

Oak Lodge,
New Road,
Clondalkin
Dublin 22 D22 F516

Engineering Soakaway Design
Calculations
Reg Ref SD21B/0530

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SCD Consulting
Engineering & Management

Report: **Engineering Soakaway Design Calculations**

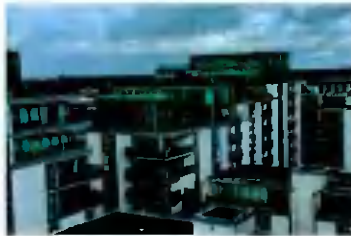
Project: **Proposed Development at Oak Lodge, New Road,
Clondalkin, Dublin 22 D22 F516**

Client: **Thomas & Hazel O'Reilly**

Project No: **100-30 - Additional Information
Planning Reg. Ref. D21B/0240**

Date: **March 2022**

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March 2022



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Proposed Development
Oak Lodge
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Dublin 22 D22 F516

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Document History: -

ISSUE	DATE	DESCRIPTION	ORIG.	PM	ISSUE CHECK
P1	Mar 2022	Issued for Add. Information	SD	SCD/PH	-

Contents

1.0 SCD Soakaway Design Calculations

Calculation Sheet



Project No: 100-30
 Client: THOMAS & HAZEL REILLY
 Project: DAK LODGE, CLAYKIN
 Calc'd by: SD

Date: MAR 22
 Checked: PH
 Pages: 1 OF 3

SOAKAWAY DESIGN CALC

Output

SOAKAWAY PIT TESTS - DATED 5TH MARCH 2022

EXCAVATE TRENCH 3m LONG X 0.6m WIDE X 1.5m DEEP

300x300x300 DEEP TEST HOLE BELOW 1.5m DEPTH

TEST NO 1: HOLE FILLED @ 10AM
 75% - 25% DEPTH = 4 MINS
 TIME TO EMPTY = 10 MINS

* SEE PHOTO RECORD APPENDIX 'A'

TEST NO 2 HOLE FILLED @ 10.30 AM
 75% - 25% DEPTH = 6.5 MINS
 TIME TO EMPTY = 15 MINS

TEST NO 3 HOLE FILLED @ 11.00 AM
 75% - 25% DEPTH = 7 MINS
 EMPTY = 19 MINS

∴ T₁ = 4 mins
 T₂ = 6.5 mins
 T₃ = 7.0 mins
 T_{MAX} = 7 mins

AREA OF ROOF & IMPERMEABLE AREA TO SOAKAWAY

ROOF AREA = 164m²

IMPERMEABLE = 41m²

TOTAL = 211m²

RETENTION PERIOD = 30 YEARS

FROM MET OFFICE CLIMATE DATA (SEE APPENDIX 'B')

MS-60 = 17.0mm
 MS-2DAY = 62.2mm
 ⇒ f = 17 / 62.2 = 0.273

Calculation Sheet



ENGINEERS IRELAND

Project No: 100-30
 Client: THOMAS & HAZEL REILLY
 Project: OAK LODGE, CLONGRACKIN
 Calc'd by: SS

Date: 1.6.22
 Checked: PH
 Pages: 2 OF 3

SOAKAWAY DESIGN CALC

Output

DESIGN IN ACCORDANCE WITH BRE DIGEST 365 (2016)

ALLOWANCE FOR CLIMATE CHANGE = 40%

REVISED $f = (0.273 \times 0.4) + 0.273 = 0.382$

SOIL INFILTRATION RATE f

VP75-25 = $0.3 \times 0.3 \times (0.15) = 0.0135 \text{ m}^3$
 @ 50 = $(0.3 \times 0.15 \times 4) + (0.3 \times 0.3) = 0.27 \text{ m}^2$
 @ 75-25 = 7 mins

$\Rightarrow f = \frac{0.0135}{0.27 \times 7 \times 60}$
 $= 11.90 \times 10^{-5} \text{ m/sec}$

INFLOW TO SOAKAWAY (L) = $L = A \times R$
 $= 211 \times 0.0158 = 3.33 \text{ m}^3$

OUTFLOW FROM SOAKAWAY (O)

$O = a_{50} \times f \times D$

$\therefore a_{50} = 2(25+10) \times 0.4 \div 2$
 $= 140.4 \text{ m}^2$

$f = 11.90 \times 10^{-5} \text{ m/s}$

$\therefore O = (140.4 \text{ m}^2) \times 11.90 \times 10^{-5} \times (D \times 60)$
 m³

SOAKAWAY = TOWERS VOLUME (S) REQ'D

$= 25 \times 0.4 \times 60 \times 0.95 = 0.956 \text{ m}^3$

\therefore FOR M10-10 $1-O = S$

$\Rightarrow 3.33 - (140.4 \text{ m}^2) \times (11.90 \times 10^{-5}) \times (10 \times 60) = 0.956$

