Engineering Services Report

Shared Educational Campus for Gaelscoil Na Camóige, Gaelscoil Chluain Dolcáin and Coláiste Chillian, Old Nangor Road, Clondalkin, Dublin 22

> February 2017 Revision A

TOBIN CONSULTING ENGINEERS







REPORT

PROJECT:

Shared Educational Campus
Old Nangor Road
Clondalkin
Dublin 22
Planning Engineering Services Report

CLIENT:

Department of Education and Skills

COMPANY:

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Client: Department of Education and Skills

Project: Shared Educational Campus, Old Nangor Road, Clondalkin, Dublin 22

Title: Planning Engineering Services Report

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1 INTRODUCTION

This report has been prepared to detail the engineering solutions to roads, drainage and water supply as part of a planning submission for a proposed schools development located on a brownfield site on Old Nangor Road, Clondalkin, Dublin 22. It should be read in conjunction with the watermain, roads, foul and storm design drawings (refer to **Appendix 1** for drawings) as outlined and noted herein. The schools are proposed by The Department of Education and Skills (DoES).

This report details the foul and storm drainage design and the water mains for said schools. The site encompasses approximately 4.87Ha of land, is a brown field site and has a boundary on all sides. It is proposed to provide direct access to the site from the existing Old Nangor Road along the southern boundary of the site. A separate entry and exit point will be designed to assist with traffic flow and increase safety.

It is proposed to discharge the foul effluent generated by the proposed campus to the existing 900mm public foul sewer which runs along New Nangor Road to the north of the site. Details of the foul drainage are outlined in detail in Section 4 below and drawing 8064-2501.

It is proposed to discharge the storm water generated by the proposed campus to the existing 300mm public storm sewer which runs along New Nangor Road to the north of the site. The controlled discharge flow rate will be set at the allowable Greenfield run off rate of 10.49l/s (Qbar) or 3.46l/s/Ha as detailed in Section 3 below and drawing 8064-2501.

It is proposed that the watermain for the development will connect to the existing 300mm public watermain located along New Nangor Road.

2 WATER SUPPLY

2.1 POTABLE WATER SUPPLY

It is proposed to connect a new 100mm diameter uPVC watermain to the existing 300mm diameter watermain on the north boundary of the site along R134 as shown on Drawing No. 8064-2502. This new watermain is to include boundary boxes with integral stopcocks at the connections. Provision is also to be made for the installation of flow meter chambers.

Staff/Student estimated water usage of 60l/day/person utilised is according to Table 3 of the EPA Design Manual – Treatment Systems for Small Communities Business, Leisure Centres and Hotels. A pre-connection enquiry was issued to Mr. Michael McAdam in South Dublin County

Council on 09/08/16. Mr McAdam concluded that "The site is adequately serviced for peak potable water demand as a 300mm main lies to the north of the site". A copy of correspondence between TOBIN and South Dublin County Council is included **Appendix 3**.

Fire hydrants will be located around the schools within a minimum distance of 46m from any part of the schools footprint and within a minimum distance of 30m to a vehicle access roadway or hard-standing area for fire appliances according to Part B of the building regulations.

Refer to Appendix 1 for Watermain layout.

3 SURFACE WATER

3.1 GENERAL

South Dublin County Council records indicate a 300mm diameter surface water (SW) pipe north of the site. A new on site surface water drainage system has been designed in accordance with the Greater Dublin Strategic Drainage Strategy (GDSDS). It will ensure surface water discharge from the site is limited to QBAR (3.46 l/s/ha), in accordance with GDSDS, through a combination of attenuation storage tanks and permeable paving. This will ensure the current surface water discharge rate from the Shared Educational Campus will be reduced from its current discharge rates, thus reducing the loadings to the 300mm diameter public surface water network located to the north of the site. All surface water from the attenuation system will connect to the existing surface water drain via a petrol interceptor and hydrobrake.

The storm drainage for the entire development has been designed using the Micro Drainage's Windes Drainage design Software in accordance with the Recommendations for Site Development Works for Housing Areas and also the recommendations of the Greater Dublin Strategic Drainage Study (GDSDS). The details of the Micro Drainage outputs for the pipe designs and associated long sections are outlined at **Appendix 6** of this report. The storm water drainage has been designed to cater for surface water from public hard surfaces in the proposed development including roadways, footpaths, and the proposed building.

The drainage network has been designed so that the network pipelines and manholes will not be surcharged as a result of the critical 2-year critical rainfall and will not overflow as a result of the critical rainfall with a 30-year and 100-year storm return period intensity.

The most up-to-date rainfall intensities for the site area have been derived from Met Eireann. 10% climate change has been implemented in the attenuation capacity design, as per South Dublin County Council requirements.

Refer to Appendix 1 for drainage drawings and Appendix 4 for attenuation calculations.

3.2 SUDS (SUSTAINABLE URBAN DRAINAGE SYSTEMS)

The general principal behind SUDs is to reduce the quantity of water leaving a site and increase the quality of water leaving the site. In practice a calculation for the site runoff is carried out using the Institute of Hydrology report No. 124. This gives the limit for discharge from the site.

In accordance with the GDSDS (Greater Dublin Strategic Drainage Study), underground storage is provided for the 1 in 30 year storm with on site attenuation provided for the 1 in 100 yr storm, to ensure that there is no flooding of the buildings. A flood risk assessment is carried out to ensure that there is no risk of damage to property or people and to mitigate against flood risks, flood routing is designed into the site layout. A flood risk assessment was carried out. A synopsis has been provided below in Section 4.4 with full details included in the planning documents.

Typical types of SUDs which may be used are Infiltration systems (Infiltration trenches, Soakaways and Permeable paving), Attenuation systems (Attenuation tanks and Proprietary systems), Attenuation Ponds, Detention Basins, Rainwater harvesting and Green Roofs.

Types of SUDs devices, which may be applicable to the campus;

Given the development is to be constructed on a brownfield site, the following SUDs approach have been reviewed and found to be suitable for the site, subject to detail design.

Permeable paving

It is proposed to use permeable block paving in a section of the staff car park bays. This will consist of a layer stone of gravel with a voids ratio of 40% approximately 0.5m in depth with a impermable geotextile lining under our typical surface courses.

Attenuation

The combined attenuation systems of permeable paving and Aquacell units (or similar approved) have been designed for storm periods with rainfall intensities taken for up to the 100 years return period. The proposed stormwater drainage system will be restricted by a hydrobrake to QBAR (10.49l/s) to the existing surface water pipe to the east of the site.

Bypass Separator

It is proposed to install a Bypass Separator under the proposed basketball courts where the storm drainage system discharges to the existing storm sewer. The stormwater from the external paved areas will include run-off from the car park and therefore may have hydrocarbons within their flow. These hydrocarbons pollutants require removal so they are not discharged back into the environment. The separator has been sized to cater for the total external paved area. The location of the separator is shown in the civils layout in **Appendix 1** with details included in **Appendix 7** of this report.

From the selection tables in the Separator Product Brochure in **Appendix 7**, a NSBE 040 or similar interceptor is required to cater for the hydrocarbons which may be present in the stormwater collected from this site. This separator is designed to cater for an approximate area of 22,222m². However, the paved area of the site is 16,693m², therefore, the separator is designed to cater for an area in excess of the required capacity.

3.3 RAINWATER HARVESTING

Storm water from the roof of the proposed building will discharge to a rainwater harvesting system (RWHT) located to the north west of the proposed building. Stored water will be distributed by pump to a static water storage tank that will feed the toilets and general landscaping taps when required. Overflow will be provided to the proposed storm sewer complete with a non-return valve. The total volume of the system will be 15,000 litres (Kingspan or similar underground commercial rainwater harvesting tanks). The location of the proposed tanks are shown on the civils layout drawing in **Appendix 1** of this report while details of the rainwater harvesting tanks are included in **Appendix 8**.

3.4 FLOOD RISK ASSESSMENT

This Flood Risk Assessment (FRA) presents a review of:

- OPW Flood Maps:
- OPW Preliminary Flood Risk Assessment Maps:
- South Dublin County Development Plan (2015-2021);
- The Planning System & Flood Risk Management (PSFRM) Guidelines; and
- Eastern CFRAM Study.

Due to the proximity of the site to the Camac River, fluvial flooding was initially identified as the primary potential risk to the proposed development.

The PSFRM guidance document recommends that "Highly Vulnerable" developments, such as the proposed schools, be constructed in flood zone C, i.e. that there is less than a 0.1% probability of the site flooding.

Based on the extrapolation of water levels predicted as part of the Eastern CFRAM study the 100 and 1000 year MRFS flood levels in the River Camac adjacent to the site have been estimated as 58.02mOD and 59.24mOD respectively. This includes an allowance for climate change.

The lowest recorded existing ground elevation at the site (63.05mOD) is 3.81m above the predicted 1-in-1000-year MRFS flood level.

Based on flood analysis carried out as part of the Eastern CFRAM study and recorded elevations at the proposed site, it is estimated that the proposed development at Old Nangor Road is located in Flood Zone C and therefore will not be inundated by flooding during the 1 in 1000 year mid-range-future-scenario.

4 FOUL WATER

4.1 GENERAL

South Dublin County council records indicate the presence of an existing 750/900mm diameter combined sewer pipe running along New Nangor Road.. It is proposed that the foul drainage from the proposed campus will discharge to this existing 750/900MMmm diameter sewer. A wayleave will be provided over this existing 750/900mm diameter pipe, to be taken in charge by the council. Following discussions with South Dublin County Council it was determined that there are "no problems with foul capacity". Full details of feedback from South Dublin County Council are included in **Appendix 3**.

