	151.7,	159.5,	186.2,
3 days		47.4,	53.2,													197.9,
4 days		52.7,	58.9,	67.8,	73.6,	78.1,	92.1,	107.2,	116.8,	130.0,	141.4,	150.0,	163.0,	172.9,	181.0,	208.5,
6 days	48.2,		68.6,							145.2,						
8 days	55.0,		77.2,													243.4,
10 days	61.2,		85.0,	96.2,	103.4,	108.9,	125.9,	143.9,	155.2,	170.4,	183.4,	193.3,	207.9,	219.0,	227.9,	258.1,
12 days	67.0,		92.2,	104.0,	111.6,	117.3,	135.1,	153.8,	165.6,	181.4,	194.9,	205.0,	220.1,	231.5,	240.7,	271.6,
16 days		96.3,	105.5,	118.3,	126.6,	132.8,	151.9,	172.0,	184.6,	201.4,	215.6,	226.3,	242.2,	254.2,	263.8,	296.1,
20 days		107.8,	117.7,	131.5,	140.3,	146.9,	167.3,	188.5,	201.7,	219.4,	234.4,	245.6,	262.2,	274.6,	284.7,	318.2,
25 days	99.4,	121.2,	131.8,	146.7,	156.1,	163.2,	184.9,	207.5,	221.5,	240.1,	255.9,	267.6,	285.0,	298.0,	308.5,	343.4,

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Appendix G Surface Water Attenuation Capacity During 1 in 100 Year Critical Storm Event



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Appendix H SuDS Management During Critical Storm Event