* NOTE SHED
 MAX LOADING
 TO PERMEABLE
 PAVING
 AT CAR PARKING
 AREA

FOR M10-10
 $= 113 \text{ mm}$
 $= 0.0113 \text{ m}$
 4.5% CC
 $\Rightarrow 1582 \text{ mm}$
 $= 0.0158 \text{ m}$

D = START
 EVAPORATION

ASSUME SOAKAWAY
 DIMS
 2.5m x 2.5m
 x 0.5m
 EFFECTIVE STORAGE

PROPOSED SOAKAWAY
 SYSTEM
 LAYIN ADACELL
 ECO 1.0m x 0.5m
 x 0.4m DEPT
 95% VOID
 25% TO

M10-10

Calculation Sheet



ENGINEERS IRELAND

Project No: 100-30
 Client: TONI & HAZEL REILLY
 Project: OAK LODGE (LONDRAKIM)
 Calc'd by: SD

Date: MAR 22
 Checked: PH
 Pages: 3 OF 3

SOAKAWAY DESIGN CALC

Output

REQUIRED SOAKAWAY WIDTH = 3.22m

FOR 570mm DRAINAGE MID-15

REQUIRED W = 3.25m

FOR MID-30 W = 4.62m

FOR MID-60 W = 4.5m

FOR MID-120 W = 5.60m

FOR 1 HOUR EVENT

SOAKAWAY 2.5m LONG x 0.4m x 4.5m
 WALL SURFACE

USE SOAKAWAY 2.5m LONG x 4.5m W.D.
 x 0.4m EFFECTIVE
 DEPTH

TIME TO UNIFORMITY t_{SS0}

$$= S \times 0.5 / 0.550 \times f$$

$$= (0.95 \times 4.5) \times 0.5 / (1 + (0.4 \times 4.5)) \times 1190 \times 0.5 \times 3600$$

$$= 2.0425 / 1.165$$

1.75 HOURS

$$L = \frac{15}{13.2 \times 0.4} + 13.2 = 18.62m$$

$$= 3.929m^2$$

$$L = \frac{30}{16.9 \times 0.4} + 16.9 = 23.66m$$

$$= 4.992m^2$$

$$L = \frac{60}{21.5 \times 0.4} + 21.5 = 30.1m$$

$$= 6.351m^2$$

$$L = \frac{120}{27.0 \times 0.4} + 27.0 = 38.36m$$

$$= 8.094m^2$$

$$L = \frac{240}{32.0 \times 0.4} + 32.0 = 42.72m$$

$$L = 10.28m^2$$

OK

Appendices



Appendix A
(Percolation test procedure and Photos)

Trial Hole No 1. Results – 9th March 2022

0.0m - 0.3m	Brown silty topsoil with tree and vegetation roots
0.3m – 0.8m	Firm brown/grey mottled gravelly clay with angular/sub angular limestone cobbles and some boulders
0.8m – 1.5m	Very stiff brown gravelly clay with sub angular limestone cobbles and boulders



Trial Hole No 1- Excavated



Trial Hole No 1 – Soil Profile



Trial Hole No 1 - Water test for seepage



Trial Hole No 1 – Water empty 300mm in 19 mins



Soakpit No 1 Test Hole – Location



SoakPit Test Hole No 1 – Excavated to 1.5m deep



Soakpit No 1 Test Hole – Soil Profile



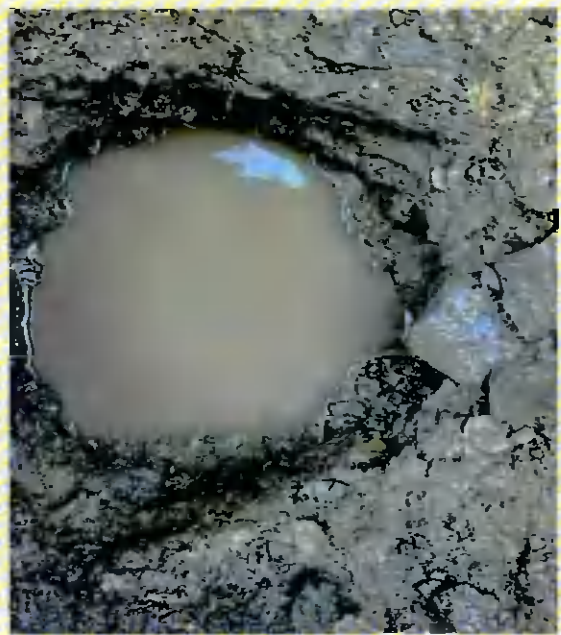
Soakpit Test Hole 2 (Test Zone)



