

**Drainage Design Report** 

for

**Residential Development** 

at

Neilstown Road, Dublin 22

Job No:

D1691-1

Architect:

John O'Neill & Associates Architects & Interior Designers Ltd.

Date:

August 2022

**Local Authority:** 

**South Dublin County Council** 

**Revision:** 

PL1

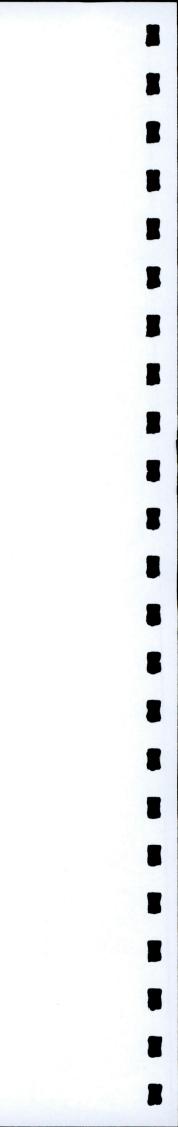








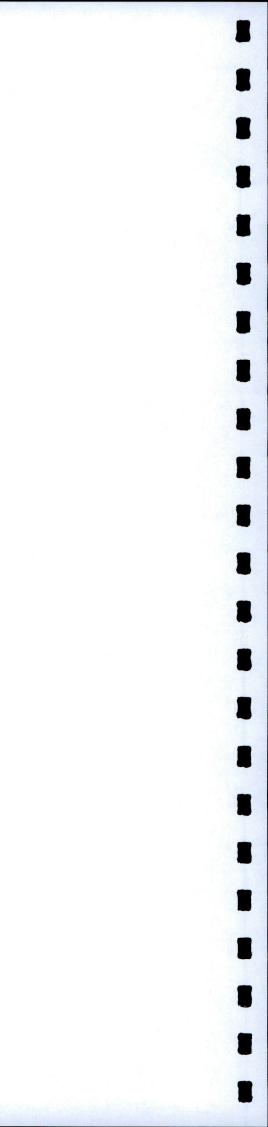
Calmount Park, Ballymount, Dublin 12.





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### **Site Overview:**

The site is located on the corner of Neilstown Road and Collinstown Road in Dublin 22. It is proposed to redevelop the existing site of Finches pub and off licence into a mixed use development containing new ground floor commercial unit, total number of 26 apartments and undercroft car parking.



Fig 1: Site Location

### **Vehicular Access:**

Vehicular access to the site is from Collinstown Road.

### **Existing & Proposed Drainage & Watermain:**

### Watermain:

The current Local Authority records show an existing 110mm diameter watermain spur off the 12" WM in Neilstown Road serving the site. A pre-connection enquiry was submitted to Irish Water and in the response we have received a "Confirmation of Feasibility" letter (see Appendix D) stating that the proposed development can be facilitated without any additional works to the local WM and Foul sewer networks. The watermain layout drawing provided as part of the planning submission indicates the proposed location of connection to the existing watermain spur and relocation of two sections of 100dia watermain to maintain 3m separation distance between the proposed structure and IW assets.



### Foul Drainage:

Irish Water in their "Confirmation of Feasibility" letter advised that a new foul sewer connection will have to be made to an existing 225mm diameter foul sewer located on the north side of Collinstown Road. The drainage layout drawing D1691-D1-Rev PL1 shows the proposed gravity discharge pipe serving the proposed development connecting to this foul sewer.

It is not envisaged that the internal network in the undercroft car parking will be taken in charge by the Local Authority however the foul sewer design will demonstrate design compliance with the relevant design codes including the minimum self-cleansing velocities of 0.75m/sec.

The "Confirmation of Feasibility" letter can be found in Appendix C.

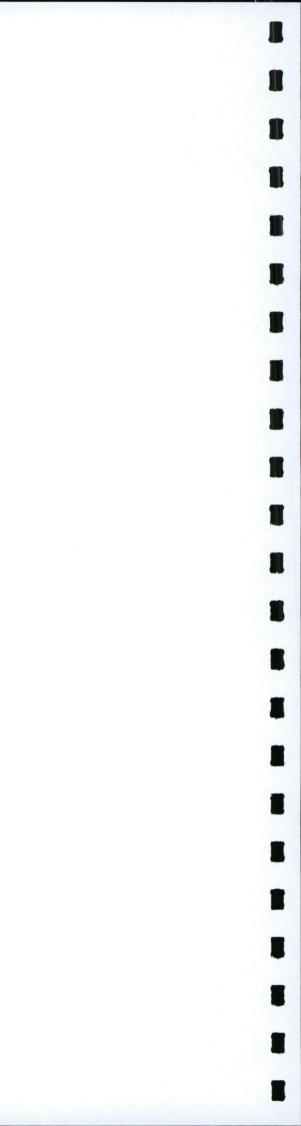
### Surface Water Drainage:

There is an existing 225mm diameter surface water drain located in the footpath of Collinstown Road. The drainage layout drawing D1691-D1-PL1 shows the restricted surface water connection from the proposed development to a new manhole on the aforementioned storm water line.

The surface water drainage design for the site will comply with the GDSDS with an allowable discharge to the public system restricted to Greenfield Runoff Rate QBAR for the site as calculated in this report. The flow restriction will be achieved by providing a flow control device (Hydrobrake or similar) on the outfall from the attenuation tank.

Due to the nature of this brown field site and the proposed high density development with car park underneath, attenuation ponds and storm water disposal through soakage in swales or wetlands are not applicable. Notwithstanding this we are proposing the alternative SUDS items forming a complete storm water runoff management train.

The treatment train approach was applied to both the storm water network and the attenuation design to ascertain that both runoff quality and quantity are appropriately addressed. An array of techniques was used to fulfil requirements of each element of the treatment train:



- Pollution prevention to prevent chemicals and other pollutants from contaminating
  the rainfall runoff, maintenance regime for the estate will be established and it will
  include regular sweeping of the car park and collection of rubbish. Provided waste bins
  will be sheltered to prevent the rainfall flushing the contaminants out of them.
- Source control and site control to detain and infiltrate the runoff as close as possible to the point of origin and to deal with as much of the runoff as possible on site an "extensive" sedum type green roof is proposed to the roof of the apartment block. This will be made up of fabric mats sown with sedum planting. This roof type allows for storm water interception and disposal through transpiration and evaporation. In addition to quantity reduction, the green roofs will improve the quality of the runoff and will become a wildlife habitat, improve biodiversity and boost the environmental credentials of the development. According to CIRIA 697 SUDS Manual, typical green roofs should attenuate storms up to a two-year return period event.
- Regional control to mimic the behaviour of the green field site and protect the receiving watercourse, the attenuation tank is designed to cater for all durations of rainfall up to 100 years return period. The design up to 100 years return will minimise the flooding potential of the receiving watercourse and other watercourses within this catchment. The storm water network and the proposed attenuation storage was checked in the drainage modelling and analysis computer software and no flooding on site was indicated for all storms up to 100 years return period of all durations with 20% CCF. The results of both 30 and 100 years storm analysis can be found in Appendices of this report.

### Flood Risk Assessment:

A desktop study carried out by Kavanagh Burke engineers did not show any pluvial or fluvial flood risks. The closest watercourse (Grand Canal) is located 1.7km to the south and the closest river (Liffey) is located in the valley 1.8km to the north from the subject site. No past single or recurring flood events were indicated within 1km of the site. Flood maps are available at floodinfo.ie website.





• Catchment Green Field Runoff Calculations





### **Surface Water Attenuation Calculations:**

### 1) Underground Attenuation Catchment

The design areas or the catchment are as follows:

Catchment Area: 1267m<sup>2</sup> (0.127 ha)

Total Impermeable Areas: 1132m<sup>2</sup>

Landscaping Areas: 135m<sup>2</sup>

### 2) Interception Storage

Interception storage accommodating the first 5mm of every rainfall from the proposed development will be provided within the Extensive Green Roof substrate installed on the roof of the proposed apartment block. The maximum water capacity of vegetation substrates in their installed state is approx. 35% (according to the green roof manufacturer's specification) providing interception of smaller rainfall events. According to CIRIA 697 SUDS Manual, typical green roofs should attenuate storms up to a two-year return period event.

The soft landscaping albeit being a small percentage of the site will also be a source of rainfall infiltration.

### 3) Greenfield Runoff Rate – QBAR, (mean annual flood flow):

Catchment Area: 0.127ha

QBAR<sub>rural</sub> (m<sup>3</sup>/sec) =  $0.00108 \times AREA^{0.89} \times SAAR^{1.17} \times SOIL^{2.17}$ 

SAAR (307000E, 234000N): 769 mm (as per Met Eireann data)

Soil Index: S1 (very low runoff)

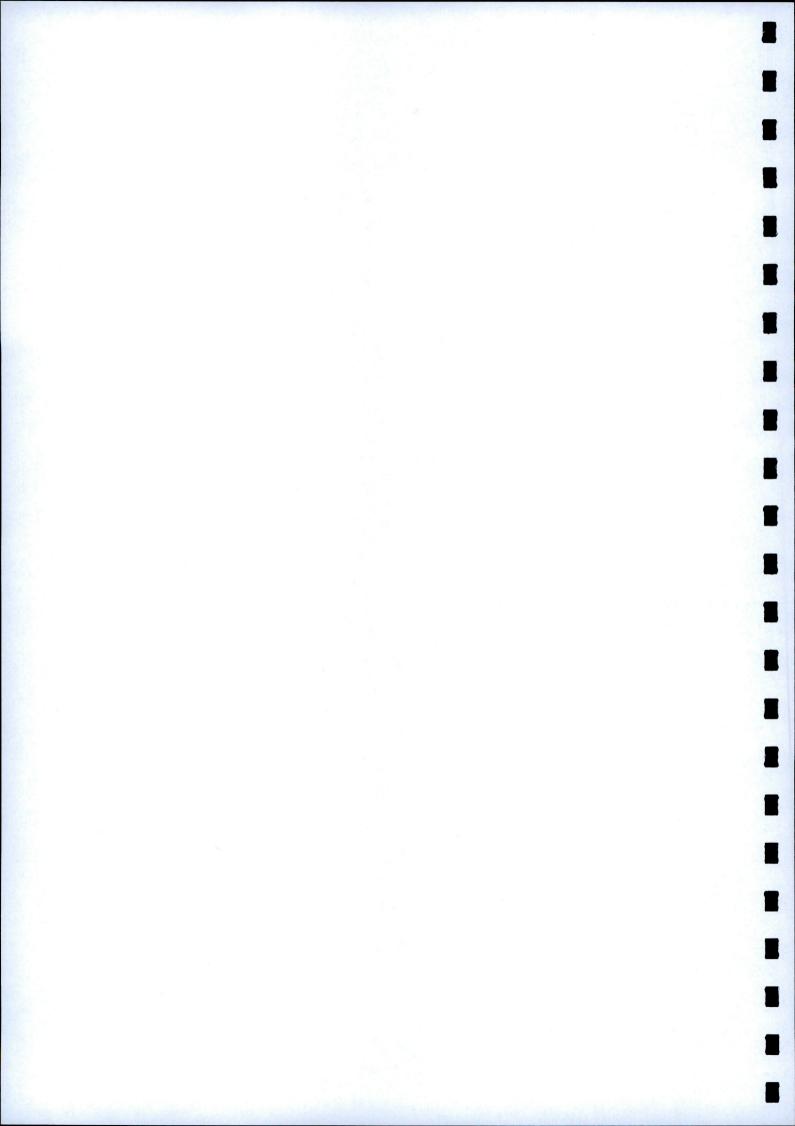
**S2** 

S3 (moderate runoff)