4.2 OCCUPANCY FIGURES & WASTEWATER FLOW RATES

The occupancy figures and associated hydraulic loadings of the proposed schools are in accordance with The Environmental Protection Agency Wastewater Treatment Manual "Treatment Systems for Small Communities, Business, Leisure Centres and Hotels". A wastewater flow rate, for students and staff, of 60 litres/person/day and 30 BOD5 grams/person/day is assumed from Table 3 of the above manual. A wastewater flow rate, for visitors, of 10 litres/person/day and 15 BOD5 grams/person/day is also assumed. A summary of the total Hydraulic and Organic loadings based on the figures in Table 3 of the above Manual is outlined below:

Source		Hydraulic L (Litres/Day)	oading	BOD₅ (Grams/Day)	Load	P.E.
Description	Total Occupancy	Per Occupancy	Total	Per Occupancy	Total	P.E.
Total Staff/students	1000 staff/students 10 visitors	60 10	60100	30 15	30,300	505

Table 4.2.1 – Summary of Hydraulic and Organic Loadings

Therefore, the total Hydraulic load for the proposed development is 60,100 litres per day and the proposed PE is 505. Calculations have been provided in **Appendix 5**.

NOTE: A co-ordination exercise was carried out taking into account existing services ensuring no clashes will be encountered between new and existing services.

Please refer to Appendix 1 for drainage drawings.

5 SITE INVESTIGATIONS

Site Investigations were carried out by Techsol Ltd. Location of site investigations is shown on drawing 8064-2000 in **Appendix 1**. A summary of the ground types encountered in the exploratory holes is listed below, in approximate stratigraphic order:

- Topsoil: The exploratory holes generally encountered topsoil to a depth of 200-300mm.
- Made Ground (fill): Reworked clay fill was encountered at locations TP04-TP06, BH02-BH08 to a maximum observed depth of 2.0m (BH08).
- Glacial Till: Firm to stiff brown sandy gravelly clay, frequently with low cobble content, was
 encountered at all locations to a maximum observed depth of 3.2m at BH08 overlying stiff to
 very stiff grey brown sandy gravelly clay to a maximum observed depth of 5.4m at BH06.
- Bedrock (limestone): Rotary drilling was not undertaken to prove the depth or integrity of the bedrock.

Infiltration tests were undertaken at three locations, IT01 to IT03. The absence of significant outflow from the pits precluded the measurement of any actual infiltration rates. The low permeability fine-grained soils are considered to be poor infiltration media, and would be deemed unsuitable for the implementation of infiltration drainage systems. All storm drains and attenuations tanks have been designed should to allow for minimal infiltration to ground in accordance with the recommendations of BRE Digest 365 and CIRIA 697 (SUDS).

6 ROADS AND TRAFFIC

6.1 GENERAL

The design and layout of access road and parking areas have been developed with reference to the following:

- Design Manual for Roads and Streets (March 2013)
- RA Design Manual for Roads and Bridges
- Traffic Signs Manual published by the DOE
- DTO Traffic Management Guidelines

Access to the site will be from Old Nangor Road along the southern boundary of the site. A separate entry and exit point will be designed to assist with traffic flow and increase safety. The proposed campus is within a 50km/hr speed limit zone. The visibility splay of 2.4m x 45m is in accordance with Design Manual for Urban Roads and Streets. This visibility splay at the junctions is achievable in both directions. The existing access road to the existing secondary school will be maintained, however it will be changed from a dual purpose entry and exit road to a single purpose entry. The existing secondary school will merge with traffic from the new primary schools on exit.

Dedicated pedestrian and cyclist access points will be provided, ensuring separation from the vehicle access point. A Swept Path Analysis has been carried out and concluded no issues with the proposed road layout. Please refer to auto-track drawings in **Appendix 1** of this report.

A Traffic and Transport Assessment, Mobility Management Plan and a Road Safety Audit were requested. Conclusions of the above are outlined below with full details included in the planning documents.

6.2 TRAFFIC AND TRANSPORT ASSESSMENT

This Traffic and Transport Assessment has been prepared to assess the proposal by The Department of Education and Skills to construct a shared educational campus consisting of 2 no. schools within the site of an existing primary and post primary school off the Old Nangor Road in Clondalkin, Co. Dublin.

- ORS have undertaken detailed traffic analysis and investigation into the likely traffic impact
 the development may have. Current and future traffic flows were established on the
 surrounding road network.
- The site access arrangements and the key junctions identified on the wider road network were subjected to capacity analysis to examine the potential traffic levels generated from the site and the existing road network. These junctions were tested for AM and PM peak conditions for baseline, potential year of opening, and future design years. While the tests demonstrate that the proposed development will marginally impact on the existing road network it must be noted that there are pre-existing capacity issues on the junctions which were tested as part of this assessment during morning and evening peak times. All tests have shown that the development proposal will not significantly reduce the capacity levels of the junctions reviewed in this assessment. The existing capacity issues on the junctions analysed during this assessment are as a result of the traffic volume in the area at peak times as the road network in the area is an arterial route which links north and south Dublin.
- The proposed access arrangements will operate efficiently and within capacity limits for all design scenarios and future design years. The proposed access arrangements will also result in a much improved scenario in terms of vehicular permeability to the school as all parking and drop offs will be accommodated within the site as opposed to the public road which is currently the case. All traffic will be able to enter and leave the site in forward gear safely and within the prescribed guidelines.
- The internal site layout has been designed to provide a safe and efficient circulatory system
 that reduces the potential for conflicting movements at the site accesses and within the site.
 All signage and safety measures possible will be implemented to ensure maximum safety
 within the site.
- In transportation engineering terms, the proposal put forward will not be a significant factor to
 the future operation and capacity of the junctions identified in this report. The development
 proposal is being put forward as a result of demand in the area for additional educational
 facilities and the location of the proposal is ideal given its proximity to the post primary
 school.
- The proposal put forward is designed to cause the least possible disruption to the existing public road network. While it is acknowledged that there are capacity issues in the area during morning and evening peak traffic periods, the proposal put forward by The Department of Education & Skills has incorporated every available means to ensure that the development can be incorporated in the area with the least possible disruption to the existing

road network. ORS would recommend that the capacity of the road network in the area of the campus is reviewed by the Local Authority with a view to providing capacity improvement measures in the future.

6.3 MOBILITY MANAGEMENT PLAN

Mobility management is a process that is intended to be ongoing over a number of years with the end target being reduced vehicle numbers arriving and departing at peak times. Sustainable transportation should be embraced by the campus and not be seen as a chore and an anti-car approach. This report assists in providing alternative modes of transport and incentives to help promote the uptake in such forms of transport. It should be noted however that the actual monitoring and review of the initiatives proposed in this plan will be a far greater part of the mobility management plan itself.

Essential to the success of the plan is the appointment of a mobility management plan coordinator. The mobility management plan coordinator for will be Thomas O'Dróna. Thomas will be responsible for implementing the measures discussed in the plan and should be granted sufficient time and resources to help ensure the plan is a success.

The mobility management plan mainly focuses on the travel attitudes of pupils, parents, and staff and it is essential to the success of the plan that these groups are consulted from the outset. Successful coordination of tasks and communication could also be transferred to these groups if they are consulted from the onset of the implementation of the plan.

Pupils, parents and staff will play a pivotal role in the implementation of the plan as; they after all are the target audience to take an active role in the plan. The plan will evolve and develop with the campus as the culture of the campus changes, taking into account new student's needs, changing staff, and changing patterns in travel.

In order to ensure that the plan is effective and up to date it is encouraged that the stakeholder survey attached in Appendix A of this report is issued annually to establish changing travel patterns and targets. It should be noted that failing to meet targets should not be viewed as a failure, particularly in the first year to year and a half following implementation of the plan. This period should be used to recognise achievable targets and put forward long term goals.

The propensity for the teaching staff and users of the proposed campus site to use alternatives to single-occupancy car travel for their work trips will inevitably depend on the convenience and availability of those alternative networks and facilities. The campus has limited influence in

influencing the travel choices other than to ensure that facilities are in place locally and to promote their use through education and regular initiatives for the pupils.

What can, and will, make the greatest difference to modal choice and future modal shift, will be the availability of transport connections between the site and the catchment areas. The onset of the development will do nothing to prevent the advancement of those necessary and any future programmed improvements to public transport and pedestrian network infrastructure. Indeed, the further development of the campus at its current location can in fact be instrumental in bringing forward these measures since it will provide the means for public transport services to generate revenue and become increasingly viable and sustainable into the future.

6.4 ROAD SAFETY AUDIT

A Road Safety Audit was carried out by ORS Ltd, a copy of which has been provided as part of this planning application. The terms of reference / procedure for the Audit were as per the relevant sections of the National Roads Authority (NRA) Design Manual for Road and Bridges (DMRB) HD 19/15.

Ten items were raised by the Audit Team during the audit process. A copy of the Road Safety Audit report has been included as part of this planning application. All ten items have been resolved and reflected on in the design to the complete satisfaction of the Audit Team Leader. A copy of the Audit Feedback form signed by the Audit Team Leader has been provided in Appendix 9 of this report.

APPENDIX 1

Civil Drawings

Civil Drawings

DWG. No:	DRAWING TITLE	
2500	BH and TP Locations	
2501	Drainage Layout	
2502	Watermain Layout	
2503	Roads Layout	
2504	Reinstatement Details	
2505	Typical Manhole Details	
2506	Road Details/Sections	
2507	Attenuation Details	
2508	Watermain Details	
2509	Pedestrian Crossing Details	
2510	Autotrack 1 of 3	
2511	Autotrack 2 of 3	
2512	Autotrack 3 of 3	



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SECTION X-X

SLUICE VALVE CHAMBER

SECTION Y-Y

Note
Concrete floor to chamber not to be provided when Class 1 watermains are used.

