

UNIT 6 FARBILL HOUSE, ATHLONE RD, KINNEGAD, CO. WESTMEATH.

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24th August 2022

South Dublin County Council Planning Department County Hall, Tallaght, Dublin 24, D24 A3XC

Planning Compliance

South Dublin County Council

Our Ref: 201-167

Planning Reference Number: SD22B/0075

Re: Planning Application @ Hillview, Athgoe Road, Newcastle, Co. Dublin, D22 N278.

**Applicant: Paul Begley** 

Dear Sir/Madam,

In the above regard, please find attached the prescribed documents in relation to condition number 2 of the granted planning application reference number SD22B/0075.

- 2 Number copies of Revised Site Layout Drawing showing soakaway details. (Drawing number 201-167-12-P1)
- 2 Number copies of BRE soakaway design report.

If you require anything further, please do not hesitate to contact the undersigned.

Yours sincerely,

Daniel McKeogh Daniel McKeogh



| \_/ | UNIT 6 FARBILL HOUSE, ATHLONE R | lD, |
|-----|---------------------------------|-----|
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# Soakaway Design

Property Address: Hillview, Athgoe Road, Newcastle, Co. Dublin, D22 N278

Report by: McK Consulting

Report Author: Billy Murtagh

#### Contents

### 1.0 Introduction

1.1 Background

### 2.0 Discussion

# 3.0 Method of Investigation

3.1.1 BRE Digest 365 Soakaway Testing

**4.0 Investigation Findings** *4.1.1 Soakaway Testing Inspection Findings* 

### 5.0 Conclusions

5.1 Calculations

# 6.0 Appendices

#### 1.0 Introduction

#### 1.1 Background

A planning application was lodged to South Dublin County Council for the construction of a new garage at Hillview, Athgoe Road, Newcastle, Co. Dublin, D22 N278.

The applicant's name is Paul Begley.

This report is the design calculations for the proposed on-site soakpit.

#### 2.0 Discussion

For the development, BRE Digest 365 soakaway testing has been carried out at the site.

Below are record photographs of the test hole at the site for the purposes of the BRE Digest 365 soakaway testing.

Figure 1-Test Hole Empty





Figure 2-Test Hole During Testing

# 3.0 Method of Investigation

# 3.1 BRE Digest 365 soakaway testing

Soakaway testing was carried out at the site in accordance with the requirements of BRE Digest 365.

#### 4.0 Investigation Findings

## 4.1 Soakaway Testing Findings

The testing was carried out on the 12th of July 2022.

The ground conditions encountered are suitable for the construction of a soakaway at the site.

Times for the test hole to empty from 75% full to 25% full:

Test Iteration 1 44 minutes
Test Iteration 2 50 minutes
Test Iteration 3 57 minutes

The testing was carried out, and water table was not encountered.

#### 5.0 Conclusion

#### 5.1 Calculations:

Based on the testing results, with a garage roof area of 98m<sup>2</sup> and allowing for a 20% increase in rainfall, it is proposed to install a 2.0m long x 2.0m wide x 2.0m deep soakaway below the invert of the incoming pipe.

We have attached the detailed calculations in the appendix below.

This report is for the information of the addressee only and may not be used by any third parties without the prior written consent of this company.

Signed:

Date: 24/08/2022

Prepared by: Billy Murtagh (BE CEng MIEI)

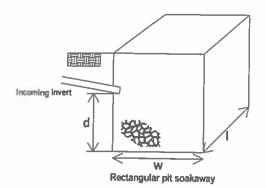
McK Consulting

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(Ph) 0449310287 Email: info@mckc.ie 6.0 Appendices

# **APPENDIX**

**CALCULATIONS** 



#### Soil infiltration rate (BRE digest 365)

;;;; Length of trial pit;  $I_{trial} = 1000 \text{ mm}$ ; Width of trial pit;  $b_{trial} = 1000 \text{ mm}$ ; Depth of trial pit (below invert);  $d_{trial} = 1000 \text{ mm}$ ; Free volume (if fill used);  $V_{trial} = 100 \text{ %}$ ;

75% depth of pit;  $d_{75} = (d_{trial} \times 0.75) = 750.00 \text{ mm}$ 50% depth of pit;  $d_{50} = (d_{trial} \times 0.50) = 500.00 \text{ mm}$ 25% depth of pit;  $d_{25} = (d_{trial} \times 0.25) = 250.00 \text{ mm}$ 

;;; Test 1 - time to fall from 75% depth to 25% depth; T1 = 126 min Test 2 - time to fall from 75% depth to 25% depth; T2 = 135 min Test 3 - time to fall from 75% depth to 25% depth; T3 = 143 min