**S4** 

S5 (very high runoff)

 $Soil = 0.1(Soil_1) + 0.3(Soil_2) + 0.37(Soil_3) + 0.47(Soil_4) + 0.53(Soil_5)$ 





As the site is relatively small in catchment terms the soil class will be  $100\% \, \text{Soil}_2$  (as per uksuds.com greenfield runoff estimation tool)

Soil Class:

Soil<sub>2</sub>

**Runoff Potential:** 

Moderate to high

SPR Value:

0.3

QBAR:

As the site area is less than 50 hectares;

QBAR for 50 hectares is firstly calculated,

QBAR  $(m^3/sec) =$ 

 $0.00108 \times AREA^{0.89} \times SAAR^{1.17} \times SOIL^{2.17}$ 

 $0.00108 \times (0.5)^{0.89} \times (769)^{1.17} \times (0.3)^{2.17}$ 

101.72 l/sec 2.034 l/sec/Ha

QBAR for the smaller area (i.e. the subject site area):

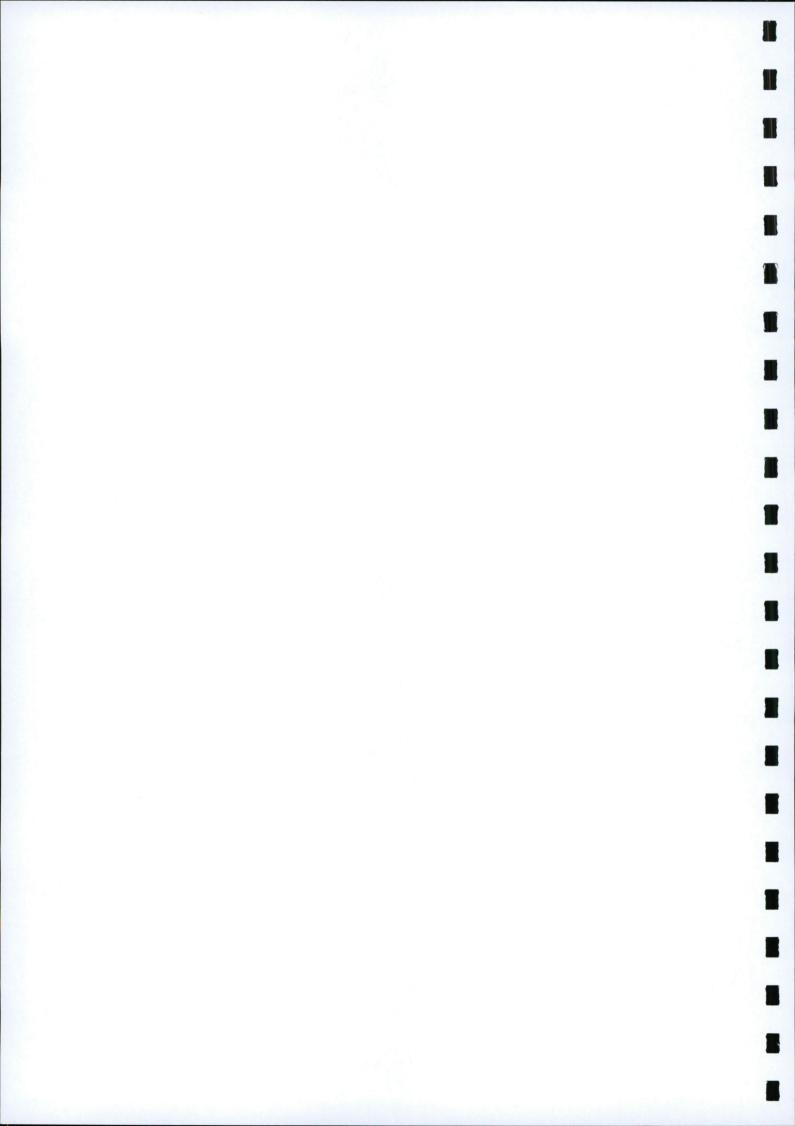
2.034 l/sec/Ha x 0.127 Ha 0.26 l/sec

<u>Due to the size of the orifice and potential blockage issues the minimum achievable</u> hydrobrake flow is 2.01/s therefore the QBAR will be set as 2.01/s

QBAR = 2.0 I/s

4) Attenuation storage volume

Refer to Appendix A for detailed storm water network modelling and attenuation storage volume check with a specific Hydrobrake flow control device included in the analysis.



Met Eireann Return Period Rainfall Depths for sliding Durations Irish Grid: Easting: 306750, Northing: 233880,

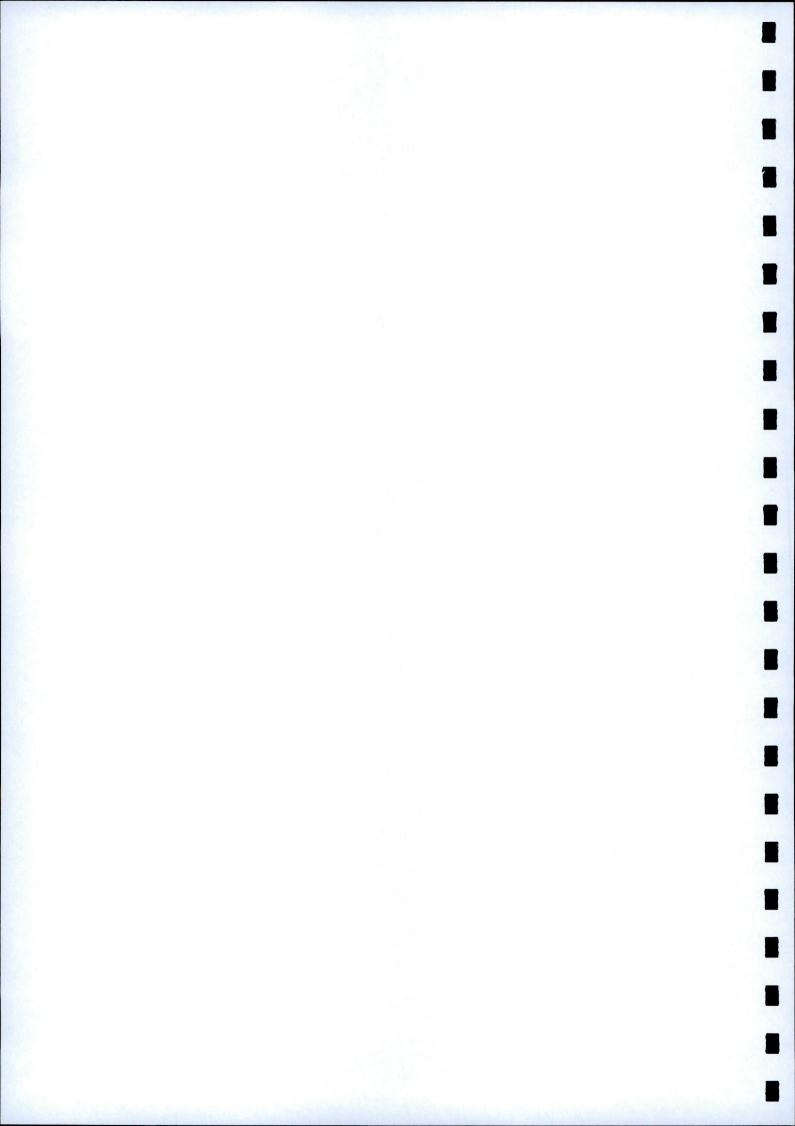
	2000	/A ,	/A ,	/A ,	/A ,	/A ,	/A ,	/A ,	/A ,	/A ,	/A ,	/A ,	/A ,	3.5,	1.7,	5.2,	4.7,	1.5,	6.3,	9.7,	2.0,	4.4,	294.6,	1.7.	
																							264.3,		
	200,	20.8,	28.9,	34.0,	41.8,	51.3,	63.0,	71.0,	77.3,	87.1,	98.2,	106.9,	120.5,	131.2,	142.7,	152.9,	161.9,	17.7,	191.5,	204.0,	215.5,	236.4,	255.2,	276.7,	
	150,	19.0,	26.5,	31.1,	38.3,	47.2,	58.1,	65.6,	71.6,	80.8	91.3,	99.2	112.3,	122.5,	133.9,	143.9,	152.8,	168.2,	181.7,	193.9,	205.1,	225.5,	243.9,	265.0,	
																							228.8,		
																							218.7,		
																							205.0,		
	30,	11.5,	16.0,	18.8,	23.6,	29.5,	37.0,	42.2,	46.3,	52.8,	60.2,	66.1,	75.4,	82.8,	93.5,	102.3,	110.00	123.4,	135.0,	145.6,	155.3,	142.9,	188.9,	207 3,	
Years	20,	10.1,	14.1,	16.5,	20.8	26.2,	32.9,	37.6,	11.4,	47.3,	54.1,	59.5,	58.1,	74.9,	85.2,	93.6, 1	01/1, 1	13.9, 1	25.1	35.2,	44.5,	61.4, 1	76.8, 1	4.6,	
Ye																							157.4,		
	5,	2, 8	7, 11	2, 13	1, 16	7 Q 21	4, 26	7, 30	4, 3	6, 39	5, 44	4, 49	6, 56	6, 6	5,07	7, 8(	9.	8, 98	3, 109	8, 118	8, 12	4, 14	6, 15	0, 17	
																							138.6,		
	4,	5.7,	8.0	9.4	12.0,	15.4,	19.8,	22.9,	25.3,	29.3,	33.9,	37.6,	43.4,	48.2.	56.8	63.7.	69.8	80.3	89.5	97.8	105.5	119.6,	132.6,	147.5,	
	3,	5.0,	7.0,	8.3,	10.7,	13.7,	17.7,	20.5,	22.7,	26.4,	30.6,	34.0,	39.4,	43.7.	51.9.	58.6	64.3.	74.3,	83.1,	91.1,	98.5	112.0,	124.4,	138.8,	
																							111.7,		
_		-	_	_	_			_	_	_			_							3.				3,	
rval	lyear	3.5	4.8	5	7.4	9.6	12.6																	115.3,	
Interval	6months,	2.3,	3.2.	3.8	5.0	6.7,	8.8	10.4	11.6.	13.7.	16.1	18.1	21.3,	23.9	29.8	34.6.	38.8	46.1.	52.6.	58.5	64.0.	74.3.	83.9	95.0	
	URATION	mins	mins	mins	30 mins	hours	hours	hours	hours	hours	hours	hours	8 hours	24 hours	System -	days.	SARO	days	days	days.	SAEP	days	20 days	days	•
	DUR	5	10	15	30	-	2	(*)	4	· · ·	0	12	18	24		1 ("	, 4	. (c	, 00	10	12	16	20	25	

N/A Data not available
These values are derived from a Depth Duration Frequency (DDF) Model
For details refer to:
'Fitzgerald D. L. (2007), Estimates of Point Rainfall Frequencies, Technical Note No. 61, Met Eireann, Dublin',
Available for download at www.met.ie/climate/dataproducts/Estimation-of-Roint-Rainfall-Frequencies\_IN61.pdf

M5-2d = 16.7mm

Ratio r=16.7/60.5 = 0.276

M5-60 = 16.7mm





- Specification/Product Information for;
- a) Petrol Interceptor







# Separators A RANGE OF FUEL/OIL SEPARATORS FOR PEACE OF MIND

Surface water drains normally discharge to a watercourse or indirectly into underground waters (groundwater) via a soakaway. Contamination of surface water by oil, chemicals or suspended solids can cause these discharges to have a serious impact on the receiving water.