400 300 PLAN ON COVER SLAB

4 T12 - 150B

80 100 150 200 250

560 560 610 690

900 900 900 900 900 1060

280 310 410 460 510 600 800

Scale @ A1:
Prepared by:
CS Project Director: MICHAEL MCDONNELL PLANNING Checked: AM FEB 2017

1:20

TYPICAL WATERMAIN DETAILS

6.1 Clondalkin Old Nangor Road Clondalkin Dublin 22

and Skills

Department of Education

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Date	07.02.17	
Description	PLANNING	
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NOTES

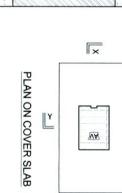
1. FIGHED DIMENSIONS ONLY TO BE TAKEN FROM THIS DRAWNING

2. ALL DRAWNINGS TO BE CHECKED BY THE CONTRACTOR ON SITE

3. ENGINEER TO BE INFORMED BY THE CONTRACTOR OF ANY DISCREPANCIES BEFORE ANY WORK COMMENCES

4. ALL LEVELS SHOWN RELATE TO ORDNANCE SURVEY DATUM

AT MALIN HEAD



500

450 400 300

510 600 800

690 690 720 800 800 1000

900 900 1050 1050 1050 1050

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PLAN ON COVER SLAP	₩	<u> </u>

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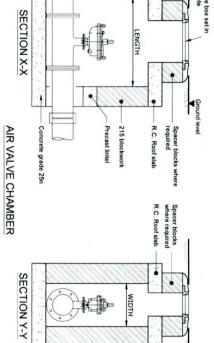
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150 250

510

PIPE DIA CHAMBER WIDTH CHAMBER LENGTH DEPTH OF COVER TO (mm) (W) (L) PIPE (H)

AIR VALVE CHAMBER DIMENSIONS



Ground level

Surface box set in concrete

R.C. Roof slab

R.C. Roof slab

×

× 7 T12 -150B

VALVE DIA. CHAMBER WIDTH CHAMBER LENGTH DEPTH OF COVER TO (mm) (V) (L) PIPE (H)

SLUICE VALVE CHAMBER DIMENSIONS

215 blockwork

215 blockwork

. Roof slab	SCOU	SCOUR SIZES
	MAIN PIPE DIA (mm)	SCOUR PIPE DIA. (mm)
5 blockwork	80 100 150	80
te valve	200	100
	250 300 350	150
watercourse or np	400 450 500	200
	600	REFER TO SPEC.

.5° D.I. Long radius bend	Natermain ————————————————————————————————————		
150		900	
H		E	
		158	
•		B	Groun
	100		Ground level
Concrete grade 25n	Gate valve To watercourse or sump	Surface box set in concrete R.C. Roof slab	
de 25n	rse or	ab set in	

TYPE 1 SCOUR CHAMBER

HYDRANT CHAMBER

SECTION Y-Y

PLAN ON COVER SLAB

Spacer blocks where required R.C. Roof slab

SECTION X-X		D)* Biograph	1		•	SCREW DOWN TYPE		Surface box set in concrete
NX-X	•	From	PI PICZ AS REQUIRED PT	· 21	· 70	on.	The second	Ground level
	Concrete grade 25n	From TEE on main line	Precast lintel	215 blockwork	R.C. Roof slab	Spacer blocks where required		-

	НУГ	HYDRANT CHAMBER DIMENSIONS	R DIMENSIONS	
VALVE DIA. (mm)	CHAMBER WIDTH (W)	CHAMBER LENGTH (L)	VALVE DIA. CHAMBER WIDTH CHAMBER LENGTH DEPTH OF COVER TO CLEAR OPE. SURFACE (mm) (mm)	CLEAR OPE. SUF BOX (mm)
50	390	720	900	375×225
80	460	960	900	575x300
100	460	960	900	575x300
450	220		200	

900	900	1500	920	150
575)	900	960	460	100
575)	900	960	460	80
375)	900	720	390	50
CLEAR OPE BOX	VALVE DIA. CHAMBER WIDTH CHAMBER LENGTH DEPTH OF COVER TO CLEAR OPE (mm) (W) (L) PIPE (H) BOX	CHAMBER LENGTH (L)	CHAMBER WIDTH (W)	(mm)
	R DIMENSIONS	HYDRANT CHAMBER DIMENSIONS	ПАН	

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<u>Y</u>	III.	Y
	<u> ×</u>	L
		Y





CS	By Chkd.	
PLANING	Description	
03.02.17	Date	
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^{Olent} DEPARTMENT OF EDUCATION AND SKILLS

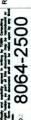
SHARED EDUCATIONAL CAMPUS OLD NANGOR ROAD CLONDALKIN

Existing Survey
BOREHOLES & TRIALPITS

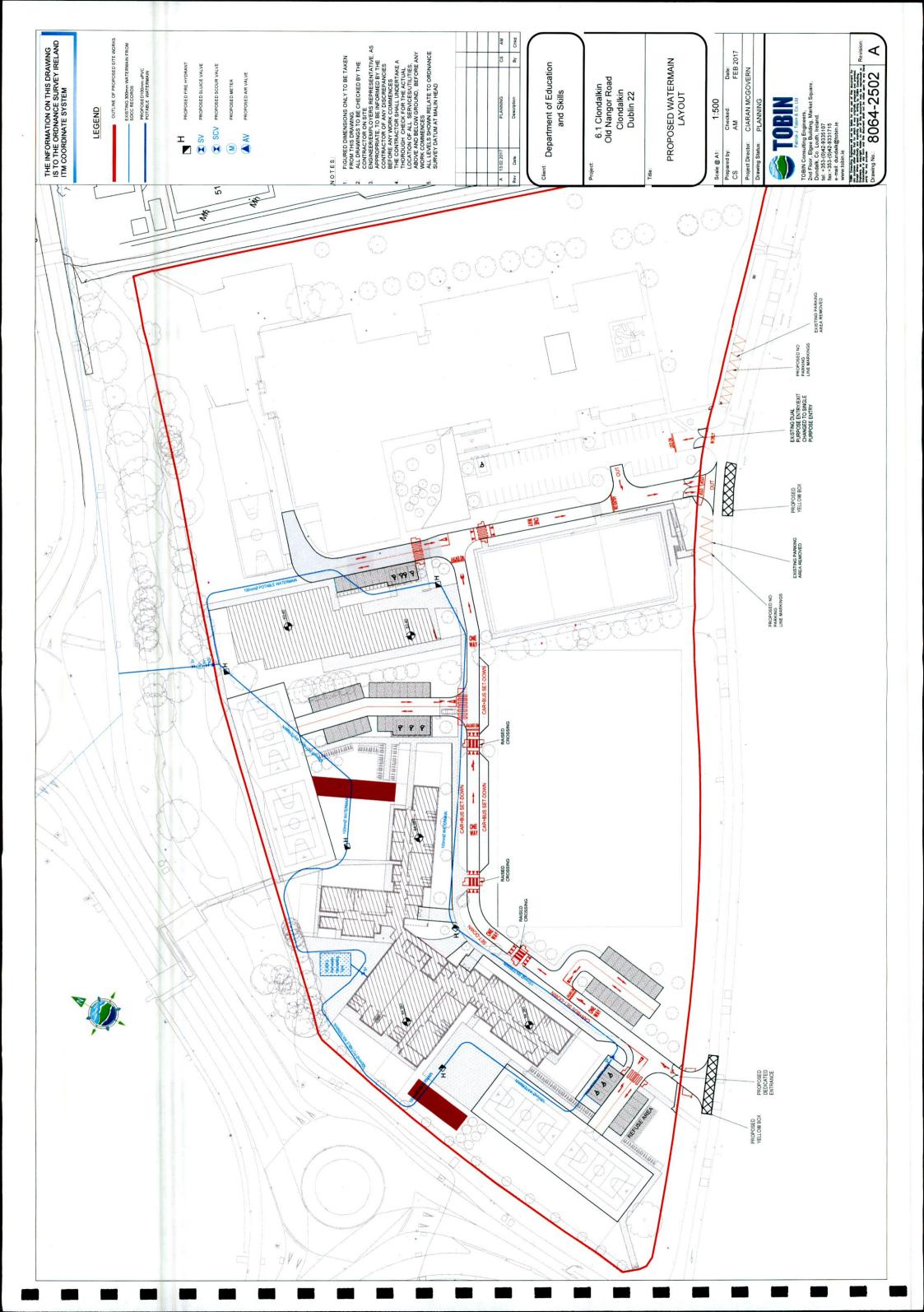
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Prepared by:	Checked:	Date:
cs	AM	FEB 2017
Project Director:	CIARAN MCGOVERN	GOVERN