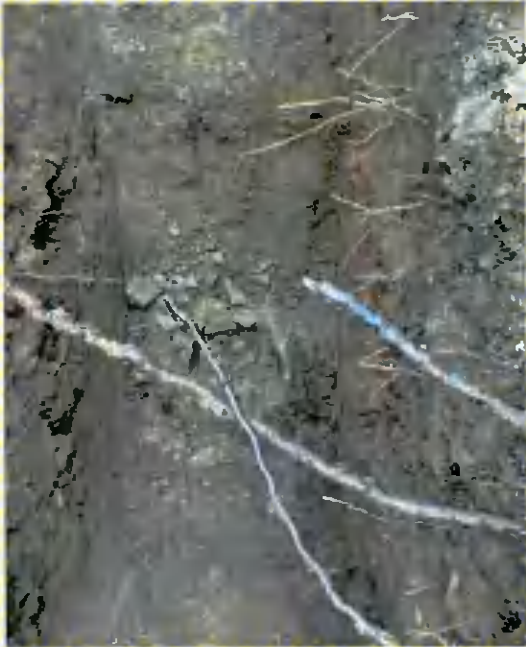
Test No 1 Pit 300 x 300 x 300 deep



Test No 1 75% Level 10:04



Test No 1 25% Level 10:08



Test Hole No 1 Empty 10:14



Test No 2 75% Level 10:34



Test No 2 25% 10:40+



Test No 2 Empty 1 10:45



Test No 3 75% Level 11:04



Test No 3 25% Level 11:11



Test No 3 Empty 11:19

Appendix B
(Design data)

Met Eireann
Return Period Rainfall Depths for sliding Durations
Irish Grid: Easting: 307199, Northing: 231026.

DURATION	Interval		Years														
	6months,	1year,	2,	3,	4,	5,	10,	20,	30,	50,	75,	100,	150,	200,	250,	500,	
5 mins	2.4,	3.5,	4.1,	5.1,	5.8,	6.3,	8.1,	10.2,	11.6,	13.6,	15.5,	16.9,	19.2,	21.0,	22.4,	N/A	
10 mins	3.3,	4.9,	5.8,	7.1,	8.1,	8.8,	11.3,	14.2,	16.2,	19.0,	21.6,	23.6,	26.7,	29.2,	31.3,	N/A	
15 mins	3.9,	5.7,	6.8,	8.4,	9.5,	10.4,	13.5,	16.7,	19.0,	22.3,	25.4,	27.7,	31.4,	34.3,	36.8,	N/A	
30 mins	5.1,	7.5,	8.8,	10.8,	12.2,	13.3,	16.9,	21.1,	24.0,	28.0,	31.7,	34.5,	39.0,	42.5,	45.5,	N/A	
1 hours	6.7,	9.7,	11.4,	13.9,	15.7,	17.0,	21.5,	26.7,	30.2,	35.1,	39.6,	43.0,	48.4,	52.7,	56.2,	N/A	
2 hours	8.8,	12.7,	14.8,	18.0,	20.1,	21.8,	27.4,	33.8,	38.0,	44.0,	49.4,	53.6,	60.1,	65.2,	69.5,	N/A	
3 hours	10.4,	14.8,	17.2,	20.8,	23.3,	25.2,	31.5,	38.7,	43.5,	50.3,	56.3,	61.0,	68.3,	73.9,	78.6,	N/A	
4 hours	11.7,	16.5,	19.2,	23.1,	25.8,	27.9,	34.8,	42.7,	47.9,	55.2,	61.7,	66.8,	74.7,	80.8,	85.9,	N/A	
6 hours	13.7,	19.3,	22.3,	26.9,	29.9,	32.3,	40.1,	48.9,	54.8,	63.0,	70.3,	76.0,	84.7,	91.5,	97.2,	N/A	
9 hours	16.1,	22.5,	26.0,	31.2,	34.6,	37.3,	46.2,	56.1,	62.7,	71.9,	80.1,	86.4,	96.2,	103.7,	110.0,	N/A	
12 hours	18.0,	25.2,	28.9,	34.6,	38.4,	41.4,	51.0,	61.9,	69.0,	79.0,	87.8,	94.7,	105.2,	113.4,	120.1,	N/A	
16 hours	21.2,	29.4,	33.7,	40.2,	44.5,	47.8,	58.7,	70.9,	78.9,	90.1,	100.0,	107.7,	119.4,	128.5,	136.0,	N/A	
24 hours	23.8,	32.8,	37.5,	44.6,	49.4,	53.0,	64.9,	78.2,	86.9,	99.0,	109.7,	118.0,	130.6,	140.4,	148.5,	176.5,	
2 days	29.8,	40.0,	45.3,	53.1,	58.2,	62.2,	74.9,	88.9,	97.9,	110.4,	121.3,	129.7,	142.4,	152.2,	160.2,	187.8,	
3 days	34.6,	45.7,	51.5,	59.9,	65.4,	69.6,	83.0,	97.6,	107.0,	119.9,	131.2,	139.7,	152.7,	162.6,	170.7,	198.6,	
4 days	38.8,	50.8,	56.9,	65.8,	71.6,	76.0,	90.0,	105.3,	115.0,	128.3,	139.8,	148.6,	161.8,	171.9,	180.2,	208.3,	
6 days	46.2,	59.6,	66.3,	76.0,	82.3,	87.1,	102.2,	118.5,	128.9,	142.8,	154.9,	164.0,	177.8,	188.2,	196.7,	225.6,	
8 days	52.7,	67.3,	74.5,	85.0,	91.7,	96.8,	112.8,	129.9,	140.7,	155.4,	167.9,	177.4,	191.6,	202.4,	211.1,	240.7,	
10 days	58.7,	74.3,	82.0,	93.1,	100.2,	105.6,	122.4,	140.3,	151.5,	166.7,	179.7,	189.5,	204.2,	215.2,	224.2,	254.5,	
12 days	64.3,	80.8,	89.0,	100.6,	108.1,	113.7,	131.3,	149.3,	161.4,	177.1,	190.5,	200.6,	215.7,	227.0,	236.2,	267.1,	
16 days	74.7,	92.8,	101.8,	114.4,	122.5,	128.5,	147.4,	167.2,	179.5,	196.1,	210.2,	220.8,	236.5,	248.3,	257.9,	290.0,	
20 days	84.3,	103.9,	113.5,	127.0,	135.6,	142.1,	162.0,	182.9,	195.9,	213.2,	228.0,	239.0,	255.3,	267.6,	277.5,	310.6,	
25 days	95.6,	116.8,	127.1,	141.6,	150.8,	157.7,	178.9,	200.9,	214.6,	232.9,	248.3,	259.8,	276.8,	289.6,	299.9,	334.1,	