The Environment Regulators,
Environment Agency, England and
Wales, SEPA, Scottish Environmental
Protection Agency in Scotland and
Department of Environment & Heritage
in Northern Ireland, have published
guidance on surface water disposal,
which offers a range of means of
dealing with pollution both at source
and at the point of discharge from site
(so called 'end of pipe' treatment).
These techniques are known as
'Sustainable Drainage Systems' (SuDS).

Where run-off is draining from relatively low risk areas such as car-parks and non-operational areas, a source control approach, such as permeable surfaces or infiltration trenches, may offer a suitable means of treatment, removing the need for a separator.

Oil separators are installed on surface water drainage systems to protect receiving waters from pollution by oil, which may be present due to minor leaks from vehicles and plant, from accidental spillage.

Effluent from industrial processes and vehicle washing should normally be discharged to the foul sewer (subject to the approval of the sewerage undertaker) for further treatment at a municipal treatment works.

### SEPARATOR STANDARDS AND TYPES

A British (and European) standard (EN 858-1 and 858-2) for the design and use of prefabricated oil separators has been adopted. New prefabricated separators should comply with the standard.

### SEPARATOR CLASSES

The standard refers to two 'classes' of separator, based on performance under standard test conditions.

### CLASS I

Designed to achieve a concentration of less than 5mg/l of oil under standard test conditions, should be used when the separator is required to remove very small oil droplets.

### CLASS II

Designed to achieve a concentration of less than 100mg/l oil under standard test conditions and are suitable for dealing with discharges where a lower quality requirement applies (for example where the effluent passes to foul sewer).

Both classes can be produced as full retention or bypass separators. The oil concentration limits of 5 mg/l and 100 mg/l are only applicable under standard test conditions. It should not be expected that separators will comply with these limits when operating under field conditions.

### **FULL RETENTION SEPARATORS**

Full retention separators treat the full flow that can be delivered by the drainage system, which is normally equivalent to the flow generated by a rainfall intensity of 65mm/hr.

On large sites, some short term flooding may be an acceptable means of limiting the flow rate and hence the size of full retention systems.

Get in touch for a FREE professional site visit and a representative will contact you within 5 working days to arrange a visit.

helpingyou@klargester.com to make the right decision or call 028 302 66799

### BYPASS SEPARATORS

Bypass separators fully treat all flows generated by rainfall rates of up to 6.5mm/hr. This covers over 99% of all rainfall events. Flows above this rate are allowed to bypass the separator. These separators are used when it is considered an acceptable risk not to provide full treatment for high flows, for example where the risk of a large spillage and heavy rainfall occurring at the same time is small.

### FORECOURT SEPARATORS

Forecourt separators are full retention separators specified to retain on site the maximum spillage likely to occur on a petrol filling station. They are required for both safety and environmental reasons and will treat spillages occurring during vehicle refuelling and road tanker delivery. The size of the separator is increased in order to retain the possible loss of the contents of one compartment of a road tanker, which may be up to 7,600 litres.

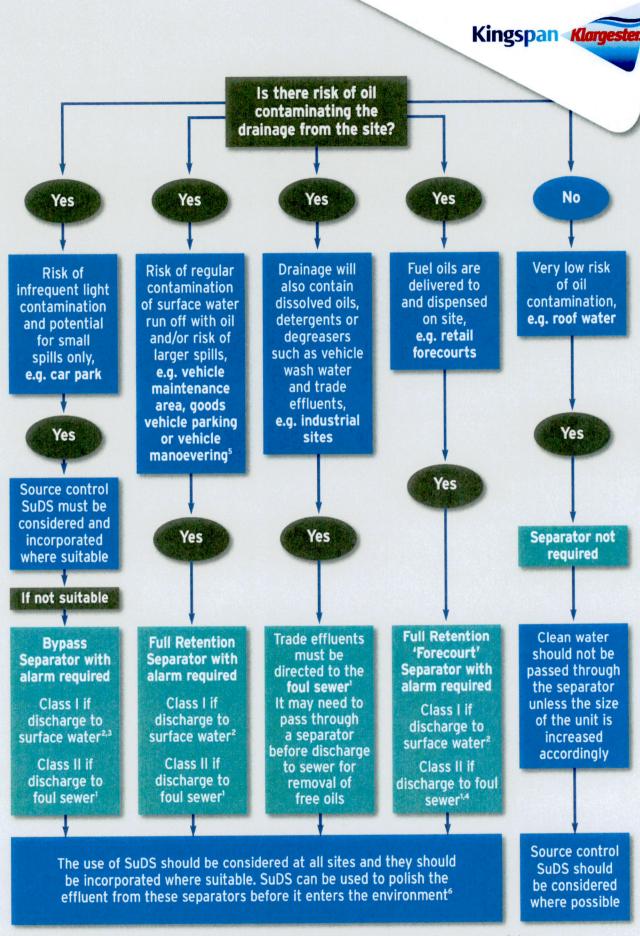
### SELECTING THE RIGHT SEPARATOR

The chart on the following page gives guidance to aid selection of the appropriate type of fuel/oil separator for use in surface water drainage systems which discharge into rivers and soakaways.

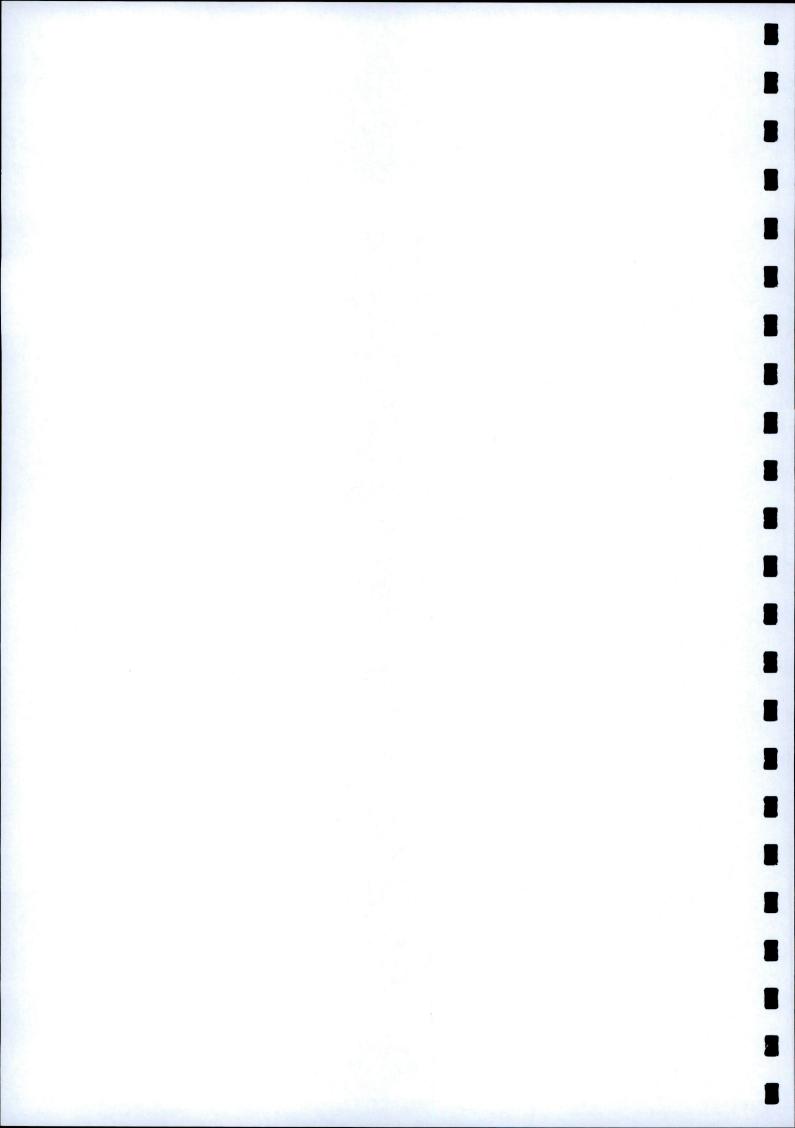
For further detailed information, please consult the Environment Agency Pollution Prevention Guideline 03 (PPG 3) 'Use and design of oil separators in surface water drainage systems' available from their website.

Klargester has a specialist team who provide technical assistance in selecting the appropriate separator for your application.





- 1 You must seek prior permission from your local sewer provider before you decide which separator to install and before you make any discharge.
- 2 You must seek prior permission from the relevant environmental body before you decide which separator to install.
- 3 In this case, if it is considered that there is a low risk of pollution a source control SuDS scheme may be appropriate.
- 4 In certain circumstances, the sewer provider may require a Class 1 separator for discharges to sewer to prevent explosive atmospheres from being generated.
- 5 Drainage from higher risk areas such as vehicle maintenance yards and goods vehicle parking areas should be connected to foul sewer in preference to surface water.
- 6 In certain circumstances, a separator may be one of the devices used in the SuDS scheme. Ask us for advice.



## Full Retention NSF RANGE

### Kingspan Klargester

### **APPLICATION**

Full retention separators are used in high risk spillage areas such as:

- Fuel distribution depots.
- Vehicle workshops.
- Scrap Yards

### **PERFORMANCE**

Klargester were the first UK manufacturer to have the required range (3-30 l/sec) certified to EN 858-1 in the UK. The NSF number denotes the flow at which the separator operates.

The British Standards Institute (BSI) have witnessed the performance tests of the required range of separators and have certified their performance, in relation to their flow and process performance to ensure that they met the effluent quality requirements of EN 858-1. Larger separator designs have been determined using the formulas extrapolated from the test range.

Each full retention separator design includes the necessary volume requirements for:

- Oil separation capacity.
- Oil storage volume.
- Silt storage capacity.
- Coalescer (Class I units only).
- Automatic closure device.

Klargester full retention separators treat the whole of the specified flow.

### **FEATURES**

- Light and easy to install.
- Class I and Class II designs.
- 3-30 l/sec range independently tested and performance sampled, certified by the BSI.
- Inclusive of silt storage volume.
- Fitted inlet/outlet connectors.



- Vent points within necks.
- Extension access shafts for deep inverts.
- Maintenance from ground level.
- GRP or rotomoulded construction (subject to model).