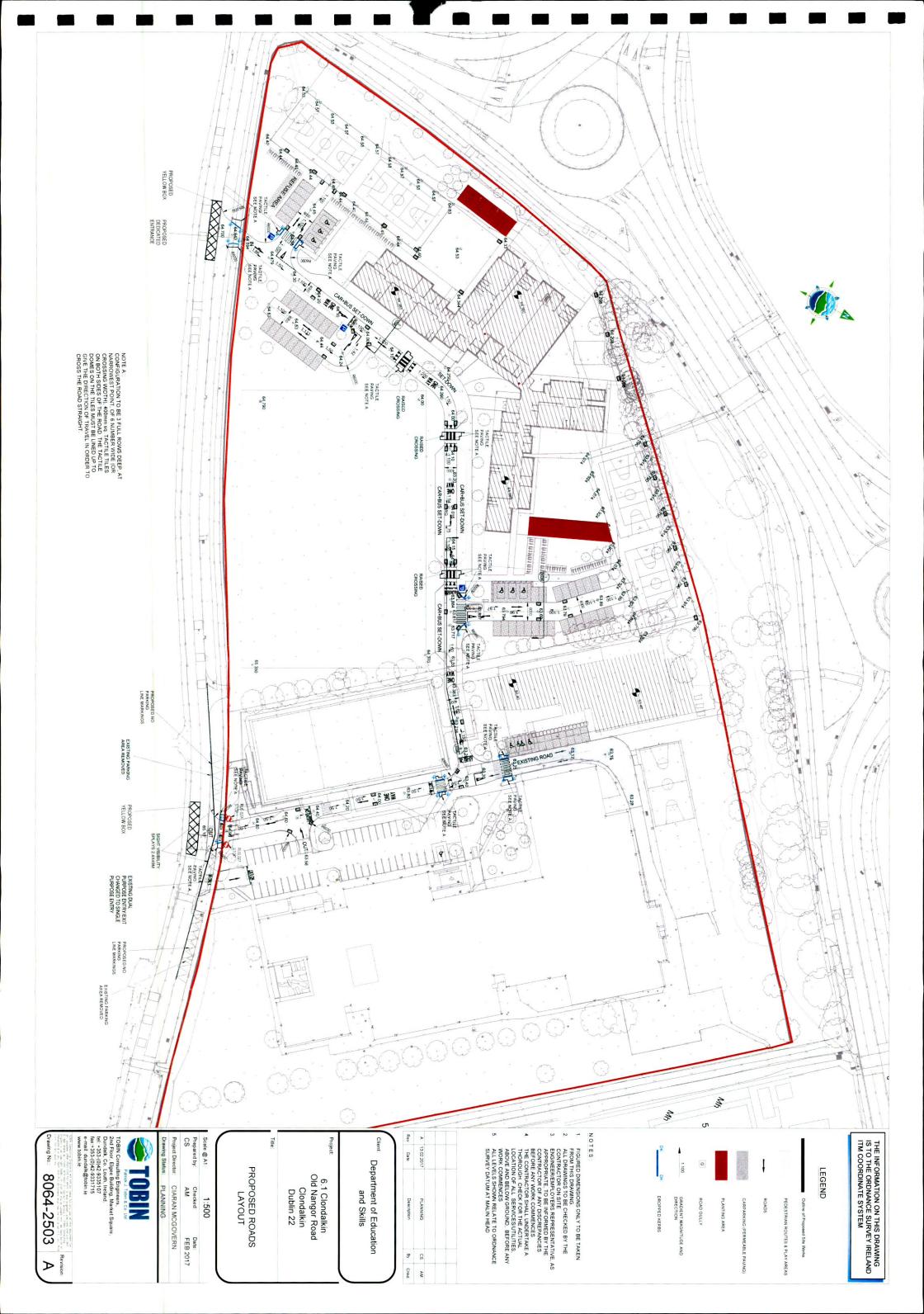


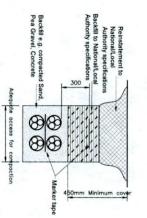
Drawing No. 8064-2500 A



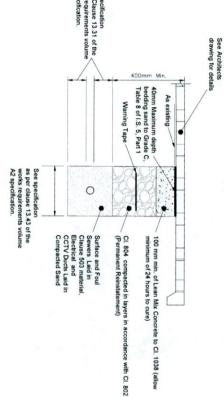






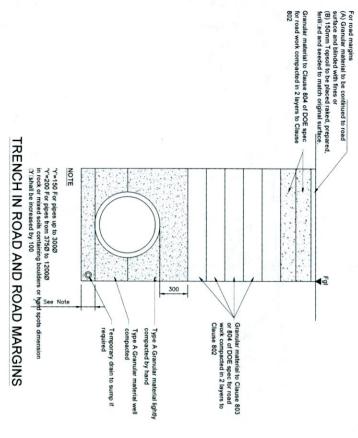


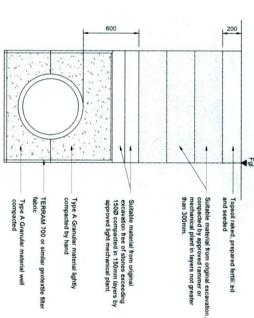
TRENCH IN FOOTWAYS, PAVEMENTS, VERGES SCALE 1:10



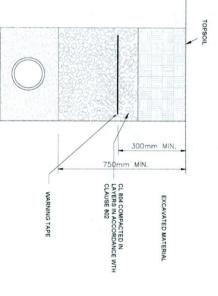
- Add fresh sand and compact with a plate compactor. Additional sand is spread to stand proud of adjacent sand.
- Use a slightly cambered profile over width of trench to counter any tendancy to settle under traffic/load.
- Relay blocks as tightly as possible.
- One pass of plate compactor, then sand and compact with two or three passes to ensure full interlock.
- 2 to 5mm joints between blocks to be filled with sand to Grade F of I.S. 5 Part 1.
- The difference in level between adjacent blocks should not exceed 3mm.

S.W & FOUL PIPE /DUCT TRENCH DETAIL IN PRECAST **BLOCK PAVING FOOTHWAYS**





(where required by poor ground conditions) FIELDS



PERMANENT REINSTATEMENT

GRASS VERGES, MEDIANS, FIELDS AND LAWNS

Prior to excavation, all grass areas are to be cut into turves which are to be carefully stacked and re-used within one week of cutting during the period 1st april to 31st august or within two weeks of cutting during the remainder of the year. Turves not used within these periods shall be regarded as

- less than 100g per sq.metre.
- 3. The areas to be grassed shall be covered with topsoil to a minimum depth of 100mm which shall be reduced to a fine tith, free from stones and debris with any dimension greater than 35mm. The topsoil shall be graded and lightly compacted to 100mm thickness whichever is greater. Any spstanding debris or stones exceeding 25mm dimension shall be removed.
- to sowing the grass seed, topsoil shall be reduced toa fine tilth. Sowing the grass seed shall be carried out by an even distribution, using a blend of (per hectare)170kg manhatlaan rye grass and 13kg dwarf clover or other mix as specified by the road authority. For slopes in excess of ten degrees, surface of the topsoil. nese quantities shall be increased by 50⊡. The seed shall be covered by lightly raking into the sowing grass seed. Imeediately prior
- runoff is discharged from the road
- All temporary reinstatement as detailed above shall be carried out immediately after backing the trench. When all settlement has taken place or after a three month period, whichever is the greater. the trench shall be topped up with topsoil to its original level.

NOMINAL PIPE DIA	MIN. TRENCH WIDTH MAX	MAX. TRENCH WIDTH
(mm)	(mm)	(mm)
100	430	630
150	490	690
225	580	780
300	680	880
375	950	1150
450	1030	1230
525	1120	1320
600	1240	1440
675	1330	1530
750	1400	1600
900	1920	2120
1050	2100	2300

	Description	Date	Rev
CS AM	PLANNING	08.02.17	Þ

	Client:
and Skills	Department of Education

6.1 Clondalkin Old Nangor Road Clondalkin Dublin 22

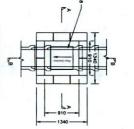
TYPICAL DETAILS FOR ROAD REINSTATEMENT AND TRENCHES

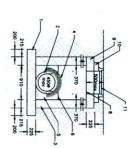
Title

VERN	CIARAN MCGOVERN	Project Director:
Date: FEB 2017	Checked: AM	Prepared by: CS
	AS SHOWN	Scale @ A1:



Revision: 8064-2504 A

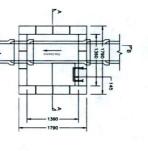




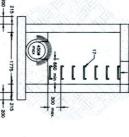
TYPE A MANHOLE

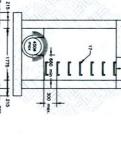
MANHOLE DETAILS FOR PIPE Ø 150,225,300,375,450. DEPTH TO INVERT DIM.

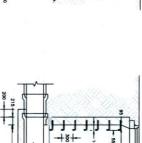
SECTION B-B



TYPE B MANHOLE SECTION A-A

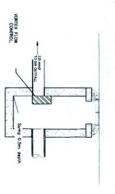




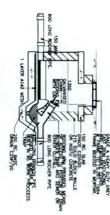


SECTION B-B





SURFACE WATER FLOW CONTROL CHAMBER SCALE 1:25



TYPICAL SECTION THROD MANHOLE INCORPORATING INTERCEPTOR, SCALE 1:20 FOR TIEING INTO COMBINED DRAIN



ROAD GULLY DETAIL SCALE 1:20.

Drawing Notes:
225mm thick Cl. 20N/20mm Mass Concrete Foundations.
225mm thick Cl. 20N/20mm Mass Concrete Foundations.
Performed half circle channel pipes. The pipeline may, where racticable, be laid through the manhole and the crown cut out to half ameter, provided flexible joints are situated on each side no further tames, provided flexible joints are situated on each side no further tames of manhole wall.

3) Manhole construction.
4) Manhole construction.
5) Manhole construction.
6) For Surface Water Manholes high-density blocks to CLS10 of IS.20 Part 1:1887 or CL 30N/20nm insitu concrete.
6) Block work shall be bedded and jointed using mortar to IS406. Beds and vertical joints shall be ecompleted as the work proceeds.
6) Usints shall be flush pointed as the work proceeds.
6) Usints shall be flush pointed as the work proceeds.
6) Water Manholes must be faced in solid Engineering Brick (minclass A or B), or insitu concrete for 1 metre above Benching Level.
6) Reflexing arch formed by 215x103x65 solid engineering brick Class A or B as per drawing.
7) Reflexing arch formed by 215x103x65 solid engineering brick Class A or B as per drawing.
7) Reflexing arches used in brick or block work manholes extend over full thickness of wall.
7) Standard his to be formed for pipe diameters greater than 600mm.
7) Benching and pipe channel pipe surround – Cl. 20/20 concrete.
8) Benching finished in 2:1 sand-cement mortar with a smooth trowel finish, at 1 in 30 slope towards channel.
7) Standard rungs at 300c/c vertically and galvanized to the latest version of B.S. 729 or equivalent. Note: Steps Irons are not acceptable.
8) Blochma square ope in roof slob.
9) Precast R.C. Roof Slob shall be 200mm thick in Class 30N/20mm, with 40mm cover to steel.
10) 1 to 2 courses of solid engineering bricks Cl.B to 1.5.91:1983 set in 1:3 (cement and mortar).

(cement and mortar).

(1) Class D400 or E600 manhole cover and frame to IS/EN 124, 150mm 11) Class D400 or E600 manhole cover and frame to roads and 100mm deep for footpaths and green areas. Non-rock design, closed keyways, manufactured from spheroidal graphite cost iron (ductile cost iron), 600 x 600 (600diam), clear opening, cover and frame coated in bitumen or other approved material, cover to have a minimum mass of 140kg/m2, frame bearing area shall be 80,000mm2 min, frames shall be designed to prevent covers falling into manhole. Frames shall be bedded on approved mortar to manufactures instructions. Instructions.

12) Short length pipe and pipe joint external to manhole shall not exceed 600mm from the inner face of manhole wall.