Longest time to fall from 75% depth to 25% depth;  $t_{ij} = max(T1, T2, T3) = 143 min$ 

Storage volume from 75% to 25% depth;  $V_{p75\_25} = (I_{trial} \times b_{trial} \times (d_{75} - d_{25})) \times V_{trial} =$ 

0.50 m<sup>3</sup>

Internal surface area to 50% depth;  $a_{p50} = ((l_{trial} \times b_{trial}) + (l_{trial} + b_{trial}) \times 2 \times d_{50}) =$ 

3.00 m<sup>2</sup>

Surface area of soakaway to 50% storage depth;  $A_{s50} = 2 \times (|_{trial} + b_{trial}) \times d_{trial} / 2 = 2.000 \text{ m}^2$ 

Soil infiltration rate;  $f = V_{p75\_25} / (a_{p50} \times t_{lg}) = 19.4 \times 10^{-6} \text{ m/s}$ 

Rectangular Pit Design

;;; Pit length; I = 2000 mm; Pit width; W = 2000 mmPit depth below invert; d = 2000 mm; Free volume;  $V_{free} = 30.0 \text{ %}$ ;;; Location of soakaway; Ireland; Return period; 50 years Ratio of 60 minute to 2 day rainfalls of 5 year return period (BRE digest 365 - fig 1); r = 0.30

Ratio of 60 minute to 2 day rainfalls of 5 year return period (BRE digest 365 - fig 1); r = 0.30;; Impermeable area;  $A = 98.0 \text{ m}^2$ ; Soil infiltration rate; f = 0.0000194 m/s

Surface area of soakaway to 50% storage depth

 $A_{s50} = 2 \times (1 + w) \times d / 2 = 8.000 \text{ m}^2$ 

Outflow factor; AF =  $A_{s50} \times f = 155.\times10^{-6} \text{ m}^{3}/\text{s}$ 

### M5 rainfalls are calculated from table 1 BRE digest 365 using Factor Z1

| Duration | M5<br>rainfalls | Growth factor Z2; | 50 year<br>rainfall; | Inflow             | Outflow             | Storage required    |
|----------|-----------------|-------------------|----------------------|--------------------|---------------------|---------------------|
| 5 mins   | 6.8 mm          | 1.65              | 11.2 mm              | 0.7 m <sup>3</sup> | 0.0 m <sup>3</sup>  | 0.7 m <sup>3</sup>  |
| 10 mins  | 9.8 mm          | 1.69              | 16.5 mm              | 1.1 m <sup>3</sup> | 0.1 m <sup>3</sup>  | 1.0 m <sup>3</sup>  |
| 15 mins  | 11.8 mm         | 1.69              | 20.0 mm              | 1.3 m <sup>3</sup> | 0.1 m <sup>3</sup>  | 1.2 m <sup>3</sup>  |
| 30 mins  | 15.4 mm         | 1.70              | 26.1 mm              | 1.7 m <sup>3</sup> | 0.3 m <sup>3</sup>  | 1.4 m <sup>3</sup>  |
| 1 hour   | 20.0 mm         | 1.66              | 33.2 mm              | 2.2 m <sup>3</sup> | 0.6 m <sup>3</sup>  | 1.6 m <sup>3</sup>  |
| 2 hours  | 25.0 mm         | 1.64              | 41.0 mm              | 2.7 m <sup>3</sup> | 1.1 m <sup>3</sup>  | 1.5 m <sup>3</sup>  |
| 4 hours  | 31.4 mm         | 1.60              | 50.3 mm              | 3.3 m <sup>3</sup> | 2.2 m <sup>3</sup>  | 1.0 m <sup>3</sup>  |
| 6 hours  | 35.6 mm         | 1.58              | 56.3 mm              | 3.7 m <sup>3</sup> | 3.4 m <sup>3</sup>  | 0.3 m <sup>3</sup>  |
| 10 hours | 42.4 mm         | 1.55              | 65.7 mm              | 4.3 m <sup>3</sup> | 5.6 m <sup>3</sup>  | -1.3 m <sup>3</sup> |
| 24 hours | 56.8 mm         | 1.50              | 85.3 mm              | 5.5 m <sup>3</sup> | 13.4 m <sup>3</sup> | -7.9 m <sup>3</sup> |

Required storage volume;

 $S_{reqd} = 1.9 \text{ m}^3$ 

Soakaway storage volume;

 $S_{act} = I \times d \times w \times V_{free} = \textbf{2.4 m}^3$ 

Soakaway storage volume- OK

Time for emptying soakaway to half volume;

 $T_{s50} = S_{reqd} \times 0.5 / (A_{s50} \times f) = 1 \text{ hr 25 min 43 s}$ 

Soakaway discharge time - OK