To specify a nominal size full retention separator, the following information is needed:-

- The calculated flow rate for the drainage area served. Our designs are based on the assumption that any interconnecting pipework fitted elsewhere on site does not impede flow into or out of the separator and that the influent is not pumped.
- The required discharge standard. This will decide whether a Class I or Class II unit is required.
- The drain invert inlet depth.
- Pipework type, size and orientation.

### SIZES AND SPECIFICATIONS

UNIT	FLOW (I/s)	DRAINAGE AREA (m²) PPG-3 (0.018)	STORAGE (lite		UNIT LENGTH (mm)	UNIT DIA.	BASE TO INLET INVERT	BASE TO OUTLET	MIN. INLET INLET (mm)	STANDARD PIPEWORK	
SIZE	.,,-,		SILT	OIL			(mm)	INVERT		DIA. (mm)	
NSFP003	3	170	300	30	1700	1350	1420	1345	500	160	
NSFP006	6	335	600	60	1700	1350	1420	1345	500	160	
NSFA010	10	555	1000	100	2610	1225	1050	1000	500	200	
NSFA015	15	835	1500	150	3910	1225	1050	1000	500	200	
NSFA020	20	1115	2000	200	3200	2010	1810	1760	1000	315	
NSFA030	30	1670	3000	300	3915	2010	1810	1760	1000	315	
NSFA040	40	2225	4000	400	4640	2010	1810	1760	1000	315	
NSFA050	50	2780	5000	500	5425	2010	1810	1760	1000	315	
NSFA065	65	3610	6500	650	6850	2010	1810	1760	1000	315	
NSFA080	80	4445	8000	800	5744	2820	2500	2450	1000	300	
NSFA100	100	5560	10000	1000	6200	2820	2500	2450	1000	400	
NSFA125	125	6945	12500	1250	7365	2820	2500	2450	1000	450	
NSFA150	150	8335	15000	1500	8675	2820	2550	2450	1000	525	
NSFA175	175	9725	17500	1750	9975	2820	2550	2450	1000	525	
NSFA200	200	11110	20000	2000	11280	2820	2550	2450	1000	600	

Rotomoulded chamber construction GRP chamber construction



### PROFESSIONAL INSTALLERS

### Klargester Accredited Installers

Experience shows that correct installation is a prerequisite for the long-lasting and successful operation of any wastewater treatment product. This is why using an installer with the experience and expertise to install your product is highly recommended.



### Services include:

- Site survey to establish ground conditions and soil types
- Advice on system design and product selection
- Assistance on gaining environmental consents and building approvals
- Tank and drainage system installation
- Connection to discharge point and electrical networks
- Waste emptying and disposal

Discover more about the Accredited Installers and locate your local expert online.

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### CARE & MAINTENANCE

#### Kingspan Environmental Services

Who better to look after your treatment plant than the people who designed and built it?



Factory trained engineers are available for site visits as part of a planned maintenance contract or on a one-off call out basis.

To find out more about protecting your investment and ensuring peace of mind, call us on:

#### 0844 846 0500

or visit us online: www.kingspanenvservice.com





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- PUMPSTOR24 PUMPING SYSTEMS
- STORMWATER ATTENUATION SYSTEMS
- OIL/WATER SEPARATORS
- BELOW GROUND STORAGE TANKS
- GREASE & SILT TRAPS



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- ABOVE GROUND RAINWATER HARVESTING SYSTEMS

UK: College Road North, Aston Clinton, Aylesbury, Buckinghamshire HP22 5EW Tel: +44 (0) 1296 633000 Fax: +44 (0) 1296 633001 Scottish Office: Tel: +44 (0) 1355 248484 email: info@klargester.com

Ireland: Unit 1a, Derryboy Road, Carnbane Business Park, Newry, Co. Down BT35 6QH

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email: info@klargester.ie

Visit our website www.klargester.com, or our company website www.kingspanenv.com







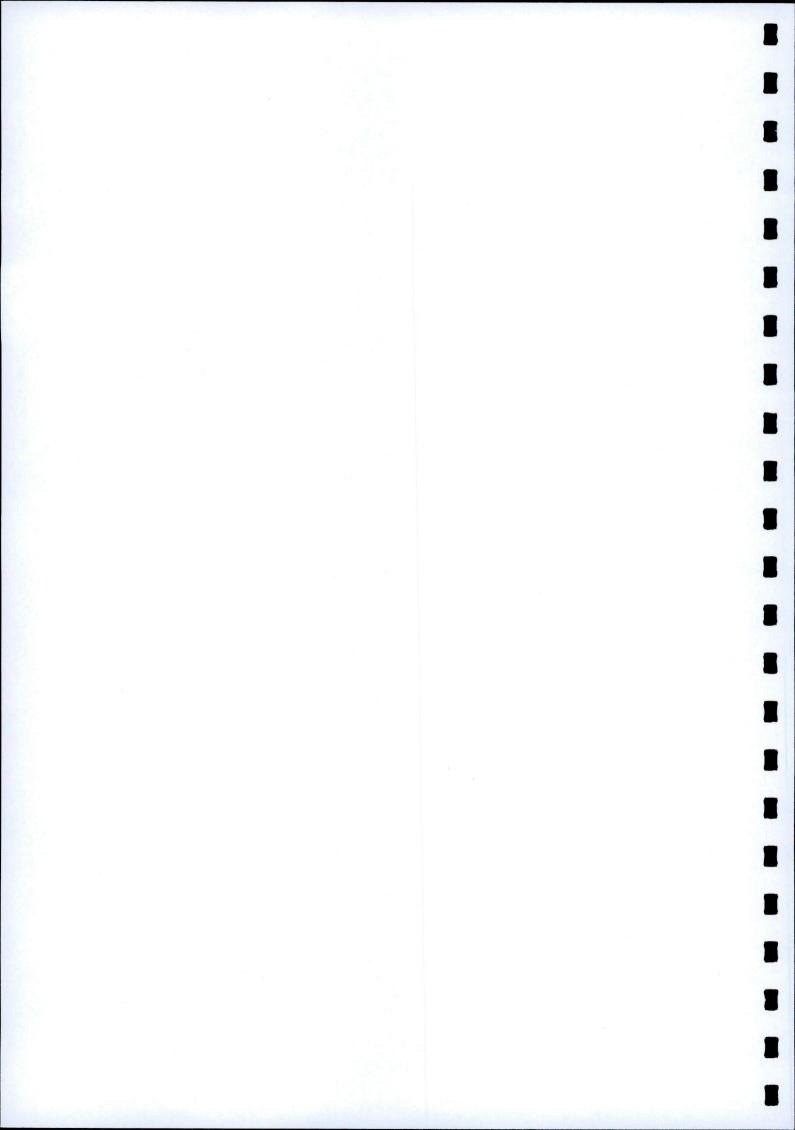






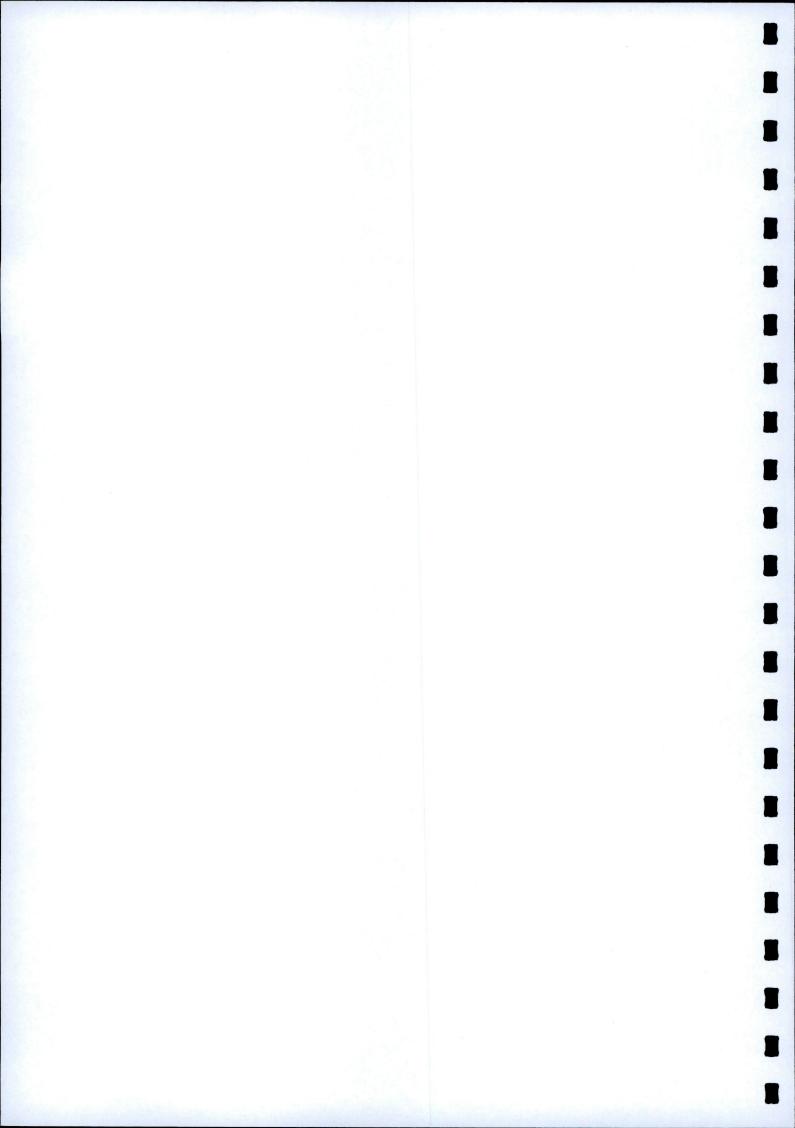
In keeping with Company policy of continuing research and development and in order to offer our clients the most advanced products, Kingspan Environmental reserves the right to alter specifications and drawings without prior notice.







Appendix A – Storm Water Drainage and Attenuation Design



KAVANAGH BURKE

Kavanagh Burke Unit G3 Calmount Business Pk Dublin 12 File: D1691 SW and Foul Rev Pl Network: SW1 Bartosz Kedzierski Page 1

**Design Settings** 

30/03/2021

Rainfall Methodology FSR Return Period (years) 2 Additional Flow (%) 0

FSR Region Scotland and Ireland M5-60 (mm) 16.700

Ratio-R 0.276 CV 0.750

Time of Entry (mins) 5.00

Maximum Time of Concentration (mins) 30.00

Maximum Rainfall (mm/hr) 100.0

Minimum Velocity (m/s) 1.00

Connection Type Level Soffits

Connection Type Level Soffit

Minimum Backdrop Height (m) 0.200

Preferred Cover Depth (m) 1.200

Include Intermediate Ground

Enforce best practice design rules x

<u>Links</u>

Name	US	DS	Length	ks (mm) /	US IL	DS IL	Fall	Slope	Dia	T of C	Rain
	Node	Node	(m)	n	(m)	(m)	(m)	(1:X)	(mm)	(mins)	(mm/hr)
1.000	SW1	SW2	13.532	0.600	63.550	63.450	0.100	135.3	225	5.20	49.6
1.001	SW2	SW3	23.649	0.600	63.450	63.340	0.110	215.0	225	5.65	48.0
1.002	SW3	EX SW	84.716	0.600	63.340	61.830	1.510	56.1	225	6.45	45.5

Name	Vel (m/s)	•		Depth		Maximum Depth (m)	(ha)	Σ Add Inflow (I/s)
1.000	1.122	44.6	15.8	1.475	1.485	1.485	0.117	0.0
1.001	0.888	35.3	15.3	1.485	1.595	1.595	0.117	0.0
1.002	1.749	69.6	14.5	1.595	1.375	1.595	0.117	0.0

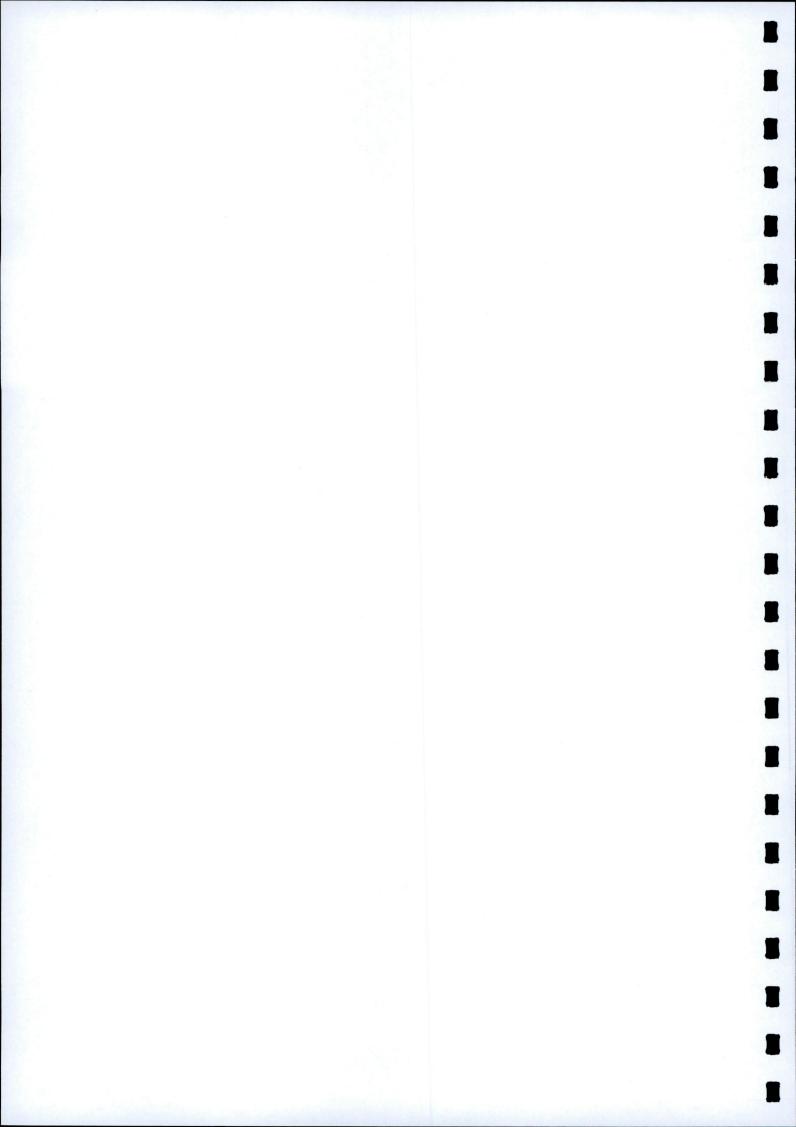
**Manhole Schedule** 

Node	Easting (m)	Northing (m)	CL (m)	Depth (m)	Dia (mm)	Connection	s	Link	IL (m)	Dia (mm)
SW1	706689.716	733902.434	65.250	1.700	1200	<b>→</b> 0				
							0	1.000	63.550	225
SW2	706703.201	733903.565	65.160	1.710	1200	1	1	1.000	63.450	225
							0	1.001	63.450	225
SW3	706703.104	733927.214	65.160	1.820	1200	<b>→</b> 0	1	1.001	63.340	225
						1	0	1.002	63.340	225
EX SW	706787.451	733919.311	63.430	1.600	1200	1—	1	1.002	61.830	225

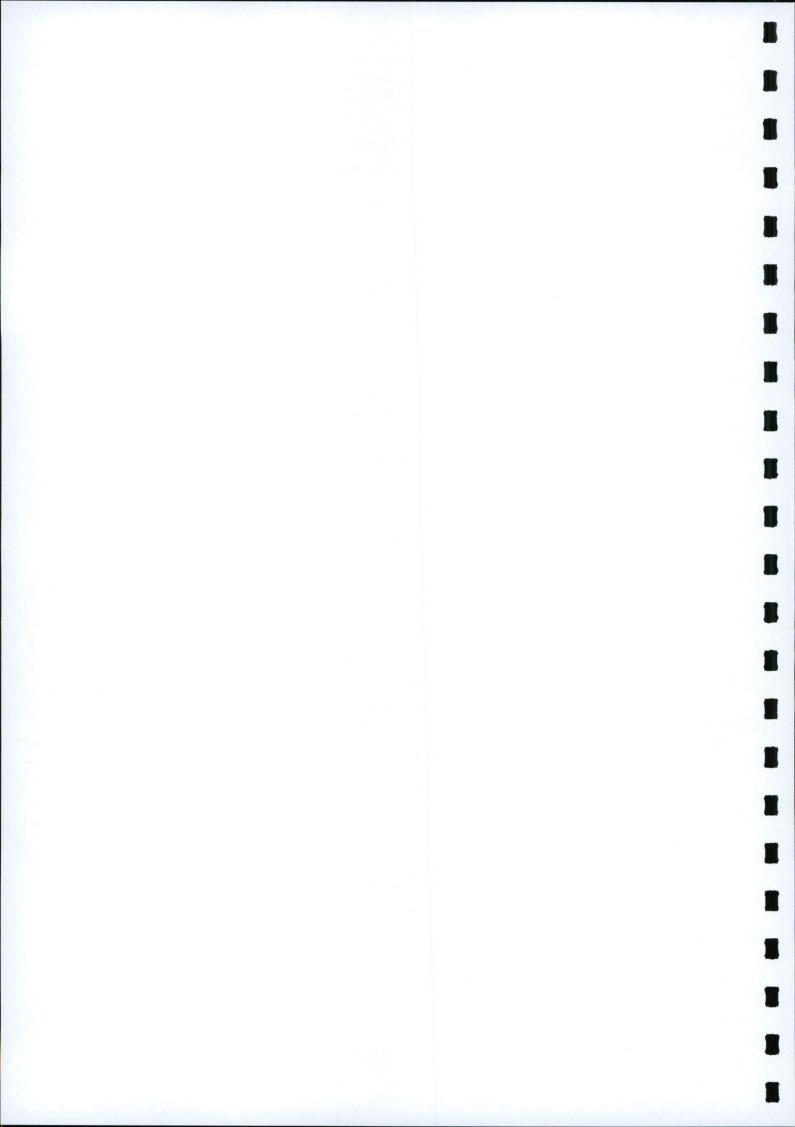
### **Simulation Settings**

Rainfall Methodology FSR Region	FSR Scotland and Ireland
M5-60 (mm)	16.700
Ratio-R	0.276
Summer CV	0.750
Winter CV	0.950

Analysis Speed Skip Steady State x
Drain Down Time (mins) 240
Additional Storage (m³/ha) 20.0
Check Discharge Rate(s) x
Check Discharge Volume x



Kavanagh Burke File: D1691 SW and Foul Rev Pl Page 2 Network: SW1 Unit G3 Calmount Business Pk Kavanagh Burke Bartosz Kedzierski Dublin 12 CONSULTING ENGINEERS 30/03/2021 **Storm Durations** 360 600 960 2160 4320 180 15 60 5760Q 720 1440 2880 30 120 240 480 **Additional Flow Additional Area Return Period Climate Change** (Q %) (years) (CC %) (A %) 0 0 20 30 0 0 100 **O** 20 20% CCF Storm Durations used for Node SW1 Online Hydro-Brake® Control analysis up to 5760min = 4 days (HE) Minimise upstream storage Objective Flap Valve **Replaces Downstream Link** Sump Available CTL-SHE-0067-2000-1000-2000 Invert Level (m) 63.550 **Product Number** 0.100 Design Depth (m) 1.000 Min Outlet Diameter (m) Min Node Diameter (mm) 1200 2.0 Design Flow (I/s) Node SW1 Depth/Area Storage Structure 63.550 Base Inf Coefficient (m/hr) 0.00000 Safety Factor 2.0 Invert Level (m) 0.00000 **Porosity** 1.00 Time to half empty (mins) 236 Side Inf Coefficient (m/hr) Depth Area Inf Area Depth Inf Area Depth Area Inf Area Area (m<sup>2</sup>)(m<sup>2</sup>)(m<sup>2</sup>)(m) (m<sup>2</sup>)(m<sup>2</sup>)(m) (m) (m<sup>2</sup>)0.0 1.010 0.1 0.000 45.0 0.0 1.000 45.0 0.0 Proposed attenuation volume = **Rainfall** Area x Depth =  $45 \times 1 = 45 \text{m}$ **Event** Peak Average **Peak Average Event** Intensity Intensity Intensity Intensity (mm/hr) (mm/hr) (mm/hr) (mm/hr) 2.187 67.619 30 year +20% CC 2880 minute summer 8.159 238.965 30 year +20% CC 15 minute summer 5.483 2.187 67.619 30 year +20% CC 2880 minute winter 30 year +20% CC 15 minute winter 167.695 6.307 1.649 30 year +20% CC 4320 minute summer 30 year +20% CC 30 minute summer 164.133 46.444 30 year +20% CC 4320 minute winter 1.649 4.153 115.181 46.444 30 year +20% CC 30 minute winter 1.349 5.270 114.603 30.286 30 year +20% CC 5760 minute summer 30 year +20% CC 60 minute summer 3.411 1.349 30 year +20% CC 5760 minute winter 76.140 30.286 30 year +20% CC 60 minute winter 87.705 309.949 72.942 19.276 100 year +20% CC 15 minute summer 30 year +20% CC 120 minute summer 217.508 87.705 100 year +20% CC 15 minute winter 48.461 19.276 30 year +20% CC 120 minute winter 60.634 214.282 100 year +20% CC 30 minute summer 57.087 14.690 30 year +20% CC 180 minute summer 100 year +20% CC 30 minute winter 150.373 60.634 14.690 30 year +20% CC 180 minute winter 37.108 39.339 148.859 100 year +20% CC 60 minute summer 30 year +20% CC 240 minute summer 45.778 12.098 98.898 39.339 30 year +20% CC 240 minute winter 30.414 12.098 100 year +20% CC 60 minute winter 93.958 24.830 100 year +20% CC 120 minute summer 35.665 9.178 30 year +20% CC 360 minute summer 24.830 100 year +20% CC 120 minute winter 62,423 23.183 9.178 30 year +20% CC 360 minute winter 73.073 18.804 100 year +20% CC 180 minute summer 7.536 28.516 30 year +20% CC 480 minute summer 47.499 18.804 100 year +20% CC 180 minute winter 18.945 7.536 30 year +20% CC 480 minute winter 100 year +20% CC 240 minute summer 58.338 15.417 30 year +20% CC 600 minute summer 23.634 6.465 15.417 100 year +20% CC 240 minute winter 38.758 30 year +20% CC 600 minute winter 16.148 6.465 11.615 45.136 30 year +20% CC 720 minute summer 21.275 5.702 100 year +20% CC 360 minute summer 11.615 29.340 14.298 5.702 100 year +20% CC 360 minute winter 30 year +20% CC 720 minute winter 9.488 35.904 4.676 100 year +20% CC 480 minute summer 17.757 30 year +20% CC 960 minute summer 9.488 100 year +20% CC 480 minute winter 23.854 4.676 30 year +20% CC 960 minute winter 11.762 100 year +20% CC 600 minute summer 29.636 8.106 13.187 3.534 30 year +20% CC 1440 minute summer 20.249 8.106 100 year +20% CC 600 minute winter 30 year +20% CC 1440 minute winter 8.863 3.534 26.587 7.126 100 year +20% CC 720 minute summer 30 year +20% CC 2160 minute summer 9.661 2.670 7.126 17.868 100 year +20% CC 720 minute winter 30 year +20% CC 2160 minute winter 6.657 2.670 Flow+ v9.1 Copyright © 1988-2021 Causeway Software Solutions Limited