13) Toe holes of 230mm minimum depth and galvanized steel safety railings to be provided in benching of sewers greater than 525mm diameter and depth to invert v3m for access to invert.
14) A safety chain is to be provided on pipes that exceed 450mm in diameter. Mild safety chain shall be 10mm nominal size grade M(H) non-colibrated chain, type 1, complying with B.S.4942 Part 2 or equivalent.

adder stringers should be adequately supported from the manhole wall evals of not more than 2.0m stringers should be boited to cleats to ladders should meet the dimensional requirements of B.S.4211 or en depth of manholes to invert is greater than 3.0m ladders shall be istead of rungs to B.S.4211 or equivalent except that stringers be not less than $65\times12\text{mm}$ in section and rungs 25mm in

Mill ladders, rungs, handrails, safety chains etc shall be hot dip vanized to B.S.729 or equivalent.

Pipe should be cut flush with the inside surface of the manhale wall so the channel extends the full length of the manhale (except for precast the channel extends the full length of the manhale (except for precast the channel extends the full length of the manhale (except for precast the channel extends the full length of the manhale (except for precast the channel extends the full length of the manhale (except for precast the channel extends the full length of the manhale (except for precast the channel extends the full length of the manhale (except for precast the channel extends the full length of the manhale (except for precast the channel extends the full length of the manhale (except for precast the channel except for precast the channel extends the full length of the manhale (except for precast the channel extends the full length of the manhale (except for precast the channel except for precast the channel extends the full length of the manhale (except for precast the channel extends the full length of the manhale (except for precast the channel extends the full length except for precast the channel extends the full length except for precast the full length extends the full

19) Position of 910 square ope in intermediate roof slab.
21) Position of 910 square ope in intermediate roof slab.
22) Position of 910 square ope in intermediate roof slab.
23 Finish to Reinforced Concrete and Mass Concrete shall comply with Class 2, Section 6.2.7, B.S.8110: Part 1: 1997.
25 Finish to the top of slabs shall comply with Type A, Section 6.2.7, B.S.810: Part 1:1997.
26 Finish to the top of slabs shall comply with Type A, Section 6.2.7, B.S.810: Part 1:1997.
27 Finish to the top of slabs shall comply with Type A, Section 6.2.7, B.S.810: Part 1:1997.
28 Finish to the top of slabs shall comply with Type A, Section 6.2.7, B.S.810: Part 1:1997.
29 Finish to the top of slabs shall comply with Type A, Section 6.2.325 block work design code taking granular fill pressure and H.B. surcharge.
20) For maniholes >3m depth to invert use 30N/20mm insitu concrete.
20) For maniholes >3m depth to invert use 30N/20mm insitu concrete.
20) For maniholes >3m depth to invert use 30N/20mm insitu concrete.
21) For Pre cost Manholes, Chamber walls and cover slab to be constructed to S EN 1917 and IS 420 2004
22) Manhole Openings to be situated furthest from the nearest Carriageway.
22) Manhole steps / access to be positioned to allow viewing of ancoming traffic.

For bedding and sealing of Chamber rings, er slab) and bottom ring to be bedded with mediate rings, joints to be sealed with approximations. the top ri cement m roved pre-

24) Pre cast Manholes to be surrounded with a minimum of 150mm thick Grade C20/40 concrete General Notes

(3) All brick to be Solid Engineering Brick Class A or B.

(4) For pipe diameter >750mm use manhole with internal diameter size = pipe size + 1 metre + 300mm, use manhole with internal diameter size = maximum of 500mm.

Description	Date	Rev	n of 150mm thick	0
PLANNING	08.02.17	>	ned jointing	-Torn
			r. For	norto
			ring (to Pre cast	gni
		I	g of oncoming	9
			st Carriageway.	egre

By Chkd. CS AM

Client Department of Education and Skills

6.1 Clondalkin Old Nangor Road Clondalkin Dublin 22

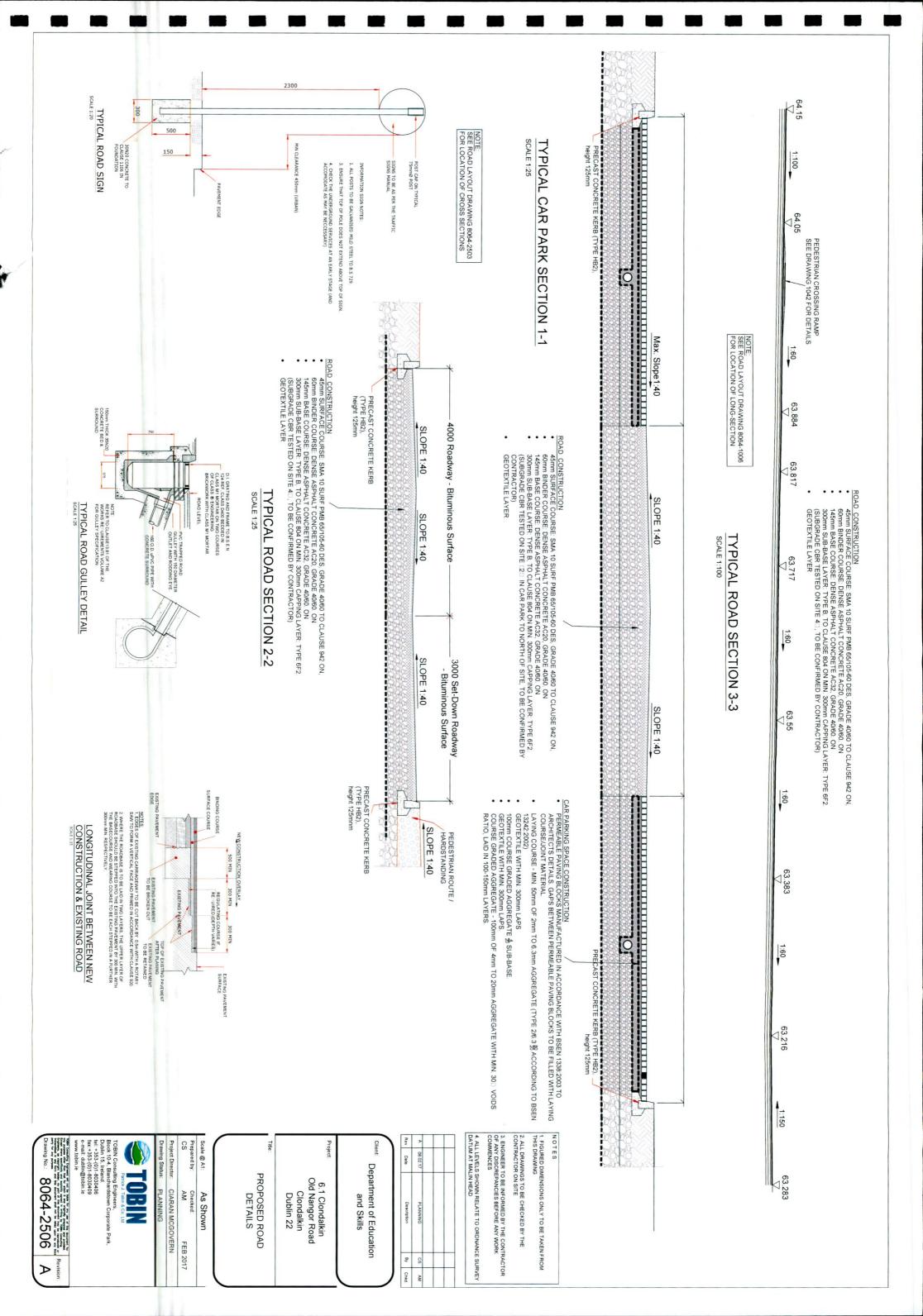
TYPICAL DRAINAGE MANHOLE DETAILS

Prepared by: CS Scale @ A1: Project Director: CIARAN MCGOVERN PLANNING Checked: 1:15 FEB 2017



Block 10-4, Blanchardstown Corporate Park, Dublin 15, Ireland, 535-(01)-8030409
wal: 435-(01)-8030409
mail: dublin@obin.ie
ww.tobin.ie

Proving No.: 8064-2505 A





TOBIN Consulting Engineers,
Block 10-4, Blanchardstown Corporate Park,
Dubin 15, Ireland.
Lei: +353-(0)1-8030405
tex: +353-(0)1-8030409
e-mail: dubin@obin.ie

Patrick J. Tobin & Co. Ltd

Project Director: Ciaran McGovern
Drawing Status: PLANNING

Scale @ A1: Prepared by: CS As Shown
Checked: Date: FEB 2017

DETAILS OF ATTENUATION STORM NETWORK

6.1 Clondalkin Old Nangor Road Clondalkin Dublin 22

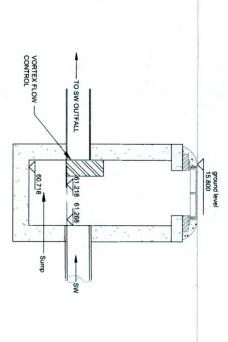
Department of Education and Skills

Rev Date A 07.02.17 Description PLANNING By Chkd. CS AM 1. FIGURED DIMENSIONS ONLY TO BE TAKEN FROM THIS DRAWING.
2. ALL DRAWINGS TO BE CHECKED BY THE CONTRACTOR ON SITE ENGINEERICATIVE. AS APPROPRIATE, TO BE INFORMED BY THE CONTRACTOR OF ANY DISCREPANCIES BEFORE ANY WORK COMMENCES