NOTES:

N/A Data not available

These values are derived from a Depth Duration Frequency (DDF) Model

For details refer to:

'Fitzgerald D. L. (2007). Estimates of Point Rainfall Frequencies, Technical Note No. 61, Met Eireann, Dublin',

Available for download at www.met.ie/climate/dataproducts/Estimation-of-Point-Rainfall-Frequencies_TN61.pdf

$$\tau \text{ VALUE} = \frac{17.0}{62.2} = 0.273$$

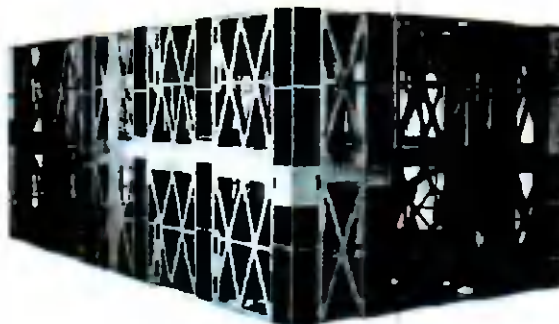


PRODUCT INFORMATION SHEET

AquaCell Eco

Description:

AquaCell Eco is manufactured from specially reformulated, recycled material and has been specifically designed for shallow, non trafficked, landscaped applications. AquaCell Eco is NOT suitable for locations subject to high water tables.



Technical specifications:

Cat code	6LB025	Void ratio	95%
Colour	Black	Material	Recycled PP
Dimensions	1m x 0.5m x 0.4m	Vertical loading	21.3 tonnes/m ² (213 kN/m ²)
Weight	7kg	Lateral loading	5.2 tonnes/m ² (52 kN/m ²)
Storage volume	190 litres	BBA approval	Certificate 03/4018

Maximum installation depths

Typical soil type	Soil weight kN/m ³	Maximum depth of installation – to base of units (m) ¹	
		Angle of internal friction ϕ (degrees) ^{2, 3}	Landscaped areas
Over consolidated stiff clay	20	24	1.53
Silty sandy clay	19	26	1.68
Loose sand and gravel	18	30	2.08
Medium dense sand and gravel	19	34	2.35
Dense sand and gravel	20	38	2.68

Minimum cover depths

Landscaped areas	
Minimum cover depth (m)	0.30 ³

1. These values relate to installations where the groundwater is a minimum of one metre below the base of the excavation.
2. AquaCell Eco units should not be used where groundwater is present.
3. 0.5m cover is required where a ride-on mower may be used.

Assumptions made:

- Ground surface is horizontal
- Shear planes or other weaknesses are not present within the structure of the soil

Source: BBA

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