Kavanagh Burke Unit G3 Calmount Business Pk Dublin 12 File: D1691 SW and Foul Rev Pl Network: SW1 Bartosz Kedzierski 30/03/2021 Page 3

### <u>Rainfall</u>

Event	Peak Intensity (mm/hr)	Average Intensity (mm/hr)	Event	Peak Intensity (mm/hr)	Average Intensity (mm/hr)	
100 year +20% CC 960 minute summer	22.071	5.812	100 year +20% CC 2880 minute summer	9.930	2.661	
100 year +20% CC 960 minute winter	14.620	5.812	100 year +20% CC 2880 minute winter	6.673	2.661	
100 year +20% CC 1440 minute summer	16.268	4.360	100 year +20% CC 4320 minute summer	7.609	1.989	
100 year +20% CC 1440 minute winter	10.933	4.360	100 year +20% CC 4320 minute winter	5.011	1.989	
100 year +20% CC 2160 minute summer	11.827	3.268	100 year +20% CC 5760 minute summer	6.317	1.617	
100 year +20% CC 2160 minute winter	8.149	3.268	100 year +20% CC 5760 minute winter	4.089	1.617	





Kavanagh Burke Unit G3 Calmount Business Pk Dublin 12 File: D1691 SW and Foul Rev Pl Network: SW1 Bartosz Kedzierski Page 4

## Results for 30 year +20% CC Critical Storm Duration. Lowest mass balance: 99.73%

30/03/2021

US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (I/s)	Node Vol (m³)	Flood (m³)		Status
SW1	200	64.283	0.733	9.4	34.8084	0.0000	SUF	RCHARGED
SW2	13	63.488	0.038	2.0	0.0425	0.0000	OK	
SW3	36	63.366	0.026	2.0	0.0294	0.0000	OK	
EX SW	37	61.856	0.026	2.0	0.0000	0.0000	OK	
US	Link	DS (	utflow	Velocity	Flow/Ca	p Lin	k	Discharge
Node		Node	(I/s)	(m/s)		Vol (r	n³)	Vol (m³)
SW1	1.000	SW2	2.0	0.503	0.04	4 0.05	27	
SW2	1.001	SW3	2.0	0.610	0.05	5 0.08	313	
SW3	1.002	EX SW	2.0	0.772	0.02	8 0.21	44	17.5
	Node SW1 SW2 SW3 EX SW US Node SW1 SW2	Node         (mins)           SW1         200           SW2         13           SW3         36           EX SW         37           US         Link           Node         SW1           SW1         1.000           SW2         1.001	Node         (mins)         (m)           SW1         200         64.283           SW2         13         63.488           SW3         36         63.366           EX SW         37         61.856           US         Link         DS         O           Node         Node           SW1         1.000         SW2           SW2         1.001         SW3	Node         (mins)         (m)         (m)           SW1         200         64.283         0.733           SW2         13         63.488         0.038           SW3         36         63.366         0.026           EX SW         37         61.856         0.026           US         Link         DS         Outflow           Node         Node         (I/s)           SW1         1.000         SW2         2.0           SW2         1.001         SW3         2.0	Node         (mins)         (m)         (m)         (l/s)           SW1         200         64.283 0         0.733         9.4           SW2         13         63.488         0.038         2.0           SW3         36         63.366         0.026         2.0           EX SW         37         61.856         0.026         2.0           VS         Link         DS         Outflow         Velocity           Node         Node         (l/s)         (m/s)           SW1         1.000         SW2         2.0         0.503           SW2         1.001         SW3         2.0         0.610	Node         (mins)         (m)         (m)         (l/s)         Vol (m³)           SW1         200         64.283         0.733         9.4         34.8084           SW2         13         63.488         0.038         2.0         0.0425           SW3         36         63.366         0.026         2.0         0.0294           EX SW         37         61.856         0.026         2.0         0.0000           US         Link         DS         Outflow         Velocity         Flow/Ca           Node         Node         (l/s)         (m/s)         0.04           SW1         1.000         SW2         2.0         0.503         0.04           SW2         1.001         SW3         2.0         0.610         0.05	Node         (mins)         (m)         (m)         (l/s)         Vol (m³)         (m³)           SW1         200         64.283  O.733         9.4         34.8084         0.0000           SW2         13         63.488         0.038         2.0         0.0425         0.0000           SW3         36         63.366         0.026         2.0         0.0294         0.0000           EX SW         37         61.856         0.026         2.0         0.0000         0.0000           US         Link         DS         Outflow         Velocity         Flow/Cap         Link           Node         (l/s)         (m/s)         Vol (r           SW1         1.000         SW2         2.0         0.503         0.044         0.05           SW2         1.001         SW3         2.0         0.610         0.055         0.08	Node         (mins)         (m)         (m)         (l/s)         Vol (m³)         (m³)           SW1         200         64.283         0.733         9.4         34.8084         0.0000         SUI           SW2         13         63.488         0.038         2.0         0.0425         0.0000         OK           SW3         36         63.366         0.026         2.0         0.0294         0.0000         OK           EX SW         37         61.856         0.026         2.0         0.0000         0.0000         OK           US         Link         DS         Outflow         Velocity         Flow/Cap         Link           Node         Node         (l/s)         (m/s)         Vol (m³)           SW1         1.000         SW2         2.0         0.503         0.044         0.0527           SW2         1.001         SW3         2.0         0.610         0.055         0.0813

Max water level in the attenuation and drainage network for storms up to 1:30y return. Critical event duration 200min. Maximum achieved water level during this event does not exceed the high water level in the proposed attenuation tank (64.55m) therefore proposed attenuation has sufficient capacity to accommodate storms up to 1in30 years return. See drawing ref. D1691-D1-PL1 for attenuation base and high water level.





Kavanagh Burke Unit G3 Calmount Business Pk Dublin 12 File: D1691 SW and Foul Rev Pl Network: SW1 Bartosz Kedzierski

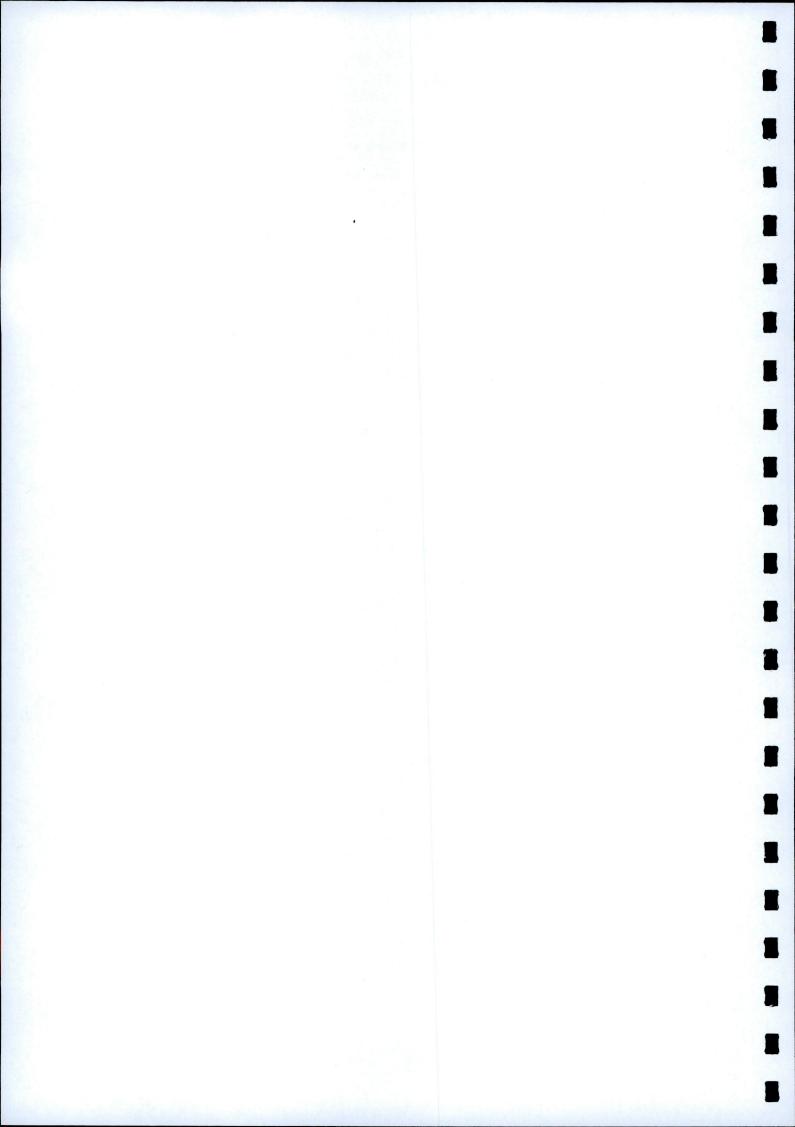
30/03/2021

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## Results for 100 year +20% CC Critical Storm Duration. Lowest mass balance: 99.73%