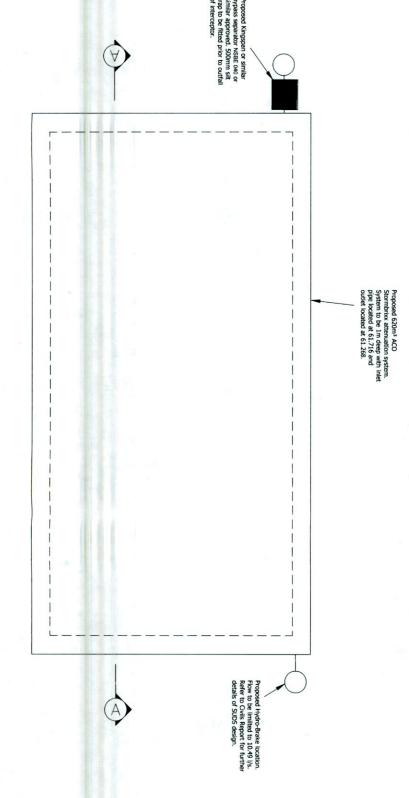
4. ALL LEVELS SHOWN RELATE TO ORDNANCE SURVEY DATUM AT MALIN HEAD

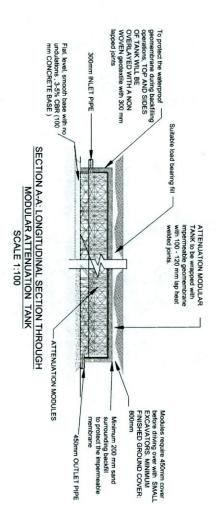
NOTES

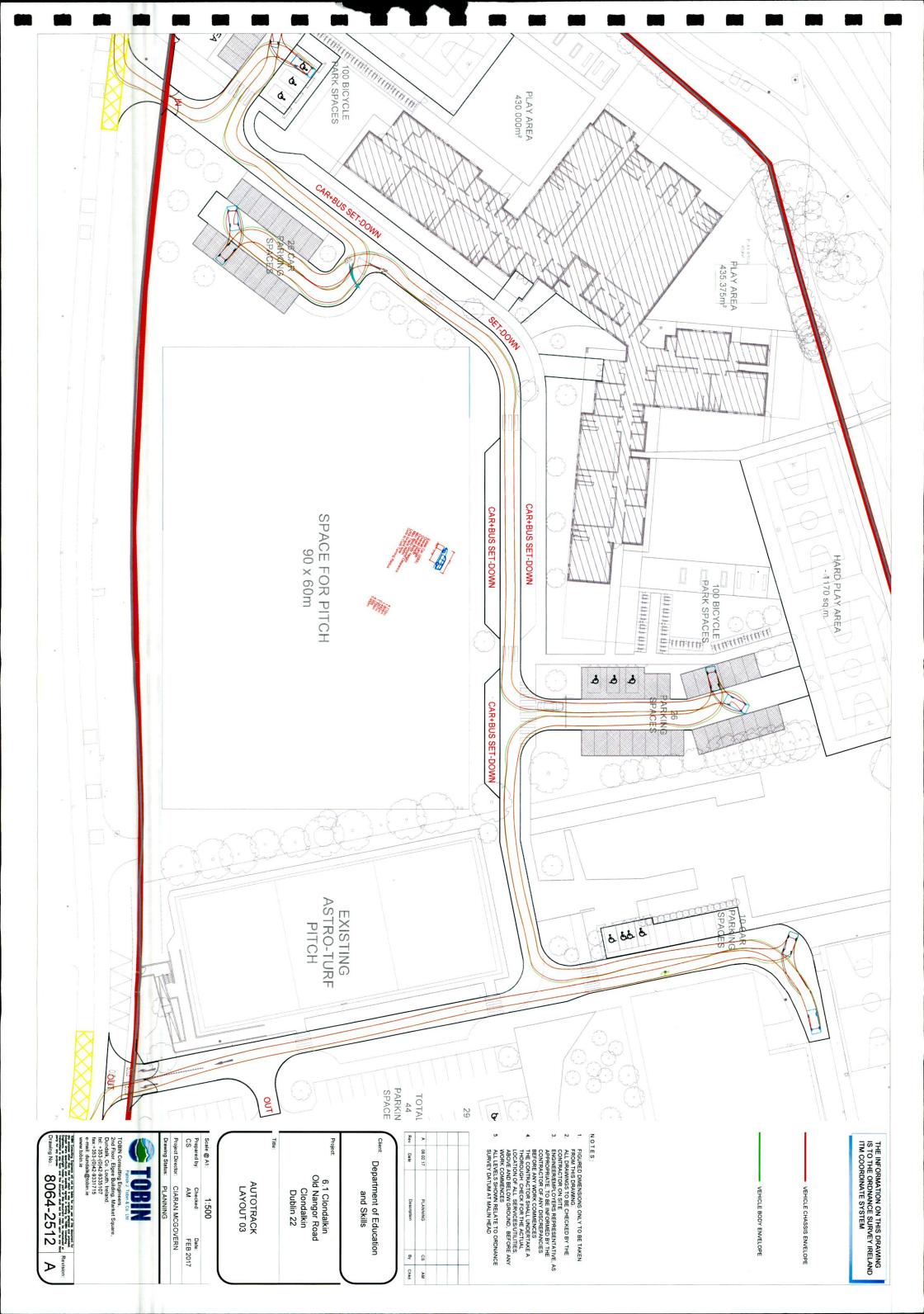
SURFACE WATER FLOW CONTROL CHAMBER SCALE 1:25

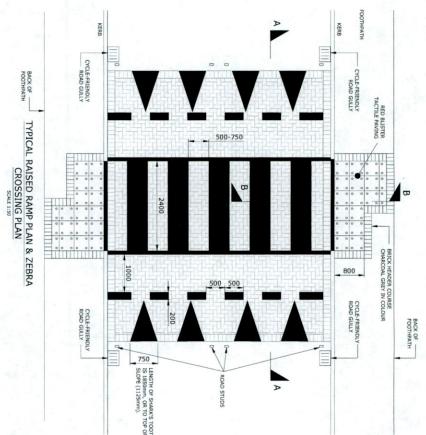


PLAN OF ATTENUATION SYSTEM - STORM NETWORK SCALE 1:100









TYPICAL TACTILE PAVING AT ZEBRA CROSSING PLAN

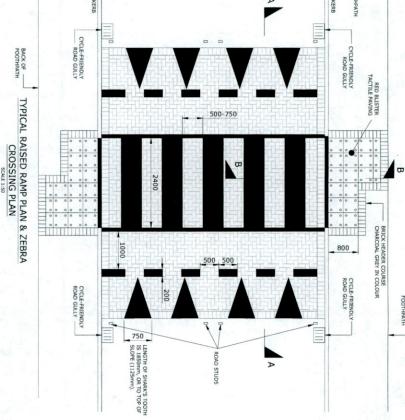
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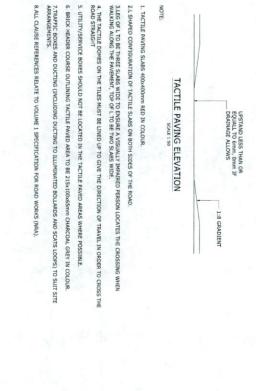
2400

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1:12 GRADIENT MAX

400x400x50mm RED BLISTER TACTILE PAVING LAID ON A 25mm DEEP 3:1 CEMENT MORTAR BED

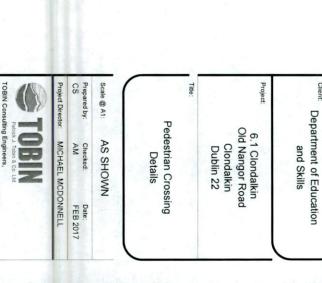




07.02.17 Date

PLANNING

By Chkd. CS AM



The Control (speem at which have been as of the second of the control of the cont