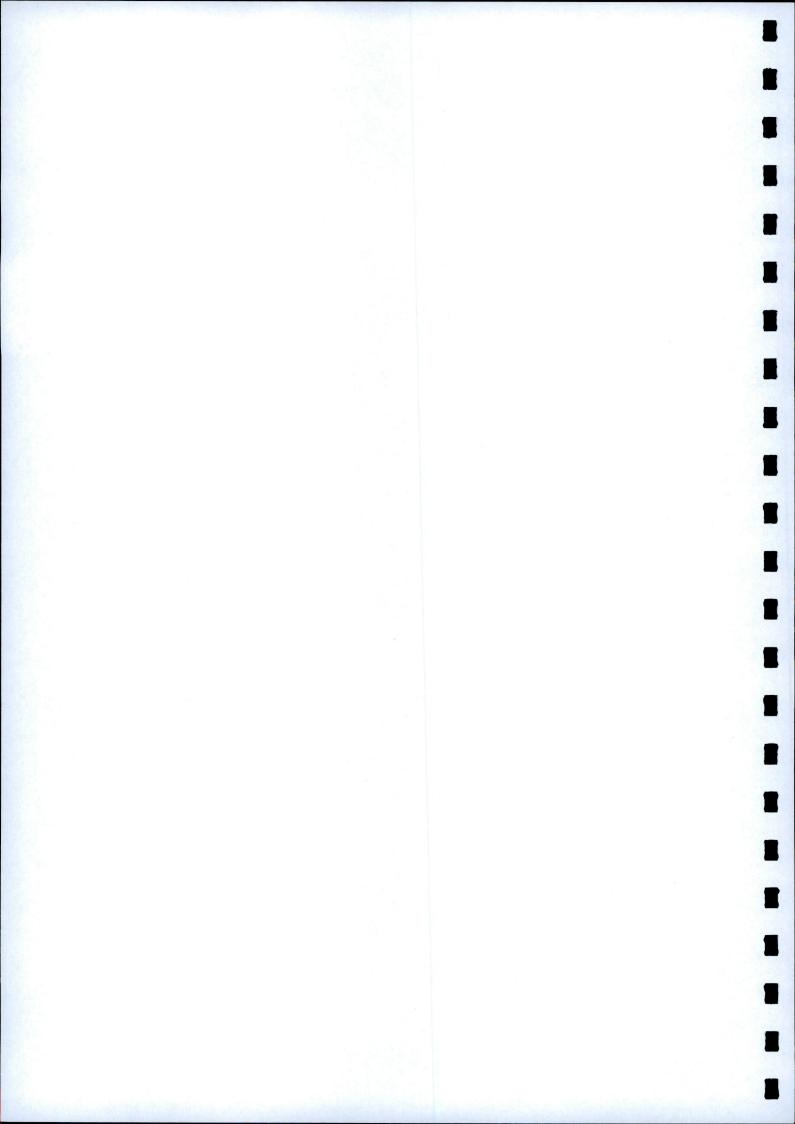
Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (I/s)	Node Vol (m³)	Flood (m³)		Status
240 minute winter	SW1	224	64.546	0.996	12.0	47.3201	0.0000	SUI	RCHARGED
15 minute winter	SW2	12	63.488	0.038	2.0	0.0426	0.0000	OK	
240 minute winter	SW3	228	63.366	0.026	2.0	0.0295	0.0000	OK	
240 minute winter	EX SW	228	61.856	0.026	2.0	0.0000	0.0000	OK	
Link Event	US	Link	DS (	utflow	Velocity	Flow/Ca	p Lin	k	Discharge
(Upstream Depth)	Node		Node	(I/s)	(m/s)		Vol (r	n³)	Vol (m³)
240 minute winter	SW1	1.000	SW2	2.0	0.504	0.04	4 0.05	30	
15 minute winter	SW2	1.001	SW3	2.0	0.620	0.05	6 0.08	313	
240 minute winter	SW3	1.002	EX SW	2.0	0.774	0.02	8 0.21	.54	47.0

Max water level in the attenuation and drainage network for storms up to 1:100y return. Critical event duration 224min. Maximum achieved water level during this event does not exceed the high water level in the proposed attenuation tank (64.55m) therefore proposed attenuation has sufficient capacity to accommodate storms up to 1in100 years return. See drawing ref. D1691-D1-PL1 for attenuation base and high water level.





Appendix B – Foul Sewer Network Design



Kavanagh Burke CONSULTING ENGINEERS

1.000

1.001

1.140 45.3

1.560 62.0

6.2

6.2

0.775

1.005

1.005

1.225

Kavanagh Burke **Consulting Engineers**  File: D1691-1 SW and Foul Rev Network: F1 Bartosz Kedzierski

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0.801

0.993

**Design Settings** 

26/08/2022

Frequency of use (kDU) 0.50 Flow per dwelling per day (I/day) 2700 Domestic Flow (I/s/ha) 0.0 Industrial Flow (I/s/ha) 0.0 Additional Flow (%)

Minimum Velocity (m/s) 1.00 **Connection Type Level Soffits** Minimum Backdrop Height (m) 0.200 Preferred Cover Depth (m) 1.200 Include Intermediate Ground

156.0

156.0

0

0

0.0

0.0

57

48

**Nodes** 

Name	Units	Cover Level (m)	Manhole Type	Depth (m)	
F1	156.0	65.150	Foul MH	1.000	
F2		65.140	Foul MH	1.230	
F3		65.050	Foul MH	1.450	

**Links** 

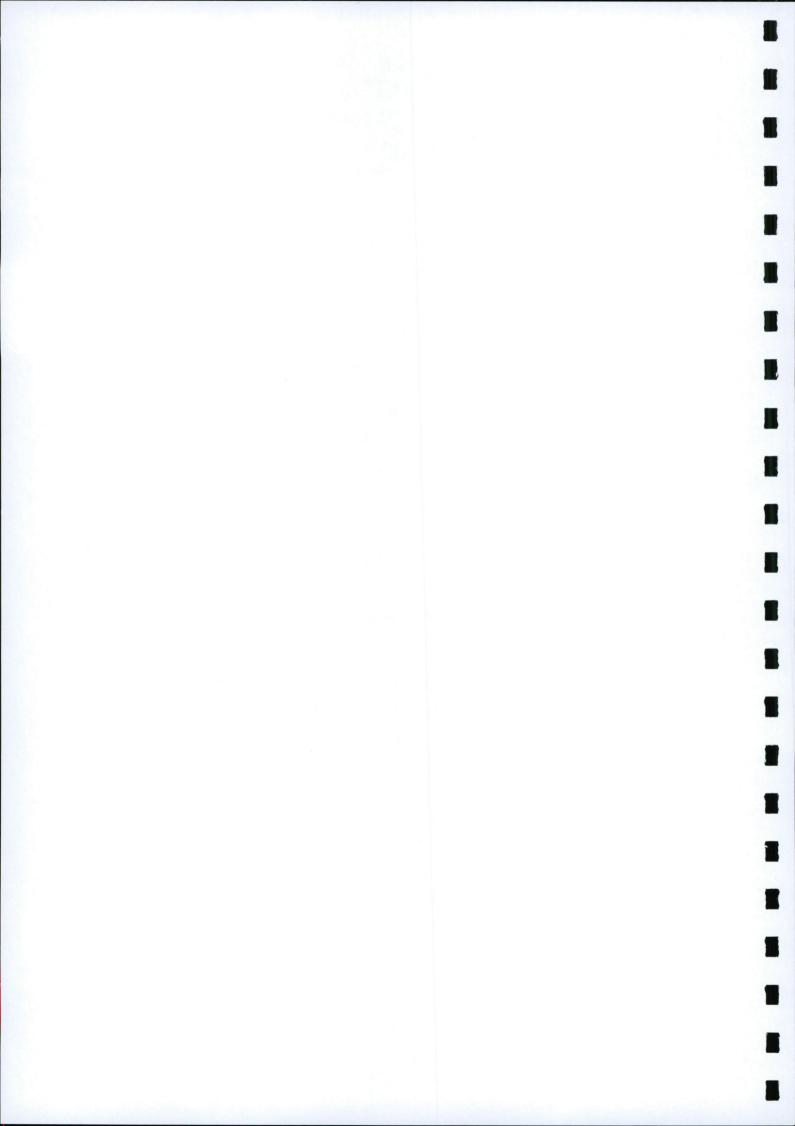
	Name	US	DS	Len	gth ks	(mm) /	US IL	DS IL	Fall	Slope	Dia	
		Nod	e Node	e (m	1)	n	(m)	(m)	(m)	(1:X)	(mm)	
	1.000	F1	F2	24.3	336	1.500	64.150	63.91	0.240	101.4	225	
	1.001	F2	F3	16.8	322	1.500	63.910	63.60	0.310	54.3	225	
Name	Vel (m/s)	Cap (I/s)	Flow (I/s)	US Depth (m)	DS Depth (m)	Σ Area (ha)	Σ Dwel (ha	_		Σ Add Inflow (ha)	Pro Depth (mm)	Pro Velocity (m/s)

0.000

0.000

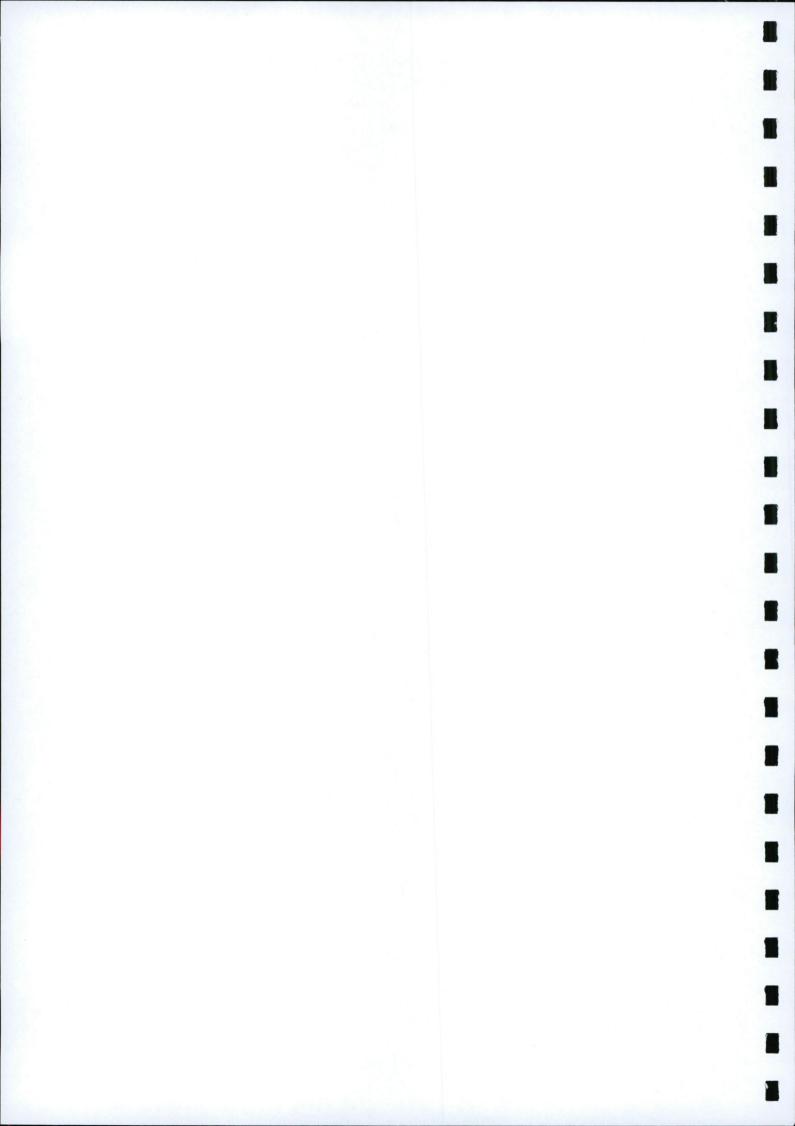
#### **Manhole Schedule**

Node	Easting (m)	Northing (m)	CL (m)	Depth (m)	Dia (mm)	Connections	Link	IL (m)	Dia (mm)
F1	706704.500	733904.741	65.150	1.000	1200	$\stackrel{\bullet}{\bigcirc}$			
						0	1.000	64.150	225
F2	706704.138	733929.074	65.140	1.230	1200	, 1	1.000	63.910	225
						1 0	1.001	63.910	225
F3	706704.878	733945.880	65.050	1.450	1200	1	1.001	63.600	225





Appendix C – Correspondence





Declan O'Sullivan

22 December 2020

Re: CDS20008071 pre-connection enquiry - Subject to contract | Contract denied

Connection for Housing Development of 30 unit(s) at Finches Public House, Neilstown Neighbourhood Center, Dublin 22, Dublin

Uisce Éireann Bosca OP 448 Oifig Sheachadta na Cathrach Theas Cathair Chorcaí

Irish Water PO Box 448, South City Delivery Office, Cork City.

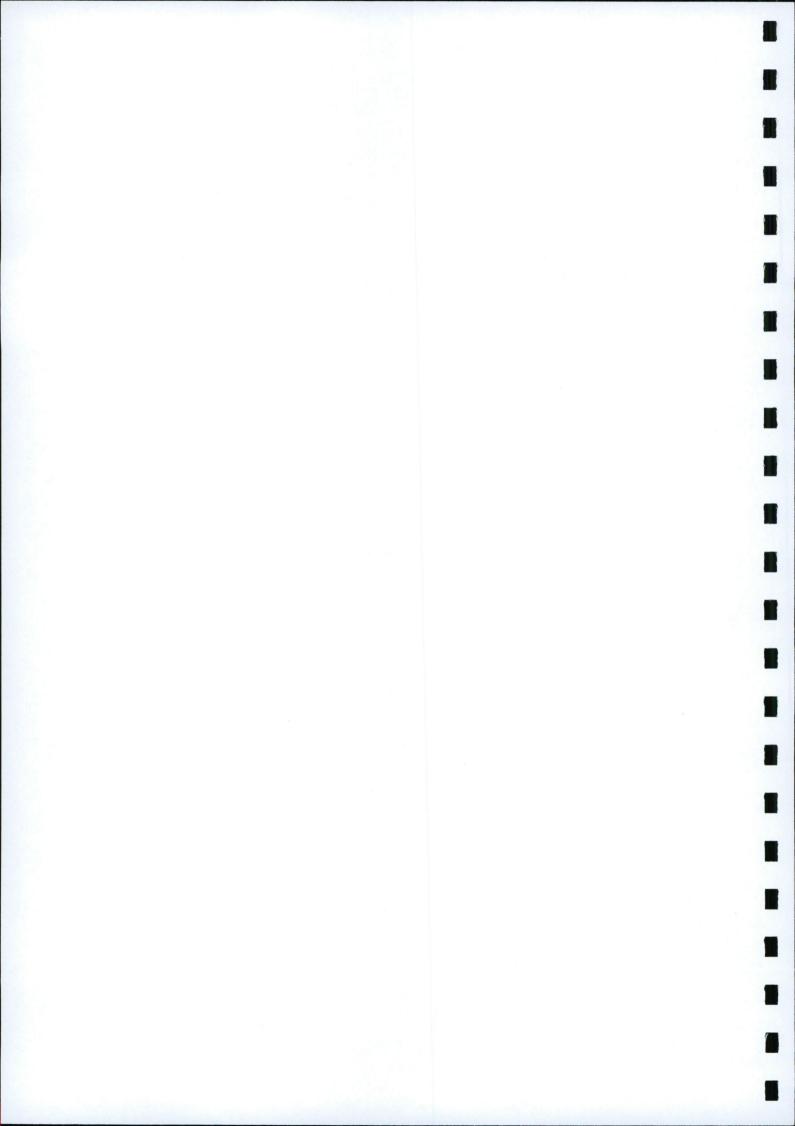
www.water.ie

Dear Sir/Madam,

Irish Water has reviewed your pre-connection enquiry in relation to a Water & Wastewater connection at Finches Public House, Neilstown Neighbourhood Center, Dublin 22, Dublin (the **Premises**). Based upon the details you have provided with your pre-connection enquiry and on our desk top analysis of the capacity currently available in the Irish Water network(s) as assessed by Irish Water, we wish to advise you that your proposed connection to the Irish Water network(s) can be facilitated at this moment in time.

SERVICE	OUTCOME OF PRE-CONNECTION ENQUIRY  THIS IS NOT A CONNECTION OFFER. YOU MUST APPLY FOR A  CONNECTION(S) TO THE IRISH WATER NETWORK(S) IF YOU WISH  TO PROCEED.
Water Connection	Feasible without infrastructure upgrade by Irish Water
Wastewater Connection	Feasible without infrastructure upgrade by Irish Water
	SITE SPECIFIC COMMENTS
Water Connection	This Confirmation of Feasibility to connect to the Irish Water infrastructure does not extend to your fire flow requirements. Please note that Irish Water can not guarantee a flow rate to meet fire flow requirements and in order to guarantee a flow to meet the Fire Authority requirements, you should provide adequate fire storage capacity within your development.
Wastewater Connection	Connection to be made to the 225mm sewer across Colinstown Road.

The design and construction of the Water & Wastewater pipes and related infrastructure to be installed in this development shall comply with the Irish Water Connections and Developer Services Standard Details and Codes of Practice that are available on the Irish Water website. Irish Water reserves the right to supplement these requirements with Codes of Practice and these will be issued with the connection agreement.



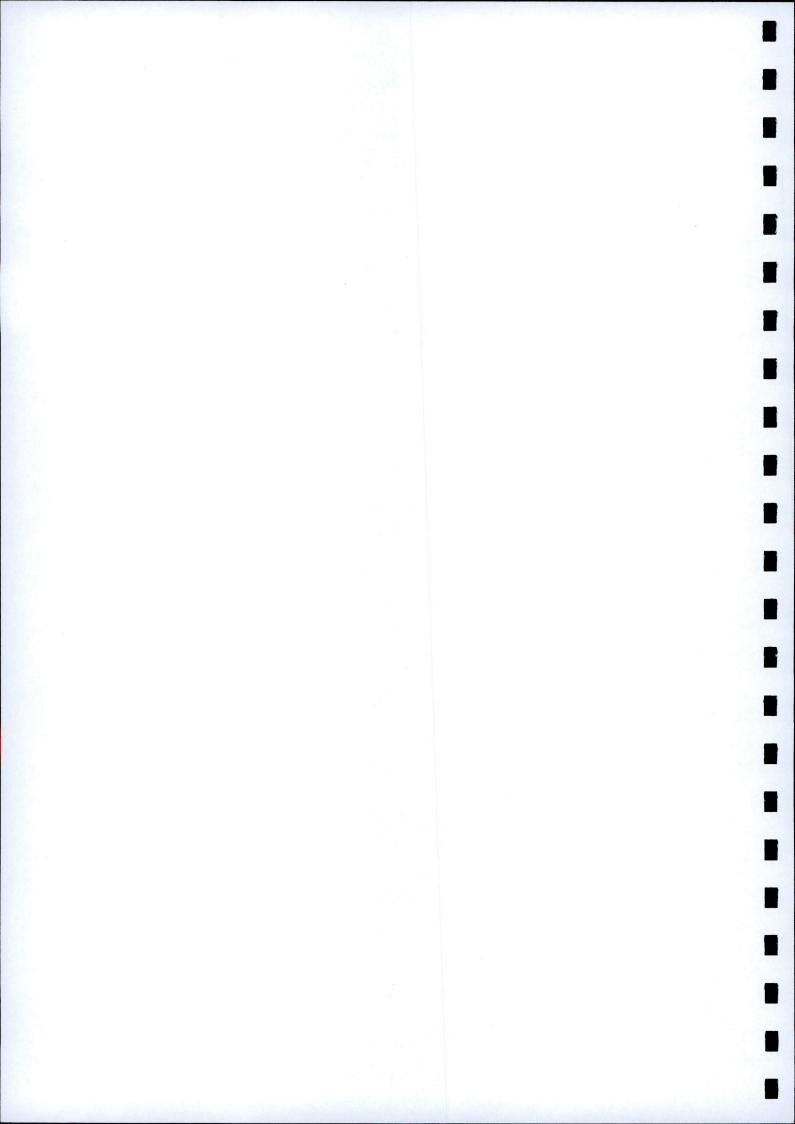
# The map included below outlines the current Irish Water infrastructure adjacent to your site:



Reproduced from the Ordnance Survey of Ireland by Permission of the Government. License No. 3-3-34

Whilst every care has been taken in its compilation Irish Water gives this information as to the position of its underground network as a general guide only on the strict understanding that it is based on the best available information provided by each Local Authority in Ireland to Irish Water. Irish Water can assume no responsibility for and give no guarantees, undertakings or warranties concerning the accuracy, completeness or up to date nature of the information provided and does not accept any liability whatsoever arising from any errors or omissions. This information should not be relied upon in the event of excavations or any other works being carried out in the vicinity of the Irish Water underground network. The onus is on the parties carrying out excavations or any other works to ensure the exact location of the Irish Water underground network is identified prior to excavations or any other works being carried out. Service connection pipes are not generally shown but their presence should be anticipated.

#### **General Notes:**



- 1) The initial assessment referred to above is carried out taking into account water demand and wastewater discharge volumes and infrastructure details on the date of the assessment. The availability of capacity may change at any date after this assessment.
- 2) This feedback does not constitute a contract in whole or in part to provide a connection to any Irish Water infrastructure. All feasibility assessments are subject to the constraints of the Irish Water Capital Investment Plan.
- 3) The feedback provided is subject to a Connection Agreement/contract being signed at a later date.
- 4) A Connection Agreement will be required to commencing the connection works associated with the enquiry this can be applied for at <a href="https://www.water.ie/connections/get-connected/">https://www.water.ie/connections/get-connected/</a>
- 5) A Connection Agreement cannot be issued until all statutory approvals are successfully in place.
- 6) Irish Water Connection Policy/ Charges can be found at https://www.water.ie/connections/information/connection-charges/
- 7) Please note the Confirmation of Feasibility does not extend to your fire flow requirements.
- 8) Irish Water is not responsible for the management or disposal of storm water or ground waters. You are advised to contact the relevant Local Authority to discuss the management or disposal of proposed storm water or ground water discharges
- 9) To access Irish Water Maps email datarequests@water.ie
- 10) All works to the Irish Water infrastructure, including works in the Public Space, shall have to be carried out by Irish Water.

If you have any further questions, please contact Marko Komso from the design team on 022 54611 or email mkomso@water.ie For further information, visit www.water.ie/connections.

Yours sincerely,

Gronne Hassis

**Yvonne Harris** 

**Head of Customer Operations** 