1000

RAMP SHAPED WITH DENSE BASE COURSE MACADAM

D.B.M WEARING COURSE (nom 14mm AGGREGATE) RED IN COLOUR AND THE SURFACE IMPRINTED IN HERRINGBONE PATTERN

COLD PLANE/BREAK OUT 1 m x 0.05m OF EXISTING WEARING COURSE AT EACH TOE OF RAMP

RAMP SHAPED WITH DENSE BASE COURSE MACADAM

925

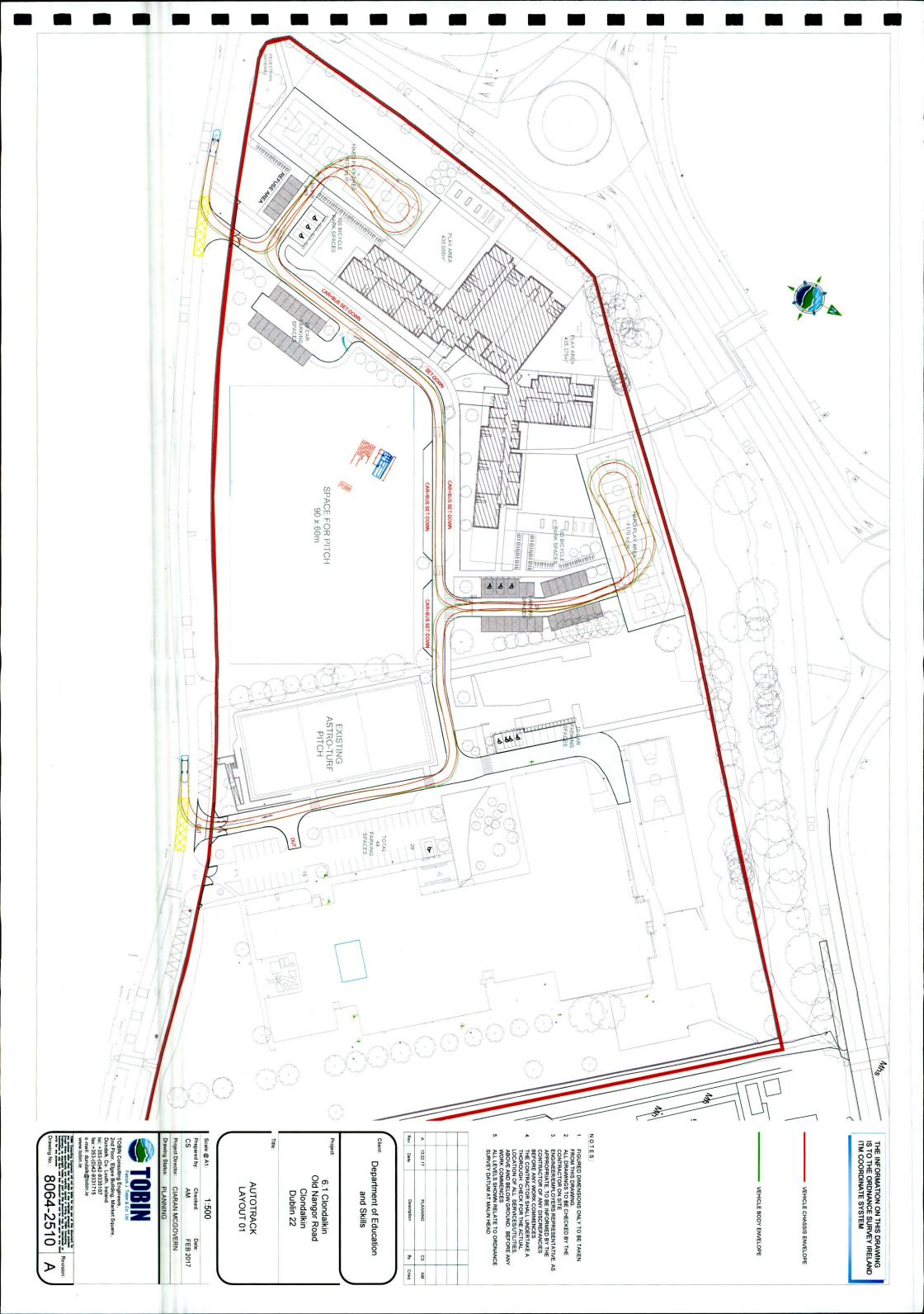
925

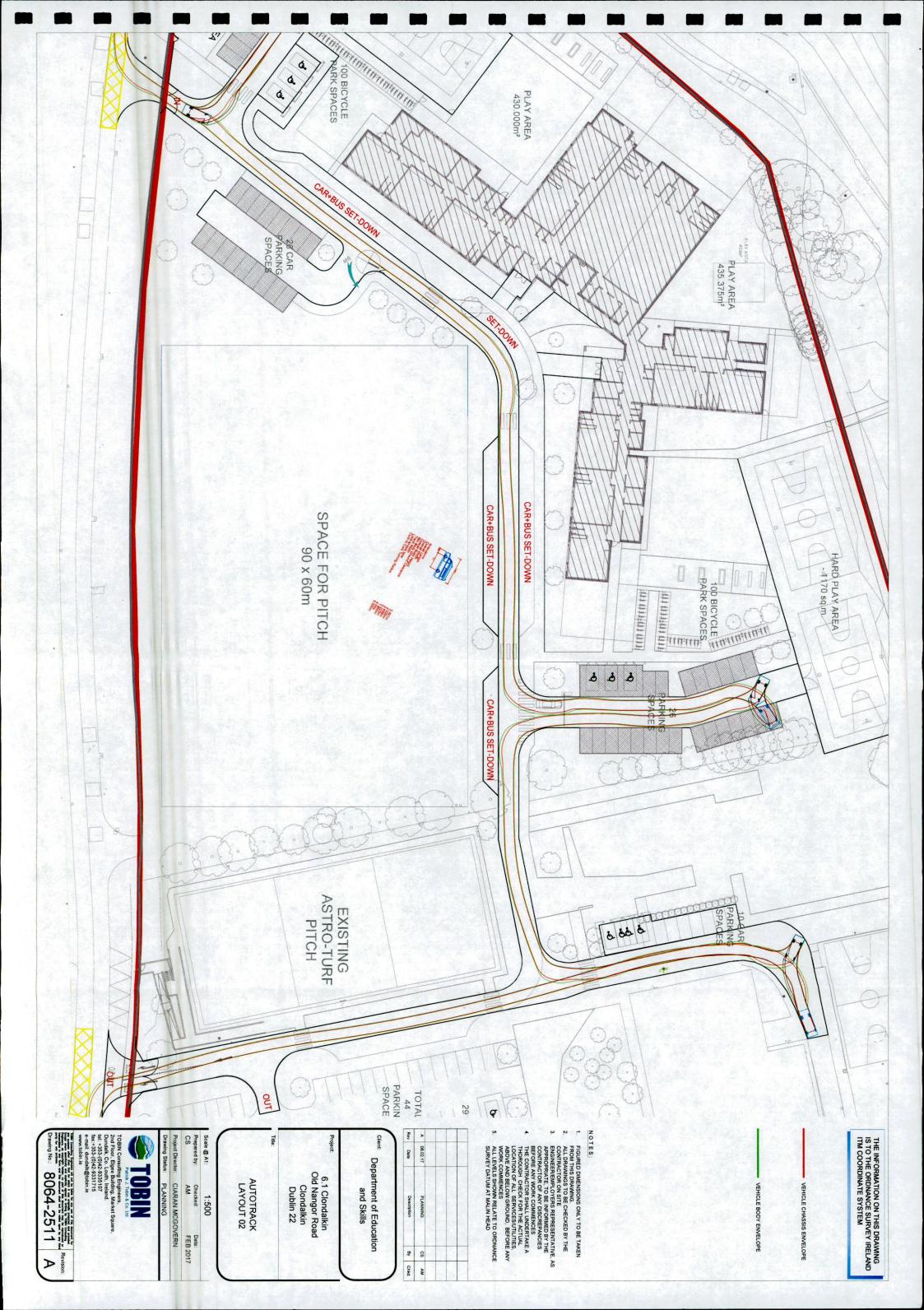
TYPICAL RAISED RAMP DETAIL SECTION A-A SCALE 1:20

1000

TYPICAL RAISED RAMP CHANNEL DETAIL SECTION B-B SCALE 1:20

1000





APPENDIX 2

Water Demand Calculations



	CALCULATION SHEET	Ref No:	8064
PROJECT:	ADAP Lot 6 Clondalkin	Sheet No:	1
TROCEST	ADAF Eot o Ciondalkin	Designer:	CS
ELEMENT:	Potable Water Demand	Date:	04/08/2016

File Location: \FSERVER4-DUB\Tobin\Projects\8064 - ADAP Lot 6 - Drumcondra & Clondalkin Schools\05-

This Element: Potable Water Demand

Potable Supply for Domestic Use

Design Population

Site	Max. No. Staff & Students	Max. No. Visitors	Total
AD Plant	1000.0 persons	10.0 persons	1010.0 persons

Staff & Students Water Usage Rate
Visitor Water Usage Rate

60.0 l/day/person (See Note 2)
10.0 l/day/person

Demand

	EPA Design Guidelines
Avg. Daily Demand	0.123 l/sec
Peak Demand	0.307 l/sec

3866.88 m3/annum

Potable Supply for Firewater

Demand

Peak Demand	37.500 l/sec	(See Note 3

Pipe Sizing

Ø	velocity
100	4.81 m/s
150	2.14 m/s
200	1.20 m/s
250	0.77 m/s

Therefore, use 150 mm diameter watermains

Notes

- 1. Pipe sizing uses an average velocity of v = 1.2 m/s
- 2. The Flow rates are obtained from Table 3 Wastewater Treatment Manuals (pg.8).
- 3. Guidelines on flow requirements for developments served by Dublin Fire Brigade Class II
- 4. Wavin Polyethylene Water Systems Technical Guide max. velocity = 5.0 m/s

APPENDIX 3

South Dublin County Council Correspondence

Craig Scully

From: Michael McAdam [mmcadam@SDUBLINCOCO.ie]

Sent: 10 August 2016 12:53

To: Craig Scully Cc: Aongus Bates

Subject: FW: Pre-connection Enquiry Form Attachments: School Old Nangor Road.jpg

Craig,

In relation to queries 1 and 2, please note John's comments, as follows;

A 300mm main runs to the north of the site, this is connected to a 600mm trunk main.

There's plenty of capacity in terms of peak demand flow.

The only way to ascertain if fire flow is adequate (35 l/s at any single hydrant for a community school) is to conduct a flow test on a hydrant.

We will carry out a test and let you know.

Please note the comments from Gabrielle, as per her email earlier in relation to point 3;

The school can connect into a manhole on the existing 750mm/900mm sewer at the NE corner of the existing school (see map attached).

The sewer is approximately 8m below ground at this location.

If you decide to connect through the existing school grounds and written permission will be required if this property is not in the same ownership as proposed development.

There are no problems with foul capacity.

Regards, Michael

From: Craig Scully [mailto:Craig.Scully@tobin.ie]

Sent: 09 August 2016 11:35

To: Michael McAdam < mmcadam@SDUBLINCOCO.ie>

Cc: Aongus Bates < Aongus.Bates@tobin.ie > Subject: Pre-connection Enquiry Form

Dear Michael

I am writing to you to issue a pre-connection enquiry form for the Shared Educational Campus (Gaelscoil na Camoige, Gaelscoil Chluain Dolcain and Colaiste Chillian) Clondalkin, Dublin 22. We spoke with Oliver Fogarty in Irish Water who directed us to South Dublin County Council.

Just to provide you with a bit of background on this project, two new schools with a combined capacity of 1000 students and staff are to be constructed adjacent to the existing Coliaste Chillian school.

Our main queries are to clarify the following:

- 1. The flow and pressure for potable water is adequate
- 2. The flow and pressure for fire fighting is adequate
- 3. The capacity of the existing public sewer is adequate

We would appreciate if you could confirm the above. If there are any queries or clarifications required, please do not hesitate to contact us.

Kind Regards

APPENDIX 4

Attenuation Calculations and Specification

Stormwater Storage and Control Calculations

INPUT OUTPUT Institute of Hydrology Report No. 124 for Sites Up To 24 Ha Greater Dublin Strategic Drainage Study

SITE DETAILS:

Location	Clondalkin	Old Nangor	Old Nangor Road			
Site Area	7.50 Acre	3.04	На		30,352	m^2
Impervious Area Drainin	55%	16,693	m ²			
Impervious Area Drainin	0%		m ²			
Pervious Area		45%	13,658	m ²		
Allowance for Imperviou	is Green Area	0%	-	m^3		

RIVER REGIME PROTECTION

Allowable Discharge From Site: QBAR = $0.00108 \text{ x AREA}^{0.89} \text{ x SAAR}^{1.17} \text{ x SOIL}^{2.17}$

Q_{BAR:} Mean Annual Peak Flow From Site m³/s

AREA: Area of Site km²

SAAR: Standard Annual Average Rainfall 820 mm

SOIL: Soil Index SOIL TYPE 4 SOIL

1	0.1	Very Low	Sandy, well drained
2	0.3	Low	Intermediate Soil (silty)
3	0.37	Moderate	Intermediate Soil (sandy)
4	0.47	High	Clayey, poorly drained
5	0.53	Very High	Steep, rocky area

Rainfall Intensities
Climate Change F 10%

0.370

QT estimated from old data where not specified by

If site is <50Ha, calculate Q-Bar for 50Ha and linearly interpolate for Site Area

QE	BAR 50 H	a - STANDA	RD	Return Period	QT Factor	Q _{ALL}	Q _{ALL}	V
AREA	Ha/Km2	50	0.5	Yrs		l/s	l/s/ha	m ³
Q _{BAR}	=	0.1728	m^3/s	1	0.85	8.92	2.94	182
Q _{BAR}	=	172.85	1/s	2	1	10.49	3.46	200
Q _{BAR}	=	3.46	l/s/Ha	5	1.3	13.64	4.49	285
QBAR	Developm	ent - REST	RICTED	10	1.7	17.84	5.88	312
AREA	Ha/Km ²	3.035	0.0303515	20	1.9	19.94	6.57	402
Q _{BAR}	=	0.0105	m^3/s	30	2.1	22.03	7.26	444
Q _{BAR}	=	10.49	1/s	50	2.31	24.24	7.99	487
Q _{BAR}	=	3.46	l/s/Ha	100	2.6	27.28	8.99	610

Interceptor Designed YES Flow Control Designed at Outlet Manhole with overflow YES

Contents list Design Suppo

Project references

Home

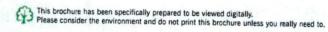
Print





Stormwater attenuation and infiltration system Interactive digital brochure







ACO StormBrixx is a unique and patented plastic geocellular stormwater management system. Designed for surface water infiltration and storage, its versatility allows it to be used in applications across all construction environments as a standalone solution or as part of an integrated sustainable urban drainage (SuDS) scheme.

What is ACO StormBrixx?

Plastic geocellular systems are a widely accepted method of creating infiltration and attenuation systems throughout the UK. They have been installed in a variety of applications for a number of years.

One drawback of these types of systems is an overall lack of accessibility for maintenance. Improving accessibility would enable Local Authorities and Water Companies to adopt them.

The Flood and Water Management Act 2010 now gives overall ownership responsibilities for SuDS systems to Local Authorities in England and Wales. As part of the National Standards within the Act, adopting authorities are required to maintain and ensure on going opperation of all sustainable fortianage systems - requirements which cannot be met by most current geocellular systems. Specifiers for projects in Scottland should refer to Sewers for Scotland 2nd Edition and SEPA for guidance on the specification of Sustainable Drainage Systems.

ACO StormBritor addresses the primary adoption needs of the Local Authorities by providing true 3D access for inspection and maintenance, whilst retaining the structural integrity of the installation.

The system can form part of the design of any integrated drainage scheme, such as open parking areas, commercial premises, retail or residential developments.

Designed and manufactured in accordance with CIRIA C680, in 2014 ACO StormBritor was awarded BBA



The ACO StormBrixx system

The ACO StormBrixx system consists of a single recycled polypropylene body that can be assembled in a variety of ways to form an open bonded structure.

form an open bonsed structure.

ACO StormBriox's unique pillar
configuration gives a high void ratio of
95%. This minimises the excavation
required to achieve a specified storage
capacity, reduces the aggregate needed
for bacidiling, and improves the flow
characteristics of runoff through the
installed tank).

ACO StormBritz benefits from a patented cell brick and cross bonding feature which provides unparalleled stability in the construction of the tank. Where brickbonding is not used or for multilayered tean structures, connectors are available to support the integrity of the structure.

Additional accessories available include inspection point and pipe connectors, geotextiles and geo-membranes, as well as a 600 x 600mm access chamber for full inspection and maintenance.

ACO StormBrisz can be configured to minimise silt accumulation and has the added feature of a low flow and drain down facility ensuring that the system can be properly maintained throughout its life.



Contents list Design Support Project references Home Print < >

System benefits explained

- Brick bonded and cross bonding stacking for optimum stability
- Low flow, draindown and silt management facility
- 3D inspection access to tank interior
- Environmentally efficient solution minimising carbon emissions in manufacture, transportation and
- High void ratio minimises excavation volume
- Fully certified performance
- BBA certified in accordance with CIRIA C680
- Manufactured from recycled and recyclable polypropylene
- Suitable for all industrial, commercial and residential applications including highways

Structural integrity

The ACO StormBrixx system has been independently tested to certify the structural integrity and the long term life expectancy of the system.

The patented brickbonding and cross bonding feature provides a strong, long term installation and also helps to improve the construction speed of the tank.

Click here for a short demonstration

Access and maintenance

ACO StormBritz addresses the fundamental requirement of access and maintenance for SuDS Approval Boards. (SABS) and water companies. The open cell structure permits completely free access for CCIV and jetting equipment which allows the whole system, including all the extremities, to be inspected and maintained from just a few access policy.

Click here for a short demonstration

Simplified handling and logistics

ACO StormBrico simplifies delivery, site logistics and installation as a result of its stackable design. Each single injection moulded body nestles, optimising logistical and installation cost significantly, thus helping to reduce the carbon footing of the switch.

Click here for a short demonstration.



Visit www.stormbrior.co.uk for further informatio on ACO StormBriox including a full system demonstration, installation movies and much more. Help with specification, design or installation can also be found here.





ACO StormBrixx attenuation and infiltration system layout

ACO StormBriss has a range of key features which are common to both alternuation and infiltration systems and are listed below. ACO StormBrics attenuation and infiltration systems also have a set of features specific to their configuration. These features are highlighted on the product images below.

- ACO StormBriox can be assembled in variety of different lank configurations to satisfy installation and site requirements.

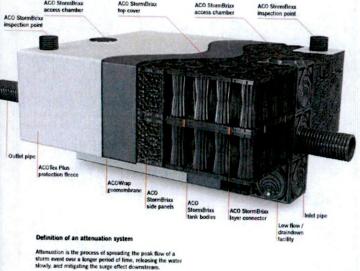
 The patented brickbonding and crossbonding feature delivers a strong and robust tank installation.

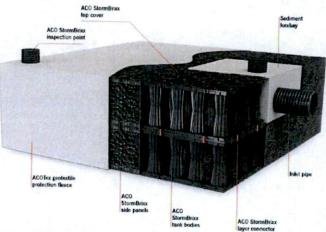
- e open cell structure provides nple access for remote CCTV and sintenance equipment to inspect all rets and areas of the system

- Delivery, site logistics and installation are all dramatically simplified, as a result of the system's stackable design. A clip-in 3-way connector improves the structural integrity of multilayered lank structures and where brickbonding is not used.

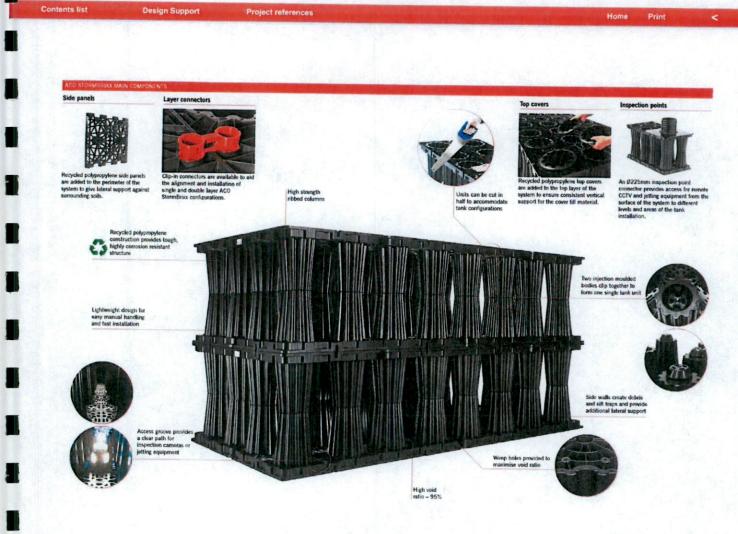


ACO StormBrixx attenuation system feat





Definition of an infiltration system



ACO StormBrixx access chamber

The access chamber is designed to provide complete 3D access to any ACO StormBriax system for simple inspection and maintenance. The modular stackable chamber is designed to be incorporated into any ACO StormBriax attenuation or infiltration system, and forms an integral part of the system's overall volume, removing the need for expensive upstream catch pit maniholes.

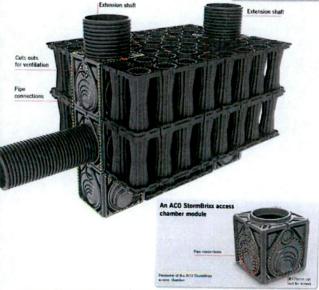
Each ACO StormBriox access chamber module provides 150mm, 225mm, 300mm and 375mm inlet and outlet pipe connections, reducing the need for expensive and time-consuming manifold connections.

consuming maintoit connections. A 375mm cut can be made in the AOO StomBrist access chamber module to enable complete inspection of all levels and areas of the system, A 100mm or 150mm vent can be created by termoving the cut outs provided in the top half of the access chamber.

Cover and frame

A Load Class D 400 Ø450mm solid ductile iron cover and frame is available to complete the ACO StormBrixx access chamber installation.





Cutting the unit for pipe



Inlet and outlet pipe connections are provided on each side of the access chamber module. Depending on the pipework requirements, cut and memore the appropriate panel. Recessed cutting lines are provided for guidance. Secondly remove 375mm panels from each side of the unit requiring access.

Building the access chamber



Once the bases of the upper module(s) have been removed, simply stack the units on top of each other ensuring that each module is clipped to the main structure using the ACO StormBriox layer connectors.

Making pipe connections



Cutting the base for a multi layered access chamber





Once the main access chamber has been constructed it will be necessary to add a 450mm ID raising piece cut to length and placed over the top of the access chamber unit.

The access chamber enables all levels and areas of the AGO StormBrixx structure to be inspected by either tracked or push nod CCTV inspection equipment. Where required, the AGO StormBrixx system can be jetted using standard equipment.

When the ACO StormBrico access chamber has been configured to create a low flow draindown channel (see opposite) or a sill trap (see page 19), the unit allows for the removal of sill and debris